Scottish Government Windfarm Carbon Assessment Tool - Version 2.14.1 Contributors: ¹D.Nayak, ¹J.U. Smith , ¹P. Smith, 27/01/2023 This spreadsheet calculates payback time for windfarm sited on peatlands using methods given in Nayak et al, 2008 (https://www.scotland.gov.uk/Publications/2008/06/25114657/0 and revised equations for 6H6 emissions (Nayak, D.R., Miller, D., Nolan, A., Smith, P. and Smith, J.U., 2010, Calculating carbon budgets of wind farms on Scottish peatland. Mires and Peat 4: Art. 9, Online: (http://www.mires.and-peat.net/map04/map.04.09.htm) Version 2.0.0 - Adapted to include detail of forestry management, Smith et al., 2011. P.Graves UNIVERSITY OF ABERDEEN http://www.scotland.gov.uk/WindFarmsAndCarbon Version 2.14.0 - Corrections to calcualtion of peat removed for hardstanding plus corrections to emission factors and changes as detailed in previous worksheets Revised by J.U.Smith to correct forestry and restoration sheets Version 2.14.1 - Equivalent to version 2.14.0 but with worksheets unprotected for your own use. Do not use this version in planning applications. The James Hutton Institute INSTRUCTIONS There are 6 worksheets giving instructions, data entry and outputs, \dots Forestry Commission Instructions Do I need to use this tool? Data needed in all calculations Core input data Data needed in all calculations Forestry input data Extra details sometimes needed for forestry calculations Construction input data Extra details sometimes needed for construction calculations Payback time and CO2 emissions Click here 2. CO2 loss due to turbine life 3. CO2 loss due to turbine life 3. CO2 loss due to backup 4. Loss of CO2 Fixing Pot. Core input data THE UNIVERSITY of EDINBURGH University of Glasgow 5. Loss of soil CO_2 5a. Volume of peat removed 5b. CO_2 loss from removed peat Note on official version number 5c. Volume of peat drained 5d. CO₂ loss from drained peat 5e. Emission rates X refers to the release number 5e. Emission rates 6. CO₂ loss by DOC & POC loss 7i, Forestry CO₂ loss - simple 7ii, Forestry CO₂ loss - detailed 7a, C sequest, in trees (3PG) 7b, C seq, in soil under trees Y refers to released updates on Z refers to unreleased updates on release X.Y Officially released versions will always have Z=0 7c. Average stand data 7d. Windspeed ratios 8. CO2 gain - site improvement If you make changes of your own In addition, there are spreadsheets containing references and requesting feedback. References please do not refer to your modified spreadsheet using the official version Frequently asked questions Notes on calculations are given in pale green text boxes.... Click here to see example of Notes Box Protocols for measurements are given in pale yellow comment boxes.... Click here to see example of Protocol Box The latest version is published at www.scotland.gov.uk/WindFarmsAn Assumptions are given in pale blue text boxes.... Click here to see example of Assumptions Box

Do I need to use this tool?		
1. Will the site be drained on construction of the windfarm?	Yes ▼	
2. Is the soil at the site highly organic? i.e. is the soil organo-mineral or organic, (i.e. a peaty gley or peat)?	Yes ▼	
3. Does windfarm construction require a significant amount of deforestation? i.e. is removal in excess of keyholing the turbines within the forest boundary?	Yes ▼	
You should use this tool because the soil is highly organic. Please move to the Core input data sheet and complete the form	n to obtain an estimate of C payback time	
	Click here to return to Instructions sheet	- Inches
	Click here to never on to Core input data sh	Click here Click here

Core input data

ENTER INPUT DATA HERE I VALUES SHOULD ONLY BE CHANGED ON THIS SHEET. DO NOT USE EXAMPLE VALUES AS DEFAULTSENTER YOUR OWN VALUES THAT ARE SPECIFIC TO YOUR PARTICULAR SITE.

Note: The input parameters include some variables that can be specified by default values, but others that must be site specific. Variables that can be taken from defaults are marked with purple tags on left hand side.

Click here to move to Payback Time

Click here to return to Instructions

Click here

	Expected values	Record	Pos	Record	ge of values	Record	Note: <u>Capacity factor</u> . The capacity factor of any power plant is the proportion of energy produ
Input data	Enter expected value here	source of data	Enter minimum value here	source of data	Enter maximum value here	source of data	Note: <u>capacity lactor</u> . The capacity ractor or any power praint is the proportion of netrepty production and uning a given period with respect to the energy that would have been produced had the farm been running continually and at maximum output (DECC (2004); see also www.bwea.com/reficapacityfactors.html). Capacity Factor = Electricity generated during the period [kWh]/ (Installed capacity [kW] x nur
Windfarm characteristics mensions	+		+		+		Capacity Factor — Electricity generated during the period [kWin] (installed capacity [kW] x hin hours in the period [h]) We recommend that a site-specific capacity factor site should be used (as measured during p stage), and should represent the <u>awerage</u> emission factor expected over the lifetime of the wir
o. of turbines etime of windfarm (years)	8 40	Ch 2 Ch 2	8 40	Ch 2 Ch 2	8 40	Ch 2 Ch 2	accounting for decline in efficiency with age (Hughes, 2012). The 5 year average capacity fact "load factor") for UK onshore wind between 2010 and 2014, based on average beginning and
formance wer rating of turbines (turbine capacity) (MW)	6	Ch 2	6	Ch 2	6	Ch2	year capacity, was 29.2% (DUKES, 2015).
pacity factor nter estimated capacity factor (percentage efficiency)	Direct input of capacity factc ▼ 35.0		Direct input of capacity facto ▼ 31.5		Direct input of capacity facto ▼ 38.5◆		Note: Extra capacity required for backup. If 20% of national electricity is generated by wind er the extra capacity required for backup is 5% of the rated capacity of the wind plant (Dale et al
kup ra capacity required for backup (%)	5		5		5 ←		We suggest this should be 5% of the actual output. If it is assumed that less than 20% of natic electricity is generated by wind energy, a lower percentage should be entered (0%). The Hous Lords Economic Affairs Committee report on The Economics of Renewable Energy (Parliame Business, 2008) notes that to cover peak demand a '20% margin of extra capacity has been stoned.
ditional emissions due to reduced thermal efficiency of the erve generation (%)	10		10		10		to keep the risk of a power cut due to insufficient generation at a very low level.' The estimate
rbon dioxide emissions from turbine life . manufacture, construction, decommissioning)	Calculate wrt installed capac ▼		Calculate wrt installed capac ▼		Calculate wrt installed capac ▼		provided by BERR was a range of 10% to 20% of installed capacity of wind energy. E.O.N is re as proposing that the capacity credit of wind power should be 8%, and The Renewable Energy Foundation proposed the use of the square root of the wind capacity (in GW) as conventional capacity (e.g. 36 GW of wind plant to match 6 GW of conventional plant).
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Characteristics of peatland before windfarm development							Note: Extra emissions due to reduced thermal efficiency of the reserve power generation ≈ 10 (Dale et al 2004).
pe of peatland erage annual air temperature at site °C)	Acid bc ▼ 10.1	Ch 15	Acid bc ▼ 10.1	Ch 15	Acid bc ▼	Ch 15	Note: Emissions from turbine life, If total emissions for the windfarm are unknown, emissions be calculated according to turbine capacity. The normal range of CO ₂ emissions is 394 to 814 MW (White & Kulcinski, 2000: White, 2007).
erage depth of peat at site (m) Content of dry peat (% by weight)	0.34	PRSA	0.34 0	PRSA	0.34 0	PRSA	Note: Type of peatland. An 'acid bog' is fed primarily by rainwater and often inhabited by spha moss, thus making it acidic (Stoneman & Brooks, 1997).
erage extent of drainage around drainage features at site (m)	10.00		5.00		15.00	Ch 9	A fen' is a type of wetland fed by surface and/or groundwater (McBride et al., 2011).
erage water table depth at site (m) soil bulk density (g cm³) Characteristics of bog plants	5.00 0.00		0.10 0.00		10.00 0.00	Ch 9	Note: Time required for regeneration of previous habitat. Loss of fixation should be assumed to
ne required for regeneration of bog plants after restoration ars)	10		5		15 🕶		over lifetime of windfarm only. This time could be longer if plants do not regenerate. The requirements for after-use planning include the provision of suitable refugia for peat-forming
bon accumulation due to C fixation by bog plants in undrained tts (tC ha ⁻¹ yr ⁻¹)	0.25		0.12		0.31		vegetation, the removal of structures, or an assessment of the impact of leaving them in situ. Methods used to reinstate the site will affect the likely time for regeneration of the previous This time could also be shorter if plants regenerate during lifetime of windfarm. If so, enter nur years estimated for regeneration.
Forestry Plantation Characteristics thod used to calculate CO ₂ loss from forest felling	Enter simple data		Enter simple data ▼		Enter simple data ▼		Note: Carbon fixation by bog plants Apparent C accumulation rate in peatland is 0.12 to 0.31 t C har¹ yr¹ (Turunen et al., 2001; Bc
rea of forestry plantation to be felled (ha) verage rate of carbon sequestration in timber (tC ha-1 yr-1)	0 3.60	Ch 8	0 2.40	Ch 8	0 4.40	Ch-8	al., 1995). The SNH guidance uses a value of 0.25 t C ha ⁻¹ yr ⁻¹ .
Counterfactual emission factors update counterfactual emission factors from							Note: Area of forestry plantation to be felled. If the forestry was planned to be removed, with n further rotations planted, before the windfarm development, the area to be felled should be en
Click here (not yet operational)	0.045		0.045		0.045		as zero. Note: <u>Plantation carbon sequestration</u> . This is dependent on the yield class of the forestry. The
al-fired plant emission factor (t CQ MWh ⁻¹) d-mix emission factor (t CQ MWh ⁻¹)	0.945 0.207		0.945 0.207		0.945▼ 0.207▼		Note: <u>Plantation carbon sequestration</u> . This is dependent on the yield class of the forestry. The technical guidance assumed yield class of 16 m³ ha¹ yr¹, compared to the value of 14 m³ ha¹ provided by the Forestry Commission. Carbon sequestered for yield class 16 m³ ha¹ y² = 3.6 yr¹ (Cannell, 1999).
ssil fuel-mix emission factor (t CQ MWh ⁻¹) Borrow pits	0.424		0.424		0.424		Note: Coal-Fired Plant and Grid Mix Emission Factors. Coal-fired plant emission factor (EF) fre electricity supplied in 2014 = 0.093 t CO ₂ MWh ⁻¹ -Grid-Mix EF for 2014 = 0.394 t CO ₂ MWh ⁻¹ -Srid-Mi
nber of borrow pits rrage length of pits (m)	1 90.28	Ch 2	1 90.28	Ch 2	1 90.28	Ctr2	= DUKES, 2015b. Note: <u>Fossil Fuel-Mx Emission Factor</u> . The emission factor from electricity supplied in 2014 frossil fuels = 0.642 t CO ₂ MW ⁻ 1. Source = DUKES, 2015b.
rage width of pits (m) rage depth of peat removed from pit (m)	90.28 0.34	Ch 2 PRSA	90.28 0.34	Ch 2 PRSA	90.28 0.34	Ch 2 PRSA	Tossil fuels = 0.642 t CO ₂ MWh ⁻¹ . Source = DUKES, 2015b.
oundations and hard-standing area associated with each turbine							
nding	Rectangular with vertical wal		Rectangular with vertical wal ▼		Rectangular with vertical wal ▼		
erage length of turbine foundations (m) erage width of turbine foundations (m)	25.5 25.5	Ch 2 Ch 2	25.5 25.5	Ch 2 Ch 2	25.5 25.5	Ch 2 Ch 2	
erage depth of peat removed from turbine foundations (m) erage length of hard-standing (m)	0.30 80	Ch 2 Ch 2	0.10 75	Ch 2 Ch 2	0.50 85	Ch 2 Ch 2	
rrage width of hard-standing (m) rrage depth of peat removed from hard-standing (m)	68 0.34	Ch 2 PRSA	65 0.34	Ch 2 PRSA	70 0.34	Ch 2 PRSA	
Access tracks al length of access track (m)	5830 3790	Ch 2 Ch 2	5830 2700	Ch 2 Ch 2	5830 ←	Ch 2	Note: Total length of access track. If areas of access track overlap with hardstanding area, ex these from the total length of access track to avoid double counting of land area lost.
sting track length (m) gth of access track that is floating road (m)	0 0	Ch 2 Ch 2 Ch 2	3790 0 0	Ch 2 Ch 2 Ch 2	3790 0 0	Ch 2 Ch 2 Ch 2	
ating road width (m) ating road depth (m) gth of floating road that is drained (m)	0.00	Ch 2 Ch 2	0.00	Ch 2 Ch 2	0.00◀	Ch 2 Ch 2	Note: <u>Floating road depth</u> . Accounts for sinking of floating road. Should be entered as the ave depth of the road expected over the lifetime of the windfarm. If no sinking is expected, enter a
gth of industrial road trials is drained (m) gth of access track that is excavated road (m)	0.00 2040	Ch 2 Ch 2	0.00 2040	Ch 2 Ch 2	0.00 ←	Ch 2 Ch 2	Note: Length of floating road that is drained. Refers to any drains running along the length of road.
rage depth of peat excavated for road (m)	4.5 0.34	Ch 2 PRSA	4.5 0.34	Ch 2 PRSA	4.5 0.34	Ch 2 PRSA	Note: Rock filled roads. Rock filled roads are assumed to be roads where no peat has been r
gth of access track that is rock filled road (m) ck filled road width (m)	0		0		0 4		and rock has been placed on the surface and allowed to settle.
ck filled road depth (m) ngth of rock filled road that is drained (m)	0		0		0		
erage depth of drains associated with rock filled roads (m) Cable Trenches	0.00		0.00		0.00		
ngth of any cable trench on peat that does not follow access cks and is lined with a permeable medium (eg. sand) (m)	0		0		0		Note: Depth of peat cut for cable trenches, in shallow peats, the cable trenches may be cut by
erage depth of peat cut for cable trenches (m)	0.00		0.00		0.00◀		peat. To avoid overestimating the depth of peat affected by the cable trenches, only enter the of the peat that is cut.
dditional peat excavated (not already accounted for above)			•				
ume of additional peat excavated (n³) a of additional peat excavated (n²)	0 0.0		0 0.0		0 0.0		Note: Peat Landslide Hazard. It is assumed that measures have been taken to limit damage (Executive, 2006, Peat Landslide Hazard and Risk Assessments. Best Practice Guide for Proposed Electricity Generation Developments. Sootish Executive, Ectiviship, pp. 34-5) so that CI Cosses due to peat landslidle can be ass
Peat Landslide Hazard blink: Peat Landslide Hazard and Risk Assessments: Best	negligible	PRSA	negligible	PRSA	negligible	PRSA	be negligible. Link: http://www.scotland.gov.uk/Publications/2006/12/21162303/1.
ctice Guide for Proposed Electricity Generation Developments nprovement of C sequestration at site by blocking drains,	riegiigibie	TROA	riegiigibie	TROA	riegiigibie	TROA	
restoration of habitat etc							
ea of degraded bog to be improved (ha) ster table depth in degraded bog before improvement (m)		drains orains willingt		drains grains willing		drains orains willing*	
ster table depth in degraded bog after improvement (m)		will not		uill not		ton Ilius	Note: Period of time when improvement can be guaranteed. This guarantee should be absolu
		drains will not		drains will not		drains will not	Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the requirement for the improvement to become effective. For example if time required for hydroic
		have its drained		have its drained		have its drained	habitat to return to its previous state is 10 years and the restoration can be guaranteed over the of the windfarm (25 years), the period of time when the improvement can be guaranteed shou entered as 25 years, and the improvement will be effective for (25-10) = 15 years.
ne required for hydrology and habitat of bog to return to its evious state on improvement (years)	2	d so is	2	d so is	2	d so is	
		omitted from this		omitted from this		omitted from this	
		calculat		calculat		calculat ion	
		ion		ion		ion	
		drains will not		drains will not	•	drains will not	
		have its drained		have its		have its drained	
riod of time when effectiveness of the improvement in degraded	2	blocke d so is	2	blocke d so is	2	blocke d so is	
g can be guaranteed (years)		omitted from		omitted from		omitted from	
		this calculat		this calculat		this calculat	
		ion		ion		ion	
orovement of felled plantation land a of felled plantation to be improved (ha) ter table depth in felled gree before improvement (m)	0		0		0		
ter table depth in felled area before improvement (m) ter table depth in felled area after improvement (m) te required for hydrology and habitat of felled plantation to return	0.00 0.00		0.00 0.00		0.00 0.00		Note: Period of time when improvement can be guaranteed. This gurantee should be absolute
the required for hydrology and habitat of felled plantation to return its previous state on improvement (years) iod of time when effectiveness of the improvement in felled	2		2		2		Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absoluted Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the requirement for the improvement to become effective. For example if time required for hydrot.
tod of unle when enecuverless of the improvement in lened intation can be guaranteed (years) storation of peat removed from borrow pits	2		2		2 ←		requirement to the improvement to become effective. For example it may required for nyarow habitat to return to its previous state is 10 years and the restoration can be guaranteed over to fit the windfarm (25 years), the period of time when the improvement can be guaranteed shower than the provided for (25 full p. 15 years).
a of borrow pits to be restored (ha) oth of water table in borrow pit before restoration with respect to	8,150		8150		8150		30 20 yours, and the improvement will be effective for (25 -10) = 15 years.
restored surface (m) oth of water table in borrow pit after restoration with respect to	0.00		0.00		0.00		
restored surface (m) e required for hydrology and habitat of borrow pit to return to its	0.00		0.00		0.00		Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absolut Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the
vious state on restoration (years) iod of time when effectiveness of the restoration of peat	2		2		2 ←		requirement for the improvement to become effective. For example if time required for hydrole habitat to return to its previous state is 10 years and the restoration can be guaranteed over the windfarm (25 years), the period of time when the improvement can be guaranteed shounds.
loved from borrow pits can be guaranteed (years) ly removal of drainage from foundations and hardstanding							of the windrarm (25 years), the period of time when the improvement can be guaranteed shot entered as 25 years, and the improvement will be effective for (25 -10) = 15 years.
ter table depth around foundations and hardstanding before toration (m) ter table depth around foundations and hardstanding after	0.00		0.00		0.00		Note: Period of time when improvement can be guaranteed. This is assumed to be the lifetime
ter table depth around foundations and hardstanding after loration (m) let to completion of backfilling, removal of any surface drains, and	0.00		0.00		0.00		windfarm as restoration after windfarm decommissioning is already accounted for in restoration site
ne to completion of backfilling, removal of any surface drains, and restoration of the hydrology (years) Restoration of site after decomissioning	0		0		0		Note: Restoration of site. If the water table at the site is returned to its original level or higher decommissioning, and habitat at the site is restored, it is assumed that C losses continue only
I the hydrology of the site be restored on decommissioning?	Yés		Yes		Yes		decommissioning, and habitat at the site is resolved, it is assumed that C losses comme on lifetime of the windfarm. Otherwise, C losses from drained peat are assumed to be 100%.
I you attempt to block any gullies that have formed due to the	Not applic ▼		Not applic ▼		Not applic ▼		-
ndfarm?	Not applic ▼ Yes		Not applic ▼ Yes		Not applic ▼ Yes		
dfarm? I you attempt to block all artificial ditches and facilitate rewetting? I the habitat of the site be restored on decommissioning?			.03		Not appli ▼		
l you attempt to block all artificial ditches and facilitate rewetting?	Not applic ▼		Not appl ▼				
you attempt to block all artificial ditches and facilitate rewetting? the habitat of the site be restored on decommissioning?	_		Not applic ▼		Not applic ▼		Note: Choice of methodology for calculating emission factors. The IPCC default methodology
you attempt to block all artificial ditches and facilitate rewetting? the habitat of the site be restored on decommissioning? you control grazing on degraded areas? you manage areas to favour reintroduction of species	Not applic ▼			<u> </u>			Note: Choice of methodology for calculating emission factors. The IPCC default methodology internationally accepted standard (IPCC, 1997). However, it is stated in IPCC (1997) that their loopin estimates, and "these rates and production periods can be used if countries do not have considered to the control of the contro

Forestry input data

ENTER DETAILS OF FORESTRY MANAGEMENT HERE!

Note: Data only needed if seried to calculate capacity factor from forestry data (cell C15 in Core input data sheet), or to include detailed forestry of the cell control of the cell capacity factor from forestry data (cell C15 in Core input data sheet), or to include detailed forestry http://linyurl.com/modifiand.carbon.code http://linyurl

Click here to move to Payback Time
Click here to return to Instructions
Click here



No POC losses for bare soil included yet. If extensive areas of base soil is present at site need modified calculated and the second se

Input data Expected value here end that the source of data Windfarm characteristics Location Expected value here end that the source of data Expected value here end that the source of data Possible range of value for source of data Factor of data Factor of data Of data Of data	Note: <u>Estimated desertions</u> . <u>Estimated dosertions</u> for maintenance set. Feer reports on obwrited <u>Uniforms</u> are publically available. However, one review by Garradt Hassan, (2011) suggest minimum downtions reported was 2% for the annual moving wavegar for between 8 to 0 poperation of new turbines, for a sumple of 2400 furtiens. For a summary offinings see Gar
Input data Enter expected value here of data Windfarm characteristics Enter minimum value here of data Windfarm characteristics	Record Re
Windfarm characteristics	maximum value here source Plassan (2011).
	of data Note: Emissions from felling and timber removal; Based on remissions factors from UK taken from Morison et all (2011), if clearfelling assum- performed by harvester and timber is assumed extracted with forwarder, the emissions are CO. p. 32
2003001	
Distance to nearest biofuel plant (km) Dimensions	Note: Emissions associated with transportation, Assuming trasportation by trucks running on diesel and 20% of journey taken on forest rod emissions factor obtained from Morison et al. (2011) is 39.33 g CO ₂ km ⁻¹ t ⁻¹ (range 38.5 - 4
Total wind farm area (ha) Performance	emissions factor obtained from Morison et al (2011) is 39.33 g CO ₂ km ⁻¹ t ⁻¹ (range 38.5 – 4 CO ₂ km ⁻¹ t ⁻¹ - average = 39.33 g CO ₂ km ⁻² t ⁻²)
Height of turbines (m) Average site windspeed (m ε ^t)	
Estimated downtime for maintenance etc (%)	
Emissions due to forestry operations Emissions from felling (g CO ₂ m ³)	
Emissions of CO ₂ associated with transportation (g CO ₂ km ⁻¹ Γ ¹)	✓
Forestry Plantation Characteristics	Nu. D
Note - total number of turbines already specified:	Note: <u>Power curve</u> Based on Vettas 2 JMW Optispeed turbine with roughness class C2, modelled over wind 5-10 m s ⁻¹ . To define a the power curve for a different turbine type, plot annual power out MWN) against annual windspeed, Win s ⁻¹ 3 and it is mare regression to obtain slope, a,
Number of turbines in this area	
Power curve - NOT USED! (In CORE INPUT DATA sheet you have selected User-defined User-defined User-defined User-defined User-defined	P = aW + b
to input capacity factor directly. No need to select!) Major soil sub-group Deep Peat Deep Peat Deep Peat	
Wajor son sub-group	Note: <u>Soil sub-group</u> Ots pine ▼
Felled Forest Biomass used as biofuel?	Peaty gley = Peaty Soils (5-50cm) e.g. peaty gley, peaty podsol Deep peat = Deep Peat (>50cm) e.g. basin and blanket bogs
Felling regime	Note: Species So far only Scots pine and Stika spruce included.
Age of forestry when felled for windfarm (yr) Area felled around each turbine (ha)	
Width of forest around felled area (m) Value of felled forestry as a biomass fuel (MWh t ¹)	Note: Value of felled forestry Values available in Mason et al., 2009.
(Carbon : Biomass) ratio of felled forestry	
Replanting regime Years after felling when replanting occurs	Note: <u>Carbon: Biomass ratio of felled forestry</u> Wood blomass can be converted to dr using wood density based values from Lavers (1983) with a subsequent assum
Age of seedlings on planting (yr) Area replanted around each turbine (ha)	C:dry matter ratio is 50% (Matthews 1993). For simplicity an integrated factor, 'wood density to biomass factor' taken from Mason et al (2009) can be used.
AREA 2	Value = 0.5
Number of turbines in this area Power curve - NOT USED!	▼
(In CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!)	
Major soil sub-group	<u> </u>
Species V	<u>▼</u>
Felled Forest Biomass used as biofuel?	▼
Felling regime Age of forestry when felled for windfarm (yr)	
Area felled around each turbine (ha)	
Width of forest around felled area (m) Value of felled forestry as a biomass fuel (MWh t ¹)	
(Carbon : Biomass) ratio of felled forestry Replanting regime	<mark></mark>
Years after felling when replanting occurs	
Age of seedlings on planting (yr) Area replanted around each turbine (ha)	
Area replanted around each turbine (na)	
AREA 3	
ASEA3 Number of turbines in this area Power curve - NOT USED!	
ANIEAS Number of turbines in this area Power curve - NOT USED! (In CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!)	
ANIEAS Number of turbines in this area Power curve - NOT USED! (In CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!) Major soil sub-group	
ANIEAS Number of turbines in this area Power curve - NOT USED! (In CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!) Major soil sub-group Species	<u> </u>
ALLS. Number of turbines in this area Power curve - NOT USED! (in CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!) Major soil sub-group Species Fellod Forest Blomass used as biofuel?	
ALLS. Number of turbines in this area Power curve - NOT USED! (in CORE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!) Major soil sub-group Species Felled Forest Biomass used as biofuel? Felling regime Age of forestry when felled for windfarm (yr)	<u> </u>
Alias Number of turbines in this area Power curve - NOT USED! (in COKE INPUT DATA sheet you have selected to input capacity factor directly. No need to select!) Major soil sub-group Species Felled Forest Biomass used as biofuel? Felling ringim Age of forestry when felled for windfarm (yr) Area felled around each turbine (ha)	<u> </u>
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Forestry input data
ENTER DETAILS OF FORESTRY MANAGEMENT HERE!
Note: Data only needed if select to calculate capacity factor from forestry data (cell C15 in Core

Click here to move to Payback Time
Click here to return to Instructions
Click here

Construction input data

ENTER DETAILS OF CONSTRUCTION HERE!

Note: This data only used in the calculation if the selection "Enter detailed information" is made in cell C50 of the Core input data sheet.

Click here to move to Payback Time
Click here to return to Core input data

Click here
Click here

	Expected values	Possible rang	e of values
	Recor		Record
Input data	Enter expected value here source	Enter minimum value here source	Enter maximum value here source
	of data	of data	of data
Construction design Note - total number of turbines already specified:	8	8	8
AREA 1 Number of turbines in this area	8 Ch 2	8 Ch 2	8 Ch-2
<u>Turbine foundations</u>		, July	
Average depth of peat removed when constructing foundations (m) Approximate geometric shape of whole dug when constructing	Rectangular 🔻	Rectangular 🔻	Rectangular ▼
foundations	Rectangular	Rectangular 🔻	Rectangular 🔻
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Hardstanding			
Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing	Rectangular	Rectangular	Rectangular
hardstanding Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
Piling	No ▼	No ▼	No ▼
Is piling used? Volume of Concrete	NO T	100	NO .
Volume of concrete used (m³)			
AREA 2			
Number of turbines in this area			
Turbine foundations Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing	▼	▼	▼
foundations Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
<u>Hardstanding</u>			
Average depth of peat removed when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing	▼	▼	·
hardstanding	, T	The second secon	, , , , , , , , , , , , , , , , , , ,
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Piling			
Is piling used?			
Volume of Concrete			
Volume of concrete used (m³)			
AREA 3			
Number of turbines in this area Turbine foundations			
Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing foundations	▼	-	▼
Length at surface (m)			
Width at surface (m) Length at bottom (m)			
Width at bottom (m)			
Hardstanding Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing	▼	▼	▼
hardstanding Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
Piling	_		_
Is piling used? Volume of Concrete			
Volume of concrete used (m³)			
ARFA 4			
Number of turbines in this area			
Turbine foundations Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing	7	▼	₹
foundations Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
<u>Hardstanding</u>			
Average depth of peat removed when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing	▼	▼	Ţ
hardstanding		1	
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m)			
Is piling used?			
Volume of Concrete Volume of concrete used (m³)			
AREA 5 Number of turbines in this area			
Turbine foundations			
Average depth of peat removed when constructing foundations (m) Approximate geometric shape of whole dug when constructing	▼	▼	
foundations			
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Hardstanding			
Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing hardstanding			
Length at surface (m)			
Width at surface (m) Length at bottom (m)			
Width at bottom (m)			
Piling Is piling used?	▼	-	▼
Volume of Concrete			
Volume of concrete used (m ³)			

Results PAYBACK TIME AND CO₂ EMISSIONS

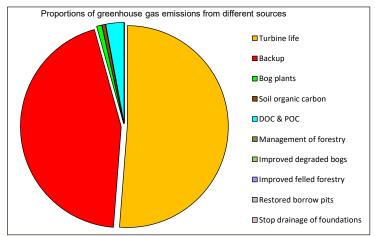
Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

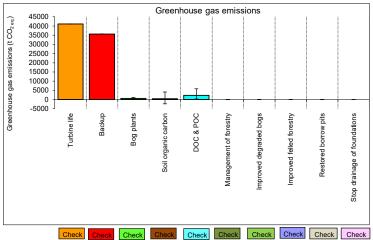
Click here to return to Input data Click here to return to Instructions

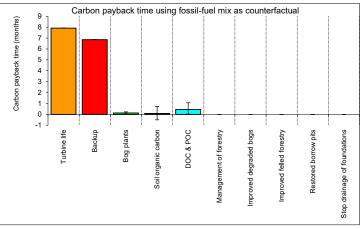


	Ехр.	Min.	Мах.
1. Windfarm CO ₂ emission saving over			
coal-fired electricity generation (tCO ₂ yr ⁻¹)	139074	125166	152981
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	30464	27417	33510
fossil fuel - mix of electricity generation (tCO ₂ yr ⁻¹)	62399	56159	68639
Energy output from windfarm over lifetime (MWh)	5886720	5298048	6475392
Total CO ₂ losses due to wind farm (t CO ₂ eq.)			
Losses due to turbine life (eg. manufacture, construction, decomissioning)	41108	41108	41108
3. Losses due to backup	35657	35657	35657
4. Losses due to reduced carbon fixing potential	669	198	1215
5. Losses from soil organic matter	460	-2298	4124
6. Losses due to DOC & POC leaching	2330	326	5861
7. Losses due to felling forestry	0	0	0
Total losses of carbon dioxide	80224	74991	87965
8. Total CO ₂ gains due to improvement of site (t CO ₂ eq.)			
8a. Change in emissions due to improvement of degraded bogs	0	0	0
8b. Change in emissions due to improvement of felled forestry	0	0	0
8c. Change in emissions due to restoration of peat from borrow pits	0	0	0
8d. Change in emissions due to removal of drainage from foundations & hardstanding	0	0	0
Total change in emissions due to improvements	0	0	0

3	l		
Total change in emissions due to improvements	0	0	0
RESULTS			
	Ехр.	Min.	Max.
Net emissions of carbon dioxide (t CO _{2 eq} .)			
	80224	74991	87965
Carbon Payback Time			
coal-fired electricity generation (years)	0.6	0.5	0.7
grid-mix of electricity generation (years)	2.6	2.2	3.2
fossil fuel - mix of electricity generation (years)	1.3	1.1	1.6
Ratio of soil carbon loss to gain by restoration (TARGET ratio (Natural Resources Wales) < 1.0)	No gains!	No gains!	No gains!
Ratio of CO ₂ eq. emissions to power generation (g / kWh) (TARGET ratio by 2030 (electricity generation) < 50 g /kWh)	14	12	17







Results
PAYBACK TIME AND CO₂ EMISSIONS
Thock time of the wir Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

Click here to return to Input data



Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greenhouse	nas	emice	einne

	Ехр.	Min	Max
Turbine life	41108	0	0
Backup	35657	0	0
Bog plants	669	471	546
Soil organic carbon	460	2758	3665
DOC & POC	2330	2004	3531
Management of forestry	0	0	0
Improved degraded bogs	0	0	0
Improved felled forestry	0	0	0
Restored borrow pits	0	0	0
Stop drainage of foundations	0	0	0

Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greenhouse gas emissions				Carbon pay	yback time	(months)
	Ехр.	Min.	Мах.	Ехр.	Min.	Мах.
Turbine life	41108	0	0	8	0	0
Backup	35657	0	0	7	0	0
Bog plants	669	471	546	0	0	0
Soil organic carbon	460	2758	3665	0	1	1
DOC & POC	2330	2004	3531	0	0	1
Management of forestry	0	0	0	0	0	0
Improved degraded bogs	0	0	0	0	0	0
Improved felled forestry	0	0	0	0	0	0
Restored borrow pits	0	0	0	0	0	0
Stop drainage of foundations	0	0	0	0	0	0
	80224			15		

Windfarm CO₂ emission saving

Note: The total emission savings are given by estimating the total possible electrical output of the windfarm multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from grid)

Click here to move to Payback Time Click here

		Total		Fo	restry Are	a 1	Fo	restry Are	a 2	For	estry Are	еа 3	Fo	restry Are	ea 4	For	restry Ar	ea 5
Values taken from input sheet	Exp	Min	Max	Exp	Min	Max	Exp	Min		Exp	Min	Max		Min	Max	Exp	Min	Max
Power Generation Characteristics		•	•															
No. of turbines	8	8	8				0	0						0	0		0	0
Power rating of turbines (turbine capacity) (MW)	6	6	6				6	6						6	6		6	6
Power of windfarm (MW)	48	48	48				0	0						0	0		0	0
Estimated downtime for maintenance etc (%)	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0	0
Counterfactual emission factors																		
Coal-fired plant emission factor (t CO ₂ MWh ⁻¹)	0.945	0.945	0.945		0.945		0.945	0.945			0.945			0.945	0.945		0.945	0.945
Grid-mix emission factor (t CO ₂ MWh ⁻¹)	0.207	0.207	0.207				0.207	0.207						0.207	0.207		0.207	0.207
Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹)	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424		0.424		0.424	0.424	0.424	0.424	0.424

Calculation of capacity factor	1	Direct inp	ut of capa	acity factor
		Exp	Min	Max
Entered connects factor (9/)		25	24 E	20 E

Parameters		Slope (a)		Intercept (b)			
Partial power curves for different turbines	Exp	Min	Max	Exp	Min	Max	
User-defined	0.0	0.0	0.0	0.0	0.0	0.0	
Vestas 2.0 MW Optispeed C2	1392.5	1392.5	1392.5	-4291.9	-4291.9	-4291.9	

		Total		Fo	restry Are	ea 1	Fo	restry Are	a 2	For	restry Ar	ea 3	Fo	restry Are	ea 4	For	estry Ar	ea 5
Calculation of capacity factor from forestry management	Exp	Min	Max	Exp	Min	Max		Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Wind speed ratio calculated in 7d				#######	#######	#######	*******	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######
Average site windspeed (m s 1)	0	0	0		0			0	0		0		0	0	0			0
Annual theoretical energy output from turbine (MW turbine 1 yr 1)	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560
Power curve				User- defined	User- defined	User- defined	Partial power curves for different turbines											
(Power curve code)					1			0	0		0		o o	0	0			0
Slope (a) Intercept (b)				0 0	0 0	0	Exp Exp	Min Min	Max Max									
Annual power output from an individual turbine (MW turbine 1 yr 1)				#######	#######	#######		#######	######	#######	""""""	#######	**********	*********	**********	**********	######	#######
Calculated capacity factor (%)				#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	######	#######

		Total		Fo	restry Ar	ea 1	Fo	restry Are	ea 2	For	estry Are	a 3	Fo	restry Are	ea 4	For	restry Ar	a 5
Calculation of annual energy outp	ut from v	vind farm	1															
Direct input of capacity factor																		
Capacity factor(%)	35	32	39	35	32	39	35	32	39	35	32	39	35	32	39	35	32	39
Annual energy output from windfarm (MW yr ⁻¹)	147168	132451	161885		0	0	0	0	0	0	0	0	0	0	0	0	0	0

RESULTS		Total		Area 1		Area 2		Area 3		Area 4		Area 5	
Windfarm CO ₂ emission saving													
over													
coal-fired electricity	139074	125166	152981	0	0	0		0		0	0		
generation (tCO ₂ yr ⁻¹)	139074	125100	152561		٠			٠		٠			
grid-mix of electricity	20464	27417.4	22540.2										
generation (tCO ₂ yr ⁻¹)	30464	2/41/.4	33510.2		٠			٠		٠			
fossil fuel - mix of electricity	62399	56159.3	60620.2										
generation (tCO ₂ yr ⁻¹)	62399	56159.3	68639.2	U	U	U		U		U	U		

Click here to move to Payback Time Click here

Windfarm CO, emission saving

Note: The total emission savings are given by estimating the total possible electrical output of the windfarm multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from gifd)

Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine life with carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

Method used to estimate CO ₂ emissions	Calculate wrt installed
from turbine life (eg. manufacture,	capacity
construction, decommissioning)?	dapadity

	Exp	Min	Max
Direct input of emissions due to turbine life (t CO ₂ windfarm ⁻¹)	0	0	0
Calculation of emissions due to turbine I	ife from e	nergy ou	tput
CO ₂ emissions due to turbine life (tCO ₂ turbine ⁻¹)	5139	5139	5139
No. of turbines	8	8	8
Total calculated CO ₂ emission of the wind farm due to turbine life (t CO ₂ windfarm ⁻¹)	41108	41108	41108

		Total		Cons	truction A	rea 1	Cons	truction A	Area 2	Cons	truction A	Area 3	Cons	truction A	Area 4	Cons	truction A
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min
Calculation of emissions due to cement used in construction																	
Volume of cement used (m 3)	0	0	0		0		0	0	0			0	0	0	0	0	0
CO ₂ emission rate (t CO ₂ m ⁻³ cement)	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316
in annual content disease	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

in an anti-ordina	U	U	0
RESULTS			
Losses due to turbine life (eg.	41108	41108	41108
Additional CO ₂ payback time of windfarm	due to to	urbine life	e (eg.
manufacture, contruction, decomissioning	ng)		
coal-fired electricity generation (months)	4	4	3
grid-mix of electricity generation (months)	16	18	15
fossil fuel - mix of electricity generation (months)	8	9	7

Click here to move to Payback Time Click here

Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine life with carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

http://www.concretecentre.com/PDF/SCF_Table%207%20Embodied%20CO2_April%202013.pdf



Embodied carbon dioxide ($co_{2}e$) of concretes used in buildings

		cc	2e (kgCO2e/	m ³) ¹	CO2e (kgCO2e/tonne)1					
CONCRETE APPLICATION	Concrete designation	CEM I concret e	30% fly ash concrete	50% ggbs concrete	CEM I	30% fly ash concrete	50% ggbs concrete			
Blinding, mass fill, strip footings, mass foundations, trench foundations 2	GEN1	177	128	101	77	55	44			
Reinforced Foundations 2	RC25/30**	316	263	197	133	111	83			
Ground floors 2	RC28/35	316	261	186	134	110	79			
Structural: in situ floors, superstructure, walls, basements 2	RC32/40	369	313	231	154	131	96			
High strength concrete 2	RC40/50	432	351	269	178	146	111			
		c	Oze (kgCOze/	m³)	CO3	e (kgCO₂e/te	onne)			
Unreinforced Precast flooring ³			-			165				
Reinforced precast flooring ³						171				
Average Generic Concrete Block ⁴			-			84				

includes 30kg/m³ steel reinforcement
 includes 100kg/m³ steel reinforcement



Core input data

ENTER INPUT DATA HERE I VALUES SHOULD ONLY BE CHANGED ON THIS SHEET. DO NOT USE EXAMPLE VALUES AS DEFAULTSENTER YOUR OWN VALUES THAT ARE SPECIFIC TO YOUR PARTICULAR SITE.

Note: The input parameters include some variables that can be specified by default values, but others that must be site specific. Variables that can be taken from defaults are marked with purple tags on left hand side.

Click here to move to Payback Time

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Click here

	Expected values	Record	Pos	Record	ge of values	Record	Note: <u>Capacity factor</u> . The capacity factor of any power plant is the proportion of energy produ
Input data	Enter expected value here	source of data	Enter minimum value here	source of data	Enter maximum value here	source of data	Note: <u>capacity lactor</u> . The capacity ractor or any power praint is the proportion of netrepty production and uning a given period with respect to the energy that would have been produced had the farm been running continually and at maximum output (DECC (2004); see also www.bwea.com/reficapacityfactors.html). Capacity Factor = Electricity generated during the period [kWh]/ (Installed capacity [kW] x nur
Windfarm characteristics mensions	+		+		+		Capacity Factor — Electricity generated during the period [kWin] (installed capacity [kW] x hin hours in the period [h]) We recommend that a site-specific capacity factor site should be used (as measured during p stage), and should represent the <u>awerage</u> emission factor expected over the lifetime of the wir
o. of turbines etime of windfarm (years)	8 40	Ch 2 Ch 2	8 40	Ch 2 Ch 2	8 40	Ch 2 Ch 2	accounting for decline in efficiency with age (Hughes, 2012). The 5 year average capacity fact "load factor") for UK onshore wind between 2010 and 2014, based on average beginning and
formance wer rating of turbines (turbine capacity) (MW)	6	Ch 2	6	Ch 2	6	Ch2	year capacity, was 29.2% (DUKES, 2015).
pacity factor nter estimated capacity factor (percentage efficiency)	Direct input of capacity factc ▼ 35.0		Direct input of capacity facto ▼ 31.5		Direct input of capacity facto ▼ 38.5◆		Note: Extra capacity required for backup. If 20% of national electricity is generated by wind er the extra capacity required for backup is 5% of the rated capacity of the wind plant (Dale et al
kup ra capacity required for backup (%)	5		5		5 ←		We suggest this should be 5% of the actual output. If it is assumed that less than 20% of natic electricity is generated by wind energy, a lower percentage should be entered (0%). The Hous Lords Economic Affairs Committee report on The Economics of Renewable Energy (Parliame Business, 2008) notes that to cover peak demand a '20% margin of extra capacity has been stoned.
ditional emissions due to reduced thermal efficiency of the erve generation (%)	10		10		10		to keep the risk of a power cut due to insufficient generation at a very low level.' The estimate
rbon dioxide emissions from turbine life . manufacture, construction, decommissioning)	Calculate wrt installed capac ▼		Calculate wrt installed capac ▼		Calculate wrt installed capac ▼		provided by BERR was a range of 10% to 20% of installed capacity of wind energy. E.O.N is re as proposing that the capacity credit of wind power should be 8%, and The Renewable Energy Foundation proposed the use of the square root of the wind capacity (in GW) as conventional capacity (e.g. 36 GW of wind plant to match 6 GW of conventional plant).
, , , , , , , , , , , , , , , , , , ,					ų.		
Characteristics of peatland before windfarm development							Note: Extra emissions due to reduced thermal efficiency of the reserve power generation ≈ 10 (Dale et al 2004).
pe of peatland erage annual air temperature at site °C)	Acid bc ▼ 10.1	Ch 15	Acid bc ▼ 10.1	Ch 15	Acid bc ▼	Ch 15	Note: Emissions from turbine life, If total emissions for the windfarm are unknown, emissions be calculated according to turbine capacity. The normal range of CO ₂ emissions is 394 to 814 MW (White & Kulcinski, 2000: White, 2007).
erage depth of peat at site (m) Content of dry peat (% by weight)	0.34	PRSA	0.34 0	PRSA	0.34 0	PRSA	Note: Type of peatland. An 'acid bog' is fed primarily by rainwater and often inhabited by spha moss, thus making it acidic (Stoneman & Brooks, 1997).
erage extent of drainage around drainage features at site (m)	10.00		5.00		15.00	Ch 9	A fen' is a type of wetland fed by surface and/or groundwater (McBride et al., 2011).
erage water table depth at site (m) soil bulk density (g cm³) Characteristics of bog plants	5.00 0.00		0.10 0.00		10.00 0.00	Ch 9	Note: Time required for regeneration of previous habitat. Loss of fixation should be assumed to
ne required for regeneration of bog plants after restoration ars)	10		5		15 🕶		over lifetime of windfarm only. This time could be longer if plants do not regenerate. The requirements for after-use planning include the provision of suitable refugia for peat-forming
bon accumulation due to C fixation by bog plants in undrained tts (tC ha ⁻¹ yr ⁻¹)	0.25		0.12		0.31		vegetation, the removal of structures, or an assessment of the impact of leaving them in situ. Methods used to reinstate the site will affect the likely time for regeneration of the previous This time could also be shorter if plants regenerate during lifetime of windfarm. If so, enter nur years estimated for regeneration.
Forestry Plantation Characteristics thod used to calculate CO ₂ loss from forest felling	Enter simple data		Enter simple data ▼		Enter simple data ▼		Note: Carbon fixation by bog plants Apparent C accumulation rate in peatland is 0.12 to 0.31 t C har¹ yr¹ (Turunen et al., 2001; Bc
rea of forestry plantation to be felled (ha) verage rate of carbon sequestration in timber (tC ha-1 yr-1)	0 3.60	Ch 8	0 2.40	Ch 8	0 4.40	Ch-8	al., 1995). The SNH guidance uses a value of 0.25 t C ha ⁻¹ yr ⁻¹ .
Counterfactual emission factors update counterfactual emission factors from							Note: Area of forestry plantation to be felled. If the forestry was planned to be removed, with n further rotations planted, before the windfarm development, the area to be felled should be en
Click here (not yet operational)	0.045		0.045		0.045		as zero. Note: <u>Plantation carbon sequestration</u> . This is dependent on the yield class of the forestry. The
al-fired plant emission factor (t CQ MWh ⁻¹) d-mix emission factor (t CQ MWh ⁻¹)	0.945 0.207		0.945 0.207		0.945▼ 0.207▼		Note: <u>Plantation carbon sequestration</u> . This is dependent on the yield class of the forestry. The technical guidance assumed yield class of 16 m³ ha¹ yr¹, compared to the value of 14 m³ ha¹ provided by the Forestry Commission. Carbon sequestered for yield class 16 m³ ha¹ y² = 3.6 yr¹ (Cannell, 1999).
ssil fuel-mix emission factor (t CQ MWh ⁻¹) Borrow pits	0.424		0.424		0.424		Note: Coal-Fired Plant and Grid Mix Emission Factors. Coal-fired plant emission factor (EF) fre electricity supplied in 2014 = 0.093 t CO ₂ MWh ⁻¹ -Grid-Mix EF for 2014 = 0.394 t CO ₂ MWh ⁻¹ -Srid-Mi
nber of borrow pits rrage length of pits (m)	1 90.28	Ch 2	1 90.28	Ch 2	1 90.28	Ctr2	= DUKES, 2015b. Note: <u>Fossil Fuel-Mx Emission Factor</u> . The emission factor from electricity supplied in 2014 frossil fuels = 0.642 t CO ₂ MW ⁻ 1. Source = DUKES, 2015b.
rage width of pits (m) rage depth of peat removed from pit (m)	90.28 0.34	Ch 2 PRSA	90.28 0.34	Ch 2 PRSA	90.28 0.34	Ch 2 PRSA	Tossil fuels = 0.642 t CO ₂ MWh ⁻¹ . Source = DUKES, 2015b.
oundations and hard-standing area associated with each turbine							
nding	Rectangular with vertical wal		Rectangular with vertical wal ▼		Rectangular with vertical wal ▼		
erage length of turbine foundations (m) erage width of turbine foundations (m)	25.5 25.5	Ch 2 Ch 2	25.5 25.5	Ch 2 Ch 2	25.5 25.5	Ch 2 Ch 2	
erage depth of peat removed from turbine foundations (m) erage length of hard-standing (m)	0.30 80	Ch 2 Ch 2	0.10 75	Ch 2 Ch 2	0.50 85	Ch 2 Ch 2	
rrage width of hard-standing (m) rrage depth of peat removed from hard-standing (m)	68 0.34	Ch 2 PRSA	65 0.34	Ch 2 PRSA	70 0.34	Ch 2 PRSA	
Access tracks al length of access track (m)	5830 3790	Ch 2 Ch 2	5830 2700	Ch 2 Ch 2	5830 ←	Ch 2	Note: Total length of access track. If areas of access track overlap with hardstanding area, ex these from the total length of access track to avoid double counting of land area lost.
sting track length (m) gth of access track that is floating road (m)	0 0	Ch 2 Ch 2 Ch 2	3790 0 0	Ch 2 Ch 2 Ch 2	3790 0 0	Ch 2 Ch 2 Ch 2	
ating road width (m) ating road depth (m) gth of floating road that is drained (m)	0.00	Ch 2 Ch 2	0.00	Ch 2 Ch 2	0.00◀	Ch 2 Ch 2	Note: <u>Floating road depth.</u> Accounts for sinking of floating road. Should be entered as the ave depth of the road expected over the lifetime of the windfarm. If no sinking is expected, enter a
gth of industrial road trials is drained (m) gth of access track that is excavated road (m)	0.00 2040	Ch 2 Ch 2	0.00 2040	Ch 2 Ch 2	0.00 ←	Ch 2 Ch 2	Note: Length of floating road that is drained. Refers to any drains running along the length of road.
rage depth of peat excavated for road (m)	4.5 0.34	Ch 2 PRSA	4.5 0.34	Ch 2 PRSA	4.5 0.34	Ch 2 PRSA	Note: Rock filled roads. Rock filled roads are assumed to be roads where no peat has been r
gth of access track that is rock filled road (m) ck filled road width (m)	0		0		0 4		and rock has been placed on the surface and allowed to settle.
ck filled road depth (m) ngth of rock filled road that is drained (m)	0		0		0		
erage depth of drains associated with rock filled roads (m) Cable Trenches	0.00		0.00		0.00		
ngth of any cable trench on peat that does not follow access cks and is lined with a permeable medium (eg. sand) (m)	0		0		0		Note: Depth of peat cut for cable trenches, in shallow peats, the cable trenches may be cut by
erage depth of peat cut for cable trenches (m)	0.00		0.00		0.00◀		peat. To avoid overestimating the depth of peat affected by the cable trenches, only enter the of the peat that is cut.
dditional peat excavated (not already accounted for above)			•				
ume of additional peat excavated (n³) a of additional peat excavated (n²)	0 0.0		0 0.0		0 0.0		Note: Peat Landslide Hazard. It is assumed that measures have been taken to limit damage (Executive, 2006, Peat Landslide Hazard and Risk Assessments. Best Practice Guide for Proposed Electricity Generation Developments. Sootish Executive, Ectiviship, pp. 34-5) so that CI Cosses due to peat landslidle can be ass
Peat Landslide Hazard blink: Peat Landslide Hazard and Risk Assessments: Best	negligible	PRSA	negligible	PRSA	negligible	PRSA	be negligible. Link: http://www.scotland.gov.uk/Publications/2006/12/21162303/1.
ctice Guide for Proposed Electricity Generation Developments nprovement of C sequestration at site by blocking drains,	riegiigibie	TROA	riegiigibie	TROA	riegiigibie	TROA	
restoration of habitat etc							
ea of degraded bog to be improved (ha) ster table depth in degraded bog before improvement (m)		drains orains willingt		drains grains willing		drains orains willing*	
ster table depth in degraded bog after improvement (m)		will not		uill not		ton Ilius	Note: Period of time when improvement can be guaranteed. This guarantee should be absolu
		drains will not		drains will not		drains will not	Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the requirement for the improvement to become effective. For example if time required for hydroic
		have its drained		have its drained		have its drained	habitat to return to its previous state is 10 years and the restoration can be guaranteed over the of the windfarm (25 years), the period of time when the improvement can be guaranteed shou entered as 25 years, and the improvement will be effective for (25-10) = 15 years.
ne required for hydrology and habitat of bog to return to its evious state on improvement (years)	2	d so is	2	d so is	2	d so is	
		omitted from this		omitted from this		omitted from this	
		calculat		calculat		calculat ion	
		ion		ion		ion	
		drains will not		drains will not	•	drains will not	
		have its drained		have its		have its drained	
riod of time when effectiveness of the improvement in degraded	2	blocke d so is	2	blocke d so is	2	blocke d so is	
g can be guaranteed (years)		omitted from		omitted from		omitted from	
		this calculat		this calculat		this calculat	
		ion		ion		ion	
orovement of felled plantation land a of felled plantation to be improved (ha) ter table depth in felled gree before improvement (m)	0		0		0		
ter table depth in felled area before improvement (m) ter table depth in felled area after improvement (m) te required for hydrology and habitat of felled plantation to return	0.00 0.00		0.00 0.00		0.00 0.00		Note: Period of time when improvement can be guaranteed. This gurantee should be absolute
the required for hydrology and habitat of felled plantation to return its previous state on improvement (years) iod of time when effectiveness of the improvement in felled	2		2		2		Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absoluted Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the requirement for the improvement to become effective. For example if time required for hydrot.
tod of unle when enecuverless of the improvement in lened intation can be guaranteed (years) storation of peat removed from borrow pits	2		2		2 ←		requirement to the improvement to become effective. For example it may required for nyarow habitat to return to its previous state is 10 years and the restoration can be guaranteed over to fit the windfarm (25 years), the period of time when the improvement can be guaranteed shower than the provided for (25 full p. 15 years).
a of borrow pits to be restored (ha) oth of water table in borrow pit before restoration with respect to	8,150		8150		8150		30 20 yours, and the improvement will be effective for (25 -10) = 15 years.
restored surface (m) oth of water table in borrow pit after restoration with respect to	0.00		0.00		0.00		
restored surface (m) e required for hydrology and habitat of borrow pit to return to its	0.00		0.00		0.00		Note: <u>Period of time when improvement can be guaranteed</u> . This gurantee should be absolut Therefore, if you enter a value beyond the lifetime of the windfarm you should provide strong evidence that this improvement can be guaranteed for the full period given. This includes the
vious state on restoration (years) iod of time when effectiveness of the restoration of peat	2		2		2 ←		requirement for the improvement to become effective. For example if time required for hydrole habitat to return to its previous state is 10 years and the restoration can be guaranteed over the windfarm (25 years), the period of time when the improvement can be guaranteed shounds.
loved from borrow pits can be guaranteed (years) ly removal of drainage from foundations and hardstanding							of the windrarm (25 years), the period of time when the improvement can be guaranteed shot entered as 25 years, and the improvement will be effective for (25 -10) = 15 years.
ter table depth around foundations and hardstanding before toration (m) ter table depth around foundations and hardstanding after	0.00		0.00		0.00		Note: Period of time when improvement can be guaranteed. This is assumed to be the lifetime
ter table depth around foundations and hardstanding after loration (m) let to completion of backfilling, removal of any surface drains, and	0.00		0.00		0.00		windfarm as restoration after windfarm decommissioning is already accounted for in restoration site
ne to completion of backfilling, removal of any surface drains, and restoration of the hydrology (years) Restoration of site after decomissioning	0		0		0		Note: Restoration of site. If the water table at the site is returned to its original level or higher decommissioning, and habitat at the site is restored, it is assumed that C losses continue only
I the hydrology of the site be restored on decommissioning?	Yés		Yes		Yes		decommissioning, and habitat at the site is resolved, it is assumed that C losses comme on lifetime of the windfarm. Otherwise, C losses from drained peat are assumed to be 100%.
I you attempt to block any gullies that have formed due to the	Not applic ▼		Not applic ▼		Not applic ▼		-
ndfarm?	Not applic ▼ Yes		Not applic ▼ Yes		Not applic ▼ Yes		
dfarm? I you attempt to block all artificial ditches and facilitate rewetting? I the habitat of the site be restored on decommissioning?			.03		Not appli ▼		
l you attempt to block all artificial ditches and facilitate rewetting?	Not applic ▼		Not appl ▼				
you attempt to block all artificial ditches and facilitate rewetting? the habitat of the site be restored on decommissioning?	_		Not applic ▼		Not applic ▼		Note: Choice of methodology for calculating emission factors. The IPCC default methodology
you attempt to block all artificial ditches and facilitate rewetting? the habitat of the site be restored on decommissioning? you control grazing on degraded areas? you manage areas to favour reintroduction of species	Not applic ▼			<u> </u>			Note: Choice of methodology for calculating emission factors. The IPCC default methodology internationally accepted standard (IPCC, 1997). However, it is stated in IPCC (1997) that their loopin estimates, and "these rates and production periods can be used if countries do not have considered to the control of the contro

Forestry input data
ENTER DETAILS OF FORE
Note: Data only needed if se
(1) for estimating compensa

http://tinyurl.com/woodlandcarboncode http://tinyurl.com/FCPolicy http://tinyurl.com/FCScotlandCompPlant

No POC losses for bare soil included yet. If extensive areas of base soil is present at site need

Click here to move to Payback Time
Click here to return to Instructions
Click here



Note: <u>Estimated downtime</u>. <u>Estimated downtime</u> for maintenance etc. Few reports on downtime wind furbines are publically available. However, one relieve by Garad Hassan (2011) suggested the minimum downtime reported was 2% for the animum downing average for between 0 to 9 years operation of new furbines, for a sample of 240 turbines. For a summary of findings see Garad Hassan (2011). Possible range of values Expected values Enter expected value here Enter minimum value here Enter maximum value here In felling and timber removal.

In felling and timber removal.

In factors from UK taken from Morison et al (2011), if clearfelling assumed to be a consistent of the constant Note: Emissis Windfarm characteristics Location
Distance to nearest biofuel plant (km) Note: Emissions associated with transportation.
Assuming trasportation by trucks running on diesel and 20% of journey taken on forest roads, emissions factor obtained from Morison et al (2011) is 39:33 g CO₂ km⁻¹ t⁻¹ (range 38.5 – 40.15 g Distance to mean.
Dimensions
Total wind farm area (ha)
Performance
Height of turbines (m) .., need (m €¹) Average site winds Estimated downtime for maintenance etc (%)

Emissions due to forestry op

Emissions from felling (g CO₂ m⁻³) Emissions of CO₂ associated with transportation (g CO₂ km⁻¹ f⁻¹) Forestry Plantation Characteristics
Note - total number of turbines already spr
Number of turbines in this area
Power curve - NOT USED!
(In CORE INPUT DATA sheet you have selected
to input capacity factor directly. No need to select!)
Mails soil sub-more. Note: Power curve
Based on Vestas 2.0MW Optispeed turbine with roughness class C2, modelled over wind speed
5-10 ms⁻¹. To define a the power curve for a different turbine type, plot annual power output, P
(MWh) against annual windspeed, V(m s⁻¹) and fit a linear regression to obtain slope, a, and ₹ ٠l ۰I P = aW + b Deep Peat ▼
Scots pine ▼ Scots pine
No
V ₹ ₹ ajor soil sub-group Note: Soil sub-group
Used in determination of forestry characteristic.
Peatly gley = Peatly Soils (5-50cm) e.g. peatly gley, peatly podso
Deep peat = Deep Peat (>50cm) e.g. basin and blanket bogs No ▼ Species
Felled Forest Blomass used as biofuel?
Felling regime
Age of forestry when felled for windfarm (yr)
Area felled around each turbine (ha)
Width of forest around felled area (m)
Value of felled forestry as a biomass fuel (MWh t*)
(Carbon: Blomass) ratio of felled forestry
Replanting regime
Vears after felling when replanting occurs
Age of seedings on planting (yr)
Area replanted around each turbine (ha) No ▼ Note: Species So far only Scots pine and Sitka spruce included. ete: Value of felled forestry Values available in Max Note: Carbon: Riomass zatio of feliat forests; Wood biomass can be converted to dry wishing wood density based values from Lavers (1983) with a subsequent assumption; and with a subsequent assumption; and with the subsequent assumption; and with the subsequent assumption; and with the subsequent assumption of the subsequent assumption; and with the subsequent assumption of the subsequent as subsequ umber of turbines in this area
ower curve - NOT USED!
(In CORE INPUT DATA sheet you have selected
to input capacity factor directly. No need to select!) ₹ ₹ ₹ v v Ī ▼ _____**-**___ Felled Forest Biomass used as biofuel? Felling regime Felling regime
Age of forestry when felled for windfarm (yr)
Area felled around each turbine (ha)
Width of forest around felled area (m)
Value of felled forestry as a biomass fuel (MWh f¹) Value of felled forestry as a biomass fuel (M (Carbon, Elkomass) ratio of felled forestry. Seplanting regime Years after felling when replanting occurs Age of seedlings on planting (yr) Area replanted around each turbine (ha) IEA 3 umber of turbines in this area ower curve - NOT USED! (In CORE INPUT DATA sheet you have selected • • to input capacity factor directly. No need to select!) ▼ ₹ Major soil sub-group Species ₹ Felled Forest Biomass used as biofuel?

Felling regime
Age of forestry when felled for windfarm (yr)
Area felled around each turbine (ha)

Width of forest around felled area (m) Width of forest around felled area (m)
Value of felled foresty as a biomass fuel (MWh t¹)
(Carbon : Biomass) ratio of felled forestry
Replanting region
Years after felling when replanting occurs
Age of seedlings on planting (vpc)
Area replanted around each turbine (ha) #A4
mber of turbines in this area
wer curve - NOT USED!
(In CORE INPUT DATA sheet you have selected
to input capacity factor directly. No need to select!) • • ▼ ▼ ╗ v Major soil sub-group elled Forest Biomass used as biofuel? Felled Forest Blomass used as blotlue?

Ellina neame
Age of forestry when felled for windfarm (yr)
Arare felled around each turbine (ha)
Width of forest around felled area (m)
Value of felled forestry as a biomass fuel (MWh f.³)
(Carbon. Biomass) ratio of felled forestry

Ellina felled forestry

Vests after felling when replanting occurs
Age of seedings on planting (yr)
Area replanted around each turbine (ha) REA.5
umber of turbines in this area
ower curve - NOT USED!
(In CORE INPUT DATA sheet you have selected
to input capacity factor directly. No need to selec **▼** ₹ **-**Ţ v ∙ Major soil sub-group Felled Forest Biomass used as biofuel?
Felling regime
Age of forestry when felled for windfarm (yr) Age of forestry when felled for windfarm (ry)
Area felled around each turbine (ha)
Width of forest around felled area (m)
Value of felled forestry as a biomass fuel (MWh f*)
(Cathor; Biomass) ratio of felled forestry
(Cathor; Biomass) ratio of felled forestry
(Cathor; Biomass) ratio of felled forestry

Years after felling when replanting occurs
Age of seedings on planting (ry)

Area replanted around each turbine (ha)

Forestry input data

ENTER DETAILS OF FORESTRY MANAGEMENT HERE!

Note: Data only needed if select to calculate capacity factor?

Click here to move to Payback Time Click here Click here to return to Instructions

Construction input data

ENTER DETAILS OF CONSTRUCTION HERE!

Note: This data only used in the calculation if the selection "Enter detailed information" is made in cell C50 of the Core input data sheet.

Click here to move to Payback Time
Click here to return to Core input data

Click here
Click here

	Expected values	Possible rang	e of values
	Recor		Record
Input data	Enter expected value here source	Enter minimum value here source	Enter maximum value here source
	of data	of data	of data
Construction design Note - total number of turbines already specified:	8	8	8
AREA 1 Number of turbines in this area	8 Ch 2	8 Ch 2	8 Ch-2
<u>Turbine foundations</u>		, July	
Average depth of peat removed when constructing foundations (m) Approximate geometric shape of whole dug when constructing	Rectangular 🔻	Rectangular 🔻	Rectangular ▼
foundations	Rectangular	Rectangular 🔻	Rectangular 🔻
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Hardstanding			
Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing	Rectangular	Rectangular	Rectangular
hardstanding Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
Piling	No ▼	No ▼	No ▼
Is piling used? Volume of Concrete	NO 1	100 -	NO .
Volume of concrete used (m³)			
AREA 2			
Number of turbines in this area			
Turbine foundations Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing	▼	▼	▼
foundations Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
<u>Hardstanding</u>			
Average depth of peat removed when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing	▼	▼	·
hardstanding	, T	The second secon	, , , , , , , , , , , , , , , , , , ,
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Piling			
Is piling used?	<u> </u>		
Volume of Concrete			
Volume of concrete used (m³)			
AREA 3			
Number of turbines in this area Turbine foundations			
Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing foundations	▼	-	▼
Length at surface (m)			
Width at surface (m) Length at bottom (m)			
Width at bottom (m)			
Hardstanding Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing	▼	▼	▼
hardstanding Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
Piling	_		_
Is piling used? Volume of Concrete			
Volume of concrete used (m³)			
ARFA 4			
Number of turbines in this area			
Turbine foundations Average depth of peat removed when constructing foundations (m)			
Approximate geometric shape of whole dug when constructing	7	▼	₹
foundations Length at surface (m)			
Width at surface (m)			
Length at bottom (m) Width at bottom (m)			
<u>Hardstanding</u>			
Average depth of peat removed when constructing hardstanding (m) Approximate geometric shape of whole dug when constructing	▼	▼	Ţ
hardstanding		1	
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m)			
Is piling used?			
Volume of Concrete Volume of concrete used (m³)			
AREA 5 Number of turbines in this area			
Turbine foundations			
Average depth of peat removed when constructing foundations (m) Approximate geometric shape of whole dug when constructing	▼	▼	
foundations			
Length at surface (m) Width at surface (m)			
Length at bottom (m)			
Width at bottom (m) Hardstanding			
Average depth of peat removed when constructing hardstanding (m)			
Approximate geometric shape of whole dug when constructing hardstanding			
Length at surface (m)			
Width at surface (m) Length at bottom (m)			
Width at bottom (m)			
Piling Is piling used?	▼	-	▼
Volume of Concrete			
Volume of concrete used (m ³)			

Results PAYBACK TIME AND CO₂ EMISSIONS

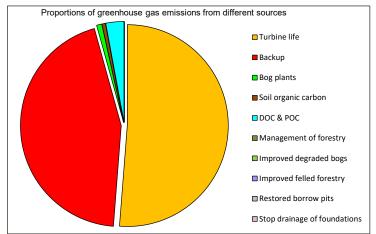
Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

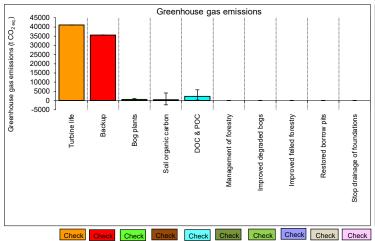
Click here to return to Input data Click here to return to Instructions

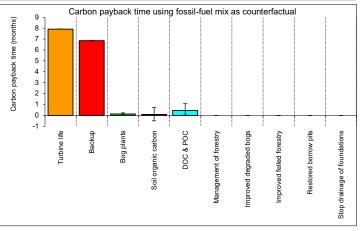


	Ехр.	Min.	Мах.
1. Windfarm CO ₂ emission saving over			
coal-fired electricity generation (tCO ₂ yr ⁻¹)	139074	125166	152981
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	30464	27417	33510
fossil fuel - mix of electricity generation (tCO ₂ yr ⁻¹)	62399	56159	68639
Energy output from windfarm over lifetime (MWh)	5886720	5298048	6475392
Total CO ₂ losses due to wind farm (t CO ₂ eq.)			
Losses due to turbine life (eg. manufacture, construction, decomissioning)	41108	41108	41108
3. Losses due to backup	35657	35657	35657
4. Losses due to reduced carbon fixing potential	669	198	1215
5. Losses from soil organic matter	460	-2298	4124
6. Losses due to DOC & POC leaching	2330	326	5861
7. Losses due to felling forestry	0	0	0
Total losses of carbon dioxide	80224	74991	87965
8. Total CO ₂ gains due to improvement of site (t CO ₂ eq.)			
8a. Change in emissions due to improvement of degraded bogs	0	0	0
8b. Change in emissions due to improvement of felled forestry	0	0	0
8c. Change in emissions due to restoration of peat from borrow pits	0	0	0
8d. Change in emissions due to removal of drainage from foundations & hardstanding	0	0	0
Total change in emissions due to improvements	0	0	0

Total change in emissions due to improvements	0	0	0
RESULTS			
	Ехр.	Min.	Max.
Net emissions of carbon dioxide (t CO _{2 eq} .)			
	80224	74991	87965
Carbon Payback Time			
coal-fired electricity generation (years)	0.6	0.5	0.7
grid-mix of electricity generation (years)	2.6	2.2	3.2
fossil fuel - mix of electricity generation (years)	1.3	1.1	1.6
Ratio of soil carbon loss to gain by restoration (TARGET ratio (Natural Resources Wales) < 1.0)	No gains!	No gains!	No gains!
Ratio of CO ₂ eq. emissions to power generation (g / kWh) (TARGET ratio by 2030 (electricity generation) < 50 g /kWh)	14	12	17







Results PAYBACK TIME AND CO₂ EMISSIONS

Note: The carbon payback time of the windfarm is calculated by comparing the loss of C from the site due to windfarm development with the carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

Click here to return to Input data Click here to return to Instructions



Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greennouse gas emissions			
	Ехр.	Min	Max
Turbine life	41108	0	0
Backup	35657	0	0
Bog plants	669	471	546
Soil organic carbon	460	2758	3665
DOC & POC	2330	2004	3531
Management of forestry	0	0	0
Improved degraded bogs	0	0	0
Improved felled forestry	0	0	0
Restored borrow pits	0	0	0
Stop drainage of foundations	0	0	0

Data used in barchart of carbon payback time using fossil-fuel mix as counterfactual

Greenhouse gas emissions Carbon payback time (months) Exp. Min Мах. Exp. Min Мах. Turbine life 41108 0 0 0 0 Backup 35657 Bog plants 669 471 546 0 460 2758 3665 Soil organic carbon DOC & POC 2330 2004 3531 Management of forestry Improved degraded bogs Improved felled forestry Restored borrow pits Stop drainage of foundations 80224

Windfarm CO₂ emission saving

Note: The total emission savings are given by estimating the total possible electrical output of the windfarm multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from grid)

Click here to move to Payback Time Click here

		Total		Fo	restry Are	a 1	Fo	restry Are	a 2	For	estry Are	еа 3	Fo	restry Are	ea 4	For	restry Ar	ea 5
Values taken from input sheet	Exp	Min	Max	Exp	Min	Max	Exp	Min		Exp	Min	Max		Min	Max	Exp	Min	Max
Power Generation Characteristics		•	•															
No. of turbines	8	8	8				0	0						0	0		0	0
Power rating of turbines (turbine capacity) (MW)	6	6	6				6	6						6	6		6	6
Power of windfarm (MW)	48	48	48				0	0						0	0		0	0
Estimated downtime for maintenance etc (%)	0	0	0	0	0	0	0	0	0	0		0	0	0	0	0	0	0
Counterfactual emission factors																		
Coal-fired plant emission factor (t CO ₂ MWh ⁻¹)	0.945	0.945	0.945		0.945		0.945	0.945			0.945			0.945	0.945		0.945	0.945
Grid-mix emission factor (t CO ₂ MWh ⁻¹)	0.207	0.207	0.207				0.207	0.207						0.207	0.207		0.207	0.207
Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹)	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424		0.424		0.424	0.424	0.424	0.424	0.424

Calculation of capacity factor	1	Direct inp	ut of capa	acity factor
		Exp	Min	Max
Entered connects factor (9/)		25	24 E	20 E

Parameters		Slope (a)			Intercept (b)	
Partial power curves for different turbines	Exp	Min	Max	Exp	Min	Max
User-defined	0.0	0.0	0.0	0.0	0.0	0.0
Vestas 2.0 MW Optispeed C2	1392.5	1392.5	1392.5	-4291.9	-4291.9	-4291.9

		Total		Fo	restry Are	ea 1	Fo	restry Are	a 2	For	restry Ar	ea 3	Fo	restry Are	ea 4	For	estry Ar	ea 5
Calculation of capacity factor from forestry management	Exp	Min	Max	Exp	Min	Max		Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Wind speed ratio calculated in 7d				#######	#######	#######	*******	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######
Average site windspeed (m s 1)	0	0	0		0			0	0		0		0	0	0			0
Annual theoretical energy output from turbine (MW turbine 1 yr 1)	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560	52560
Power curve				User- defined	User- defined	User- defined	Partial power curves for different turbines											
(Power curve code)					1			0	0		0		o o	0	0			0
Slope (a) Intercept (b)				0 0	0	0	Exp Exp	Min Min	Max Max									
Annual power output from an individual turbine (MW turbine 1 yr 1)				#######	#######	#######		#######	######	#######	""""""	#######	**********	*********	**********	**********	######	#######
Calculated capacity factor (%)				#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	#######	######	#######

		Total		Fo	restry Ar	ea 1	Fo	restry Are	ea 2	For	estry Are	a 3	Fo	restry Are	ea 4	For	restry Ar	a 5
Calculation of annual energy outp	ut from v	vind farm	1															
Direct input of capacity factor																		
Capacity factor(%)	35	32	39	35	32	39	35	32	39	35	32	39	35	32	39	35	32	39
Annual energy output from windfarm (MW yr ⁻¹)	147168	132451	161885		0	0	0	0	0	0	0	0	0	0	0	0	0	0

RESULTS		Total		Area 1		Area 2		Area 3		Area 4		Area 5	
Windfarm CO ₂ emission saving													
over													
coal-fired electricity	139074	125166	152981	0	0	0		0		0	0		
generation (tCO ₂ yr ⁻¹)	139074	125100	152561		۰	۰		٠		٠			
grid-mix of electricity	20464	27417.4	22540.2										
generation (tCO ₂ yr ⁻¹)	30464	2/41/.4	33510.2		۰	۰		٠		٠			
fossil fuel - mix of electricity	62399	56159.3	60620.2										
generation (tCO ₂ yr ⁻¹)	62399	56159.3	68639.2	U	U	U		U		U	U		

Click here to move to Payback Time Click here

Windfarm CO, emission saving

Note: The total emission savings are given by estimating the total possible electrical output of the windfarm multiplied by the emission factor for the counterfactual case (coal-fire generation and electricity from gifd)

Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine I with carbon-savings achieved by the windfarm while displacing electricity generated fro coal-fired capacity or grid-mix.

Method used to estimate CO ₂ emissions	Calculate wrt installed
from turbine life (eg. manufacture,	capacity
construction, decommissioning)	oupdoity

	Exp	Min	Max
Direct input of emissions due to turbine life (t CO ₂ windfarm ⁻¹)	0	0	0
Calculation of emissions due to turbine	life from	energy o	utput
CO ₂ emissions due to turbine life (tCQ turbine ⁻¹)	5139	5139	5139
No. of turbines	8	8	8
Total calculated CO ₂ emission of the wind farm due to turbine life (t CO ₂ windfarm ⁻¹)	41108	41108	41108

		Total Construction Area 1 Construction Area 2 Construction Area 3			Cons	Construction Area 3 Construction				Area 4 Construction Area 5								
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Calculation of emissions due to cement used in construction																		
Volume of cement used (m3)	0	0	0		0	0	0	0	0	0			0	0	0	0		0
CO ₂ emission rate (t CO ₂ m ⁻³ cement)	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316	0.316
Total CO2 emissions due to cement used in	0	0	0		0	0	0	0	0	0			0	0	0	0		0

to-stien	U	U	U
RESULTS			
Losses due to turbine life (eg.	41108	41108	41108
Additional CO ₂ payback time of windfare	n due to t	turbine lit	fe (eg.
manufacture, contruction, decomission	ing)		
coal-fired electricity generation (months)	4	4	3
grid-mix of electricity generation (months)	16	18	15
fossil fuel - mix of electricity generation (months)	8	9	7

Click here to move to Payback Time Click here

Emissions due to turbine life

Note: The carbon payback time of the windfarm due to turbine life (eg. manufacture, construction, decomissioning) is calculated by comparing the emissions due to turbine life with carbon-savings achieved by the windfarm while displacing electricity generated from coal-fired capacity or grid-mix.

http://www.concretecentre.com/PDF/SCF_Table%207%20Embodied%20CO2_April%202013.pdf



Embodied carbon dioxide ($co_{z^{\Phi}}$) of concretes used in buildings

		CC	Dze (kgCOze/	m ³) ¹	CO2e (kgCO2e/tonne)1			
CONCRETE APPLICATION	Concrete designation	CEM I concret e	30% fly ash concrete	50% ggbs concrete	CEM I concrete	30% fly ash concrete	50% ggbs concrete	
Blinding, mass fill, strip footings, mass foundations, trench foundations ²	GEN1	177	128	101	77	55	44	
Reinforced Foundations ²	RC25/30**	316	263	197	133	111	83	
Ground floors 2	RC28/35	316	261	186	134	110	79	
Structural: in situ floors, superstructure, walls, basements 2	RC32/40	369	313	231	154	131	96	
High strength concrete 2	RC40/50	432	351	269	178	146	111	
		CO₂e (kgCO₂e/m³)		m²)	CO24	e (kgCO₂e/to	onne)	
Unreinforced Precast flooring ³		-				165		
Reinforced precast flooring ³		-				171		
Average Generic Concrete Block ⁴		-				84		

includes 30kg/m³ steel reinforcement includes 100kg/m³ steel reinforcement

Emissions due to backup power generation

Note: CO₂ loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

	Expected	Minimum	Maximum
Reserve capacity required for backup			
No. of turbines	8	8	8
Power rating of turbines (turbine capacity) (MW)	6	6	6
Power of wind farm (MW h ⁻¹)	48	48	48
Rated capacity (MW yr ⁻¹)	420480	420480	420480
Extra capacity required for backup (%)	5	5	5
Additional emissions due to reduced thermal efficiency of the reserve generation (%)	10	10	10
Reserve capacity (MWh yr ¹)	2102	2102	2102
Carbon dioxide emissions due to backup power generation			
Coal-fired plant emission factor (t CQ MWh ⁻¹)	0.945	0.945	0.945
Grid-mix emission factor (t CO ₂ MWh ⁻¹)	0.207	0.207	0.207
Fossil fuel- mix emission factor (t CO ₂ MWh ⁻¹)	0.424	0.424	0.424
Lifetime of windfarm (years)	40	40	40
Annual emissions due to backup from			
coal-fired electricity generation (tCQ ₂ yr ⁻¹)	1987	1987	1987
grid-mix of electricity generation (tCO ₂ yr ⁻¹)	435	435	435
fossil fuel - mix of electricity generation (tCQ yr ⁻¹)	891	891	891

Note. Wind generated denticity is inherently variable a modeling unique shallenges to the electricity pre-moting shallenges for provision of a supply to meet consumer demand (Next, 2004). Backap power is required to accompany wind generation to stabilish the supply to the consumer. This backap power will sussill be obtained from a focal state source, At a high level of wind power posentiation in the owned generating man, and with current grid state source, At a high level of wind power power power will sussill be obtained from a focal state to the control of the state of

RESULTS			
Total emissions due to backup from			
coal-fired electricity generation (tCQ)	79471	79471	79471
grid-mix of electricity generation (tCO ₂)	17408	17408	17408
fossil fuel - mix of electricity generation (tCQ)	35657	35657	35657
Additional CC ₂ payback time of windfarm due to backup			
coal-fired electricity generation (months	7	8	6
grid-mix of electricity generation (months)	7		
fossil fuel - mix of electricity generation (months	7	8	6

Emissions due to backup power generation

Note: CO₂ loss due to back up is calculated from the extra capacity required for backup of the windfarm given in the input data.

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

	Expected	Minimum	Maximum
Area where carbon accumulation by bog plants is lost			
Total area of land lost due to windfarm construction (m ²)	66052	61532	70132
Total area affected by drainage due to windfarm construction (m ⁻²)	79851	38386	124157
Total area where fixation by plants is lost (m ²)	145904	99918	194289
Total loss of carbon accumulation			
Carbon accumulation in undrained peats (tC ha ⁻¹ yr ⁻¹)	0.25	0.12	0.31
Lifetime of windfarm (years)	40	40	40
Time required for regeneration of bog plants after restoration (years)	10	5	15
Carbon accumulation up to time of restoration (tCO ₂ eq. ha ⁻¹)	46	20	63
RESULTS			
Total loss of carbon accumulation by bog plants			
Total area where fixation by plants is lost (ha)	15	10	19
Carbon accumulation over lifetime of windfarm (tCO 2 eq. ha ⁻¹)	46	20	63
Total loss of carbon fixation by plants at the site (t CO ₂)	669	198	1215
Additional CO ₂ payback time of windfarm due to loss of CO2 fixing	g potential		
coal-fired electricity generation (months)	0	0	0
grid-mix of electricity generation (months)	0	0	0
fossil fuel - mix of electricity generation (months)	0	0	0

Assumptions:

1. Bog plants are 100% lost from the area where peat is removed for construction.

2. Bog plants are 100% lost from the area where peat is drained.

3. The recovery of carbon accumulation by plants on restoration of land is as given in inputs.

Click here to move to Payback Time Click here

Emissions due to loss of bog plants

Note: Annual C fixation by the site is calculated by multiplying area of the windfarm by the annual C accumulation due to bog plant fixation

Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO 2 loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

	Expected result	Minimum result	Maximum result
CO ₂ loss due to windfarm construction			
CO ₂ loss from removed peat (t CO ₂ equiv)	-6154	-5160	-7188
CO ₂ loss from drained peat (t CO ₂ equiv)	6614	2861	11312
RESULTS			
Total CO ₂ loss from peat (removed + drained) (t CO ₂ equiv)	460	-2298	4124
Additional CO ₂ payback time of windfarm due to loss of soil CO ₂			
coal-fired electricity generation (months)	0		0
grid-mix of electricity generation (months)	0		1
fossil fuel - mix of electricity generation (months)	0	0	1

Click here to move to Payback Time Click here

Emissions due to loss of soil organic carbon

Note: Loss of C stored in peatland is estimated from % site lost by peat removal (sheet 5a), CO 2 loss from removed peat (sheet 5b), % site affected by drainage (sheet 5c), and the CO2 loss from drained peat (sheet 5d).

Volume of Peat Removed

Note: *site lost by peat removal is estimated from peat
removed in borrow pits, buther foundations, hard-standing and access tracks.

If peat is removed for any other reason, this must be
added in as additional peat excavated in the core input
sheet.

Peat removed from borrow pits	Total						
reat removed from borrow pits	Exp	Min	Max				
Number of borrow pits	1	1	1				
Average length of pits (m)	90.28	90.28	90.28				
Average width of pits (m)	90.28	90.28	90.28				
Average depth of peat removed from pit (m)	0.34	0.34	0.34				
Area of land lost in borrow pits (m ²) Volume of peat removed from borrow pits	8150.48	8150.48	8150.48				
(m ³)	2771.16	2771.16	2771.16				

Peat removed from turbine foundations		Total		Cons	truction /	Area 1	Cons	truction /	rea 2	Cons	truction A	Area 3	Cons	truction	Area 4	Cons	truction.	Area 5
reat removed from turbine foundations	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
Method used to calculate CO ₂ loss from	Rectangu	ılar with v	ertical															
foundations	walls																	
Calculation method code		1																
No. of turbines	8	8	8	8				0	0	0			0	0	0		0	0
Length at surface (m)				26	26	26		0	0	0			0	0	0		0	0
Width at surface (m)				26	26	26		0	0	0			0	0	0		0	0
Length at bottom (m)				26	26	26		0	0	0			0	0	0		0	0
Width at bottom (m)				26	26	26		0	0	0			0	0	0		0	0
Depth of foundations (m)				0	0		0	0	0	0	0	0	0	0	0	0	0	0
"Area" of land lost in hard-standing (m 2)	5202	5202	5202	5202	5202	5202		0	0	0			0	0	0		0	0
Volume of peat removed from foundation	1560.6	520.2	2601	1560.6	520.2	2601		0	0	0			0	0	0		0	0
area (m³)	1000.6	520.2	2601	1500.0	520.2	2001	U	U	U	U	U	U	U	U	U	U	U	U
Peat removed from hard-standing			I															
Method used to calculate CO ₂ loss from	Rectangu	ılar with v	ertical															
foundations	walls		or trous															
Calculation method code		1																
No. of turbines	8	l 8	8	8	8	8		0	0	0	0	0	0	0	0	0	0	0
Length at surface (m)	- J			80	75	85		Ô	0	Ô	0	0	0	ő	ő	Ô	0	ő
Width at surface (m)				68	65	70		ő	Ô	Ô	ő	ő	ő	ő	ő	ő	ő	ő
Length at bottom (m)				80	75	85		ō	ō	ō	ō	ō	ō	ō	ō	ō	ō	ō
Width at bottom (m)				68	65	70		ō	ō	ō	ō	ō	ō	ō	ō	ō	0	0
Depth of hardstanding (m)				0	0.34	0.34		ō	ō	ō	ō	ō	ō	ō	ō	ō	ō	ō
Area of land lost in hard-standing (m 2)	43520	39000	47600	43520	39000	47600	0	0	0	0	0	0	0	0	0	0	0	0
Volume of peat removed from																		
hardstandingarea (m³)	14796.8	13260	16184	14796.8	13260	16184		0	0	0	0	0	0	0	0	0	0	0

Peat removed from access tracks		Total	
Peat removed from access tracks	Exp	Min	Max
Floating roads			
Length of access track that is floating road			
(m)	0	0	0
Floating road width (m)	0	0	0
Floating road depth (m)	0	0	0
Area of land lost in floating roads (m 2)	0	0	0
Volume of peat removed for floating roads	0	0	0
Excavated roads			
Length of access track that is excavated			
road (m)	2040	2040	2040
Excavated road width (m)	4.5	4.5	4.5
Average depth of peat excavated for road			
(m)	0.34	0.34	0.34
Area of land lost in excavated roads (m ²)	9180	9180	9180
Volume of peat removed for excavated			
roads	3121.2	3121.2	3121.
Rock-filled roads			
Length of access track that is rock filled road			
(m)	0	0	0
Rock filled road width (m)	0	0	0
Rock filled road depth (m)	0	0	0
Area of land lost in excavated roads (m ²)	0	0	0
Volume of peat removed for rock-filled roads	0	0	0
Total area of land lost in access tracks (m ²) Total volume of peat removed due to access	9180	9180	9180
tracks (m ³)	3121.2	3121.2	3121.
Additional peat excavated -		ı	
(not already accounted for above)			
Volume of additional peat excavated (m 3)	0	0	0
	-	_	_
Area of additional peat excavated (m 2)	0	0	0

RESULTS		Total	
	Exp	Min	Max
Total volume of peat removed (m³) due to windfarm construction Total area of land lost due to windfarm	22249.8	19672.6	24677.4
construction (m ²)	66052	61532.5	70132.5

Click here to move to 5b. CO2 loss from removed peat

Click here to move to Payback Time

Click here

Volume of Peat Removed

Note: % site lost by peat removal is estimated from peat removed in borrow pits, turbine foundations, hard-standing and access tracks.

If peat is removed for any other reason, this must be added in to the volume of peat removed, area of land lost and % site lost at the bottom of this worksheet.

CO₂ loss from removed peats

CO₂ loss from removed peat

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

Expected

Minimum

Maximum

C Content of dry peat (% by weight)	0	0	0
Dry soil bulk density (g cm ³)	0.00	0.00	0.00
% C contained in removed peat that is lost as CO ₂	100	100	100 ◀
Total volume of peat removed (m³) due to windfarm construction	22250	19673	24677
CO ₂ loss from removed peat (t CO ₂)	0	0	0
	1	1	1
CO ₂ loss from undrained peat left in situ			
Total area of land lost due to windfarm construction (ha)	7	6	7
CO ₂ loss from undrained peat left in situ (t CO ₂ ha ⁻¹)	932	839	1025
CO ₂ loss from undrained peat left in situ (t CO ₂)	6154	5160	7188
CO ₂ loss attributable to peat removal only	1	1	
CO ₂ loss from removed peat (t CO ₂)	0	0	0
CO ₂ loss from undrained peat left in situ (t CO ₂)	6154	5160	7188
RESULTS			
CO ₂ loss attributable to peat removal only (t CO ₂)	-6154	-5160	-7188

Click here to move to 5. Loss of soil ${\rm CO_2}$

Click here to move to Payback Time

Click here

CO₂ loss from removed peats

Note: If peat is treated in such a way that it is permanently restored, so that less than 100% of the C is lost to the atmosphere, a lower percentage can be entered in cell C10

Assumption: If peat is not restored, 100% of the carbon contained in the removed peat is lost as CO₂

Volume of peat drained

Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

Extent of drainage around each metre	Total					
of drainage ditch	Exp	Min	Max			
Average extent of drainage around	10	5	15			

Peat affected by drainage around	Total						
borrow pits	Exp	Min	Max				
Number of borrow pits	1	1	1				
Average length of pits (m)	90	90	90				
Average width of pits (m)	90	90	90				
Average depth of peat removed from pit (m)	0.3	0.3	0.3				
Area affected by drainage per borrow pit (m ²)	4011	1906	6317				
Total area affected by drainage around borrowpits (m²)	4011	1906	6317				
Total volume affected by drainage	682	324	1074				

Peat affected by drainage around		Total		Cons	truction	Area 1	Cons	truction	Area 2	Cons	truction	Area 3	Construction Area 4			Construction Area 5		
turbine foundation and hardstanding	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max
No. of turbines	8	8	8	8	8	8	0	0	0	0	0	0	0	0	0	0	0	0
Average length of turbine foundations at base (m)				26	26	26	0	0	0	0		0	0	0	0		0	0
Average width of turbine foundations at base(m)				26	26	26	0	0	0	0		0	0	0	0		0	0
Average depth of peat removed from turbine foundations (m)				0.3	0.1	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Average length of hard-standing at base (m)				80		85	0	0	0	0		0	0	0	0		0	0
Average width of hard-standing at base (m)				68	65		0	0	0	0		0	0	0	0		0	0
Average depth of peat removed from				0.3	0.3	0.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
hard-standing (m)												1.1	1.1					1.1
Maximum depth of drains (m)				0.3	0.3	0.5	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Total length of foundation and				106	101	111	0	0	0	0		0	0	0	0	0	0	0
hardstanding (m)							Ŭ	, i	· ·	ŭ		ŭ	ŭ	Ŭ	ŭ		Ŭ	Ŭ
Total width of foundation and				94	91	96	0	0	0	0		0	0	0	0	0	0	0
hardstanding (m)				J-T		30	Ŭ	Ŭ	Ŭ	Ŭ		v	Ŭ	Ŭ	Ŭ		·	
Area affected by drainage of foundation	4380	2010	7080	4380	2010	7080	0	0	0	0		0	0	0	0	0	0	0
and hardstanding area (n ²)	4300	2010	7000	4300	2010	7000	,	,	٥	٥		٥	,	U	٥		٠	U
Total area affected by drainage of	35040	16080	56640	35040	16080	56640	0	0	0	0		0	0	0	0	0	0	0
foundation and hardstanding area (n ²) Total volume affected by drainage of										U					U			
foundation and hardstanding area (n ³)	5957	2734	14160	5957	2734	14160	0	0	0	0		0	0	0	0		0	0

Peat affected by drainage of access		Total	
tracks	Exp	Min	Max
Floating roads			
Length of floating road that is drained (m)	0	0	0
Floating road width (m)	0.0	0.0	0.0
Average depth of drains associated with floating roads (m)	0.00	0.00	0.00
Area affected by drainage of floating			
roads (m²)	0	0	0
Volume affected by drainage of floating roads (m ³)	0	0	0
Excavated Road			
Length of access track that is excavated road (m)	2040	2040	2040
Excavated road width (m)	5	5	5
Average depth of peat excavated for road (m)	0.3	0.3	0.3
Area affected by drainage of excavated	40800	20400	61200
roads (m ²)	40000	20400	01200
Volume affected by drainage of	6936	3468	10404
excavated roads (m3)	0000	0.00	10101
Rock-filled roads			
Length of rock filled road that is drained (m)	0	0	0
Rock filled road width (m)	0	0	0
Average depth of drains associated with	0.0	0.0	0.0
rock filled roads (m)	0.0	0.0	0.0
Area affected by drainage of rock-filled roads (m ²)	0	0	0
Volume affected by drainage of rock-			
filled roads (m²)	0	0	0
Total area affected by drainage of	40800	20400	61200
access track (m ²) Total volume affected by drainage of	.5500	20400	0.200
access track (m ³)	6936	3468	10404

Peat affected by drainage of cable	Total						
trenches	Exp	Min	Max				
Length of any cable trench on peat that does not follow access tracks and is lined with a permeable medium (eg. sand) (m)	0	0	0				
Average depth of peat cut for cable trenches (m)	0.0	0.0	0.0				
Total area affected by drainage of cable trenches (m²)	0	0	0				
Total volume affected by drainage of cable trenches (m³)	0.00	0.00	0.00				

Drainage around additional peat excavated	Total Exp Min Max						
excavated	Exp	IVIII	wax				
Volume of additional peat excavated (m³)	0.0	0.0	0.0				
Area of additional peat excavated (n ²)	0.0	0.0	0.0				
Average depth of excavated peat (m)	0	0	0				
Radius of area excavated (m)	0	0	0				
Radius of excavated and drained area (m)	0	0	0				
Total area affected by drainage (m²)	0	0	0				
Total volume affected by drainage (m³)	0.00	0.00	0.00				

Assumption: Area excavated is assumed to be a circle

RESULTS	Total						
RESOLIS	Exp	Min	Max				
Total area affected by drainage due to windfarm (m²)	79851	38386	124157				
Total volume affected by drainage due to windfarm (m³)	13574.7	6525.552	25637.86				

Click here to move to 5d. CO2 loss from Click here drained peat

Click here to move to Payback Time Click here

Volume of peat drained

Note: Extent of site affected by drainage is calculated assuming an average extent of drainage around each drainage feature as given in the input data.

CO, loss due to drainage

Note: Note, CO, losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et al, 2008 - Final report).

Click here to move to 5. Loss of soil CQ Click here
Click here to move to Payback Time Click here

Will the hydrology of the site be restored on decommissioning? Will the habitat of the site be restored on decommissioning? Yes Calculations of C Loss from Drained Land if Site is NOT Restored after Decommissioning of C Loss from Drained Land if Site is NOT Restored after Decommissioning of C Loss from Drained Land (the CQ Log			
Will the habitat of the site be restored on decommissioning? Yes Calculations of C Loss from Drained Land if Site is NOT Restored after Decomposition of the property of the property of the Land is Site is NOT Restored after Decomposition of the property of the Land is Capability of the Capability	4	12	
	Yes	Yes	
Total volume affected by drainage due to wind farm (n^2) 13575 C Content of dry peat (% by weight, 0 0.000 Total GHG tensity (g or ") 0.000 Total GHG emissions from Drained Land (t CQ equiv.) 0 Total GHG Emissions from Undrained Land (t CQ equiv.) 0 0 Total GHG Emissions from Undrained Land (t CQ equiv.) 0 0 Total GHG Emissions from Undrained Land (t CQ equiv.) 0 0 Total GHG Emissions from Undrained Land (t CQ equiv.) 0 0 Total GHG Emissions of C loss from Drained Land (t Site IS Restored after Decommis 1. Losses if Land is Drained 1 Total GHG Emissions from Drained Land (t Ct_D equiv.) 0 0 Total GHG Emissions from Drained Land (t Ct_D+C) ha¹ yr¹) 0.000 (years) Methane Emissions from Drained Land (t Ct_D+C) ha¹ yr¹) 0.000 Conversion factor: Ct_D+C to CO_2 equivalents 30.67 CH_4 emissions from drained land (t CC_2 equiv.) 0 0 Total GHG emissions from Drained Land (t CC_2 equiv.) 14054 Total GHG emissions from Drained Land (t CC_2 equiv.) 14054 Total GHG emissions from Drained Land (t CC_2 equiv.) 14054 Total GHG emissions from Drained Land (t CC_2 equiv.) 14054 Total GHG emissions from Undrained Land (t Ct_D+C) ha¹ yr¹) 3.000 Methane Emissions from Undrained Land (t Ct_D+C) ha¹ yr¹) 0.04 Conversion factor: Ct_P-C to CO_2 equivalents 30.67 CH_2 emissions from Undrained Land (t Ct_D+C) ha¹ yr¹) 0.04 Conversion factor: Ct_P-C to CO_2 equivalents 30.67 CH_2 emissions from Undrained Land (t Ct_D+C) ha¹ yr¹) 0.04 Carbon Dioxide Emission in undrained soil (t Ct_D+C) ha¹ yr¹) 0.04 Carbon Dioxide Emission in undrained soil (t Ct_D+C) ha¹ yr¹) 0.000 CO_2 emissions from Undrained Land (t Ct_D+C) ha¹ yr¹) 0.000 CO_2 emissions from Undrained Land (t Ct_D+C) ha² yr¹) 0.000 CO_2 emissions from Undrained Land (t Ct_D+C) ha² yr²) 0.000 CO_2 emissions from Undrained Land (t Ct_D+C) 0.000 CO_2 emissions from Undrained Land	Yes	Yes	
C Content of dry peat (% by weight,	mmissionin		
Dry soil bulk density (g cr³) Total GHG emissions from Drained Land (t CQ equiv.) Total GHG Emissions from Drained Land (t CQ equiv.) Calculations of C loss from Drained Land if Site IS Restored after Decommis 1. Losses if Land is Drained Flooded period (days year¹) Lifetime of windfarm (years) Time required for regeneration of bog plants after restoration (years) Rate of methane emission in drained soil ((t Ct₂-C) ha¹ yr¹) Conversion factor: Ct₁-C to Co₂ equivalents Rate of carbon dioxide emission in drained soil (t CQha¹ yr¹) Carbon Dioxide Emissions from Drained Lanc Rate of carbon dioxide emission in drained soil (t CQha¹ yr¹) 35.20 Co₂ emissions from Drained Land (t CC₂ equiv.) 1054 2. Losses if Land is Undrainec Flooded period (days year¹) Lifetime of windfarm (years) 1064 Methane Emissions from Undrained Land Rate of methane emission in undrained soil (t CQ♭ ha¹ yr¹) 0.04 Conversion factor: Ct₁-C to Co₂ equivalents 30.67 CH₂ emissions from Undrained Land Rate of methane emission in undrained soil (t CQ♭ ha¹ yr¹) 0.04 Conversion factor: Ct₁-C to Co₂ equivalents 30.67 CH₂ emissions from Undrained Land Rate of carbon dioxide emission in undrained soil (t CQ♭ ha¹ yr¹) 0.04 Conversion factor: Ct₁-C to Co₂ equivalents 30.67 Carbon Dioxide Emissions from Undrained Land Rate of carbon dioxide emission in undrained soil (t CQ♭ ha¹ yr¹) 0.04 Carbon Dioxide Emissions from Undrained Land Rate of carbon dioxide emission in undrained soil (t CQ♭ ha¹ yr¹) 0.00 Co₂ emissions from Undrained Land (t CQ₂ equiv.) 7440	6526	25638	
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(years) Methane Emissions from Drained Lanc Rate of methane emission in drained soil ((t Ct)+C) ha¹ yr¹) O.000 Conversion factor: Ct)+C to CO₂ equivalents 30.67 Ct)+Q emissions from drained land (t CC₂ equiv.) O Carbon Dioxide Emissions from Drained Lanc Rate of carbon dioxide emission in drained soil (t CQha¹ yr¹) 35.20 CO₂ emissions from drained land (t CC₂) 14054 2. Losses if Land is Undrained Flooded period (days year¹) Lifetime of windfarm (years) 100 Wethane Emissions from Undrained Land Rate of methane emission in undrained soil (t Ct)+C ha¹ yr¹) O.04 Conversion factor: Ct)+C to CO₂ equivalents 30.67 Ct)+Q emissions from Undrained Land Rate of methane emission in undrained soil (t Ct)+C ha¹ yr¹) O.04 Conversion factor: Ct)+C to CO₂ equivalents Rate of carbon dioxide emission in undrained Land Rate of carbon dioxide emission in undrained Land Rate of carbon dioxide emission in undrained soil (t CQha¹ yr¹) O.00 CO₂ emissions from Undrained Land (t CQ equiv.) 7440 Total GHG Emissions from Undrained Land (t CQ equiv.)	40	40	nooded at any time of the year
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Conversion factor: CH_k -C to CO_2 equivalents 30.67 CH _e emissions from drained land (t CC_2 equiv.) 0 Carbon Dioxide Emissions from Drained Lant Rate of carbon dioxide emission in drained soil (t $CQha^1 yr^1$) 35.20 CO ₂ emissions from drained land (t CC_2) 14054 Total GHG emissions from Drained Land (t CC_2 equiv.) 14054 2. Losses if Land is Undrainec Flooded period (days year ¹) 178 Lifetime of windfarm (years) 40 Time required for regeneration of bog plants after restoration (years) 10 Methane Emissions from Undrained Land Rate of methane emission in undrained soil ((t CI_2 C) $ha^{-1} yr^{-1}$) 0.04 Conversion factor: CH_1 -C to CO_2 equivalents 30.67 CH _e emissions from undrained land (t CC_2 equiv.) 240 Carbon Dioxide Emissions from Undrained Lant Rate of carbon dioxide emission in undrained soil (t $CQha^{-1} yr^{-1}$) 0.00 CO ₂ emissions from undrained land (t CC_2) 7200 Total GHG Emissions from Undrained Land (t CC_2) 7440	0.000	0.000	Note:Conversion = (23 x 16/1
$ \begin{array}{c} CH_4 \text{emissions from drained land (t CC_2 equiv.)} & 0 \\ \hline \textbf{Carbon Dioxide Emissions from Drained Lanc} \\ \textbf{Rate of carbon dioxide emission in drained soil (t CQha^1 yr^1)} & 35.20 \\ \hline \textbf{CO}_2 \text{emissions from drained land (t CC_2)} & 14054 \\ \hline \textbf{Total GHG emissions from Drained Land (t CC_2 equiv.)} & 14054 \\ \hline \textbf{2. Losses if Land is Undrainec} \\ \hline \textbf{Flooded period (days year^1)} & 178 \\ \hline \text{Lifetime of windfarm (years)} & 40 \\ \hline \textbf{1ime required for regeneration of bog plants after restoration (years)} & 10 \\ \hline \textbf{Methane Emissions from Undrained Land} \\ \hline \textbf{Rate of methane emission in undrained soil ((t Ct]+C) ha^1 yr^1)} & 0.04 \\ \hline \textbf{Conversion factor: } CH_c-C to CO_2 equivalents & 30.67 \\ \hline \textbf{CH}_4 \text{emissions from undrained land} \\ \hline \textbf{Rate of carbon dioxide Emissions from Undrained Lanc} \\ \hline \textbf{Rate of carbon dioxide emission in undrained soil (t CQha^1 yr^1)} & 0.00 \\ \hline \textbf{CO}_2 \text{emissions from undrained land} \\ \hline \textbf{Rate of carbon dioxide emission in undrained soil (t CQha^1 yr^1)} & 0.00 \\ \hline \textbf{CO}_3 \text{emissions from undrained land (t CC_2)} & 7200 \\ \hline \textbf{Total GHG Emissions from Undrained Land (t CC_2 equiv.)} & 7440 \\ \hline \end{array}$	0.000	0.000	30.67 CO ₂ equiv. (CH ₄ -C)-1
Carbon Dioxide Emissions from Drained Lanc Rate of carbon dioxide emission in drained soil (t CQha¹ yr¹) 35.20 CO₂ emissions from drained land (t CC₂) 14054 Total GHG emissions from Drained Land (t CC₂ equiv.) 14054 2. Losses if Land is Undrainec Flooded period (days year¹) Lifetime of windfarm (years) 10 Methane Emissions from Undrained Land Rate of methane emission in undrained soil (t CQ♭C) ha¹ yr¹) 0.04 Conversion factor: CH₂-C to CO₂ equivalents 30.67 CH₂ emissions from undrained land Rate of carbon dioxide emission in undrained soil (t CQ♭C) Rate of carbon dioxide emission in undrained soil (t CQ♭C) Rate of carbon dioxide emission in undrained soil (t CQ♭C) Total GHG Emissions from Undrained Land Rate of carbon dioxide emission in undrained soil (t CQ♭C) Total GHG Emissions from Undrained Land (t CQ₂ equiv.) 7440	30.67	30.67	
Rate of carbon dioxide emission in drained soil (t $\mathbb{CQ} ha^1 yr^1$) 35.20 \mathbb{CO}_2 emissions from drained land (t \mathbb{CC}_2) 14054 Total GHG emissions from Drained Land (t \mathbb{CC}_2 equiv.) 14054 2. Losses if Land is Undrainec Flooded period (days year) 178 Lifetime of windfarm (years) 40 Time required for regeneration of bog plants after restoration (years) 10 $\mathbb{CQ} hand \mathbb{C} h$	0	0	
CO₂ emissions from drained land (t CC₂) 14054 Total GHG emissions from Drained Land (t CC₂ equiv.) 2. Losses if Land is Undrainec Flooded period (days year¹) Lifetime of windfarm (years) Time required for regeneration of bog plants after restoration (years) Methane Emissions from Undrained Land Rate of methane emission in undrained soil ((t Ct≱C) ha¹ yr¹) O.04 Conversion factor: Ct₄-C to CO₂ equivalents Ct₄-emissions from undrained land (t Cc₂ equiv.) Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQha¹ yr¹) O.00 Copy emissions from undrained land Rate of carbon dioxide emission in undrained soil (t CQha¹ yr¹) Total GHG Emissions from Undrained Land Rate of carbon dioxide emission in undrained soil (t CQha¹ yr²) Total GHG Emissions from Undrained Land (t CC₂ equiv.) 7440	35.20	35.20	
Total GHG emissions from Drained Land (t CC₂ equiv.) 2. Losses if Land is Undrainec Flooded period (days year¹) Lifetime of windram (years) Lifetime of windram (years) 10 Wethane Emissions from Undrained Land Rate of methane emission in undrained soil ((t Ct⅓-C) ha¹ yr¹) 0.04 Conversion factor: CH₂-C to CO₂ equivalents 30.67 CH₂ emissions from undrained land (t Cc₂ equiv.) 240 Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t Cc⊋ha⁻¹ yr⁻¹) 0.00 CO₂ emissions from undrained Land (t Cc₂) 7200 Total GHG Emissions from Undrained Land (t Cc₂ equiv.) 7440	6080	24037	
Flooded period (days year ¹) Lifetime of windfarm (years) 10 Wethane Emissions from Undrained Land Rate of methane emission in undrained soil ((t Ctg\C) ha¹ yr¹) O.04 Conversion factor: CH _t -C to CO ₂ equivalents 30.67 CH ₄ emissions from undrained land (t Cc ₂ equiv.) Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQ ha¹ yr¹) O.00 Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQ ha¹ yr¹) O.00 CO ₂ emissions from undrained land (t CQ) Total GHG Emissions from Undrained Land (t CC ₂ equiv.) 7440	6080	24037	1
Flooded period (days year ¹) Lifetime of windfarm (years) 10 Wethane Emissions from Undrained Land Rate of methane emission in undrained soil ((t Ctg\C) ha¹ yr¹) O.04 Conversion factor: CH _t -C to CO ₂ equivalents 30.67 CH ₄ emissions from undrained land (t Cc ₂ equiv.) Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQ ha¹ yr¹) O.00 Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQ ha¹ yr¹) O.00 CO ₂ emissions from undrained land (t CQ) Total GHG Emissions from Undrained Land (t CC ₂ equiv.) 7440	-	•	=
Lifetime of windfarm $\sqrt{\text{pears}}$ 40 Time required for regeneration of bog plants after restoration (years) 10 (Wears)	178	178	7
Time required for regeneration of bog plants after restoration (years)	40	40	
(years) Methane Emissions from Undrained Land Rate of methane emission in undrained soil ((t Ct+C) ha¹ yr¹) 0.04 Conversion factor: Ct+C to CO₂ equivalents 30.67 Ct+d emissions from undrained land (t Cc₂ equiv.) Carbon Dioxide Emissions from Undrained Lanc Rate of carbon dioxide emission in undrained soil (t CQha¹ yr¹) 0.00 CO₂ emissions from undrained land (t Cc₂) 7200 Total GHG Emissions from Undrained Land (t CC₂ equiv.)	5	15	
Rate of methane emission in undrained soil ((t $Cl_{\!\!P}C$) ha ⁻¹ yr ⁻¹) 0.04 Conversion factor: $Cl_{\!\!P}C$ to $Co_{\!\!2}$ equivalents 30.67 $Cl_{\!\!4}$ emissions from undrained land (t $Cc_{\!\!Q}$ equiv.) 240 Carbon Dioxide Emissions from Undrained Lant Rate of carbon dioxide emission in undrained soil (t $Co_{\!\!P}$) 7200 $Co_{\!\!2}$ emissions from undrained land (t $Cc_{\!\!Q}$) 7200 Total GHG Emissions from Undrained Land (t $Cc_{\!\!Q}$) 7440	5	15	
	0.04	0.04	
$ \begin{array}{ll} \text{CH}_4 \text{emissions} \text{from undrained land} (\text{t C}_2 \text{equiv.}) & 240 \\ \text{Carbon Dioxide Emissions from Undrained Lanc} \\ \text{Rate of carbon dioxide emission in undrained soil} (\text{t C}_2 \text{hs}^1 \text{yr}^1) & 0.00 \\ \text{CO}_2 \text{emissions} \text{from undrained land} (\text{t C}_2) & 7200 \\ \text{Total GHG Emissions from Undrained Land} (\text{t CC}_2 \text{equiv.}) & 7440 \\ \end{array} $	30.67	30.67	Note:Conversion = (23 x 16/12
Rate of carbon dioxide emission in undrained soil (t $\mathbb{C}\mathbb{Q}$ has \mathbb{Q}^1 yr \mathbb{Q}^1) 0.00 \mathbb{Q} 0.2 emissions from undrained land (t $\mathbb{C}(\mathbb{Q})$) 7200 Total GHG Emissions from Undrained Land (t $\mathbb{C}\mathbb{Q}$ equiv.) 7440	104	410	30.67 CO ₂ equiv. (CH ₄ -C) ⁻¹
CO ₂ emissions from undrained land (t CC ₂) 7200 Total GHG Emissions from Undrained Land (t CC ₂ equiv.) 7440			
Total GHG Emissions from Undrained Land (t CC ₂ equiv.) 7440	0.00	0.00	
	3115	12315	
3. CO ₂ Losses due to Drainage	3219	12725	
			_
Total GHG emissions from drained land (t CQ equiv.) 14054	6080	24037	
Total GHG emissions from undrained land (t CC ₂ equiv.) 7440	3219	12725	
RESULTS Total GHG emissions due to drainage (t CC₂ equiv.) 6614	2861	11312	

Click here to move to 5. Loss of soil CQ Click he

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CO, loss due to drainage
Note: Note, CQ; losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been derived directly from experimental data for acid bogs and fens (see Nayak et a 2008 - Final report).

Emission rates from soils

e: Note, CO₃ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is ablished approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al. 2008 - Final report).

Click here to move to 5d. Click here
here to move to Payback Time Click here

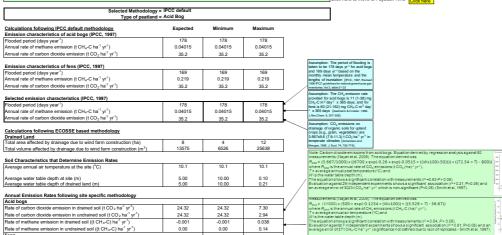
ote: Carbon dioude emissions from fens. Equation derived by regression analysis against 44 easurements (Nayake tal., 2009). The equation derived by regression analysis against 44 easurements (Nayake tal., 2009). The excustion derived was given 16.647.000 v. 16.244 x expl. 0.737 x expl. 0.073 x ((Wx100)-50)))+(13.3,23 x 7) where fig. is the analysis of option (m.).

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is the water table deputing.

Le equation shows a significant correlation with measurements (r² = 0.41, P>0.05)

Le equation shows a significant correlation with measurements (responsible to the second of the control of the contr



0.00

65.24 65.24

0.00

65.24 65.24 -0.003

0.14

18.71 7.82 0.073

Rate of methane emission in drained soil ((CH+,C) ha' yr'). Fens Rate of methane emission in undrained soil ((CH+,C) ha' yr'). Fens Rate of carbon dioxide emission in drained soil ((CO), ha' yr'). Rate of carbon dioxide emission in undrained soil ((CO), ha' yr'). Rate of carbon dioxide emission in undrained soil ((CO), ha' yr'). Rate of methane emission in drained soil ((CH+,C) ha' yr'). Rate of methane emission in undrained soil ((CH+,C) ha' yr'). 0.00 0.21 Selected emission characteristics following site specific methods of carbon dioxide emission in drained soil (t CO₂ ha⁻¹ yr⁻¹) Rate of carbon dioxide emission in undrained soil $(tCQ_2 \ln y^{-1})$ Rate of methane emission in drained soil $(tCQ_2 \ln x^{-1})$ y^{-1}) Rate of methane emission in drained soil $(tCH_4 - C) \ln x^{-1} y^{-1}$) Rate of methane emission in undrained soil $(tCH_4 - C) \ln x^{-1} y^{-1}$) 24.32 -0.001 -0.001 2.94 0.038 0.00 0.00 0.14

RESULTS Selected Emission Rates Selected Emission Rates
Rate of carbon dioxide emission in drained soil (t CO_2 ha⁻¹ yr⁻¹)
Rate of carbon dioxide emission in undrained soil (t CO_2 ha⁻¹ yr⁻¹)
Rate of methane emission in drained soil (tt CO_2 ha⁻¹ yr⁻¹) 35.20 0.00 0.000 35.20 0.00 0.000 Rate of methane emission in undrained soil ((t CH₄-C) ha⁻¹ yr⁻¹) 0.04 0.04

Click here to move to 5d. CO2 loss from drained peat
Click here to move to Payback Time
Click here



Note: Note, CO₂ losses are calculated using two approaches: IPCC default methodology and more site specific equations derived for this project. The IPCC methodology is included because it is the established approach, although it contains no site detail. The new equations have been thoroughly tested against experimental data (see Nayak et al., 2008 - Final report).

Emissions due to loss of DOC and POC
Note: Note, CO₂ losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC
POC leaching
No POC losses for bare soil included yet. If extensive areas of bare soil is present at site need modified calculation (Birnle et al, 1991)

	Expected	Minimum	Maximum	
Total C loss				Note: Only restored drained land included because if land is not
Gross CO ₂ loss from restored drained land (t CO ₂)	6854	2965	11722	restored, the C lost has already been counted as carbon dioxide
Gross CH ₄ loss from restored drained land (t CO ₂ equiv.)	0	0	0	
Gross CO ₂ loss from improved land (t CO ₂)				
Degraded Bog	0	0	0	
Felled Forestry	0	0	0	
Borrow Pits	0	0	0	
Foundations & Hardstanding	0	0	0	Assumption: DOC loss ranges between 7 - 40% of the total
Gross CH ₄ loss from improved land (t CO ₂ equiv.)				gaseous loss if calculated from the reported (minimum and
Degraded Bog	0	0	0	maximum) values in Worrall 2009 and is 26% of the total gaseous loss if calculated from the mean of reported maximum and minimur
Felled Forestry	0	0	0	value in Worrall 2009. These DOC values are flux based on soil
Borrow Pits	0	0	0	water concentration (i.e. 12.5 - 85.9 MgC/KM ² /yr)
Foundations & Hardstanding	0	ō	ō	and not on flux at catchment outlet (i.e. 10.3 - 21.8 MgC/KM²/yr
Conversion factor: CH ₄ -C to CO ₂ equivalents	30.6667	30.6667	30.6667	Worrall, F. et al., 2009. The multi-annual carbon budget of a peat-covered catchment. Science of
% total soil C losses, lost as DOC	26	7	40	Assumption: In the long term, 100% of leached DOC is assumed to
% DOC loss emitted as CO ₂ over the long term	100	100	100	be lost as CO ₂
% total soil C losses, lost as POC	8	4	10	Assumption: POC loss ranges between 4-10% of the total
% POC loss emitted as CO ₂ over the long term	100	100	100	gaseous loss if calculated from the reported values and is
Total gaseous loss of C (t C)	1873	810	3203	8% of the total gaseous loss if calculated from the mean or
Total C loss as DOC (t C)	487	57	1281	reported maximum and minimum value in Worrall 2009.
Total C loss as POC (t C)	150	32	320	POC range is (7 - 22.4 MgC/KM ² /yr) (Worrall et al, 2009).
RESULTS				
Total CO ₂ loss due to DOC leaching (t CO ₂)	1782	208	4689	Assumption: In the long term, 100% of leached POC is assumed to
Total CO ₂ loss due to POC leaching (t CO ₂)	548	119	1172	be lost as CO ₂
Total CO ₂ loss due to DOC & POC leaching (t CO ₂)	2330	326	5861	
Additional CO ₂ payback time of windfarm due to DOC &	POC			
coal-fired electricity generation (months)	0	0	0	
grid-mix of electricity generation (months)	1	0	2	
fossil fuel - mix of electricity generation (months)	0	0	1	

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Emissions due to loss of DOC and POC
Note: Note, CO₂ losses from DOC and POC are calculated using a simple approach derived from generic estimates of the percentage of the total CO2 loss that is due to DOC

Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

	Expected	Minimum	Maximum
Emissions due to forestry felling			
Area of forestry plantation to be felled (ha)	0	0	0
Carbon sequestered (tC ha ⁻¹ yr ⁻¹)	3.6	2.4	4.4
Lifetime of windfarm (years)	40	40	40
Carbon sequestered over the lifetime of the windfarm (t C ha ⁻¹)	144	96	176
RESULTS			
Total carbon loss due to felling of forestry (t CO ₂)	0	0	0
Additional CO ₂ payback time of windfarm due to management	of forestry		
coal-fired electricity generation (months)	0	0	0
grid-mix of electricity generation (months)	0	0	0
fossil fuel - mix of electricity generation (months)	0	0	0

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Emissions due to forest felling - calculation using simple management data

Note: Emissions due to forestry felling are calculated from the reduced carbon sequestered per crop rotation. If the forestry was due to be removed before the planned development, this C loss is not attributable to the wind farm and so the area of forestry to be felled should be entered as zero.

	Exp	Total Min	Max	Fo Exp	restry Are Min	a 1 Max	Fo Exp	restry Are Min	a 2 Max	Fo Exp	restry Are Min	a 3 Max	Fo Exp	restry Are Min	a 4 Max	Fo Exp	restry Are Min	a 5 Max
Loss of carbon sequestration due to felling																		
of forestry for the wind farm																		
Number of turbines Area felled around each turbine (ha)	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
Area of forestry plantation to	0	0	0	0		0	0	0	0		o	0	0	0	0		0	
be felled for wind farm (ha) Area replanted around each				0		0	0	0	0		0	0	0	0	0		0	
turbine (ha) Area of forestry plantation to	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
be replanted (ha) Area deforested for wind	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
farm (ha) Carbon sequestered per hectare for lifetime of the				0		0	0	0	0		0	0	o	0	0		0	
wind farm (t C ha ⁻¹) Total potential carbon sequestration loss due to felling of forestry for the wind farm (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Cleared Forest Floor																		
Emissions Soil type				Deep	Deep	Deep	Deep	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat
Life time of wind farm (years)	40	40	40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40
Area deforested for wind farm (ha)	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
Carbon released per hectare				5.00		5.00	5.00	5.00	5.00		5.00	5.00	5.00	5.00	5.00		5.00	
unforested (tC ha ⁻¹ yr ⁻¹) Total emissions due to			_															
cleared land (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Emissions from harvesting operations																		
Soil type				Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat	Deep Peat
Emissions from harvesting operations (g CO ₂ m ⁻³)	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
Age of forest to be felled (years)	0	0	0	0		0	0	0	0		0	0	0	0	0		0	
Area of forestry plantation to be felled for wind farm (ha)	0	0	0	0		0	0	0	0		0	0	o	0	0		0	
Volume of wood felled (m ³ ha				0		0	0	0	0		0	0	0	0	0		0	
Emissions due to harvesting operations (t	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
CO ₂)																		
Savings from use of felled forestry as biofuel																		
Is timber used as biofuel? Area of forestry plantation to	0	0	0	No 0		No 0	No 0	No 0	No 0		No 0	No 0	No 0	No 0	No 0		No 0	
be felled for wind farm (ha) Carbon in felled forestry (tC	ŭ	Ů	Ů															
ha ⁻¹) (Carbon : Biomass) ratio of				6 0.0		6 0.0	#N/A 0.0	#N/A 0.0	#N/A 0.0		#N/A 0.0	#N/A 0.0	#N/A 0.0	#N/A 0.0	#N/A 0.0		#N/A 0.0	
felled forestry Biomass weight of felled	0	0	0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	
Value of felled forestry as a		-	-	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
biomass fuel (MWh t ⁻¹) Total biomass power value (MWh)				0		0	0	0	0		0	0	0	0	0		0	
Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹)	0.424	0.424	0.424	0.424		0.424	0.424	0.424	0.424		0.424	0.424	0.424	0.424	0.424		0.424	
Savings in CO ₂ emissions associated with using felled	0	0	0	0		0	0	0	0		o	0	o	0	0		0	
forestry as a biofuel (t CO ₂) Distance to nearest biomass																		
power plant (km)	0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	0.0	0.0	0.0		0.0	
Emissions of CO ₂ associated with transportation by each km distance (t CO ₂ km ⁻¹) Total emissions of CO ₂	0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00		0.00	0.00	0.00	0.00	0.00		0.00	
associated with transportation (t CO _{2 eq.})				0		0	0	0	0		0	0	0	0	0		0	
Fossil fuel equivalent saving (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Savings from use of replanted forestry as a																		
biofuel Area of replanted forestry																		
(ha) Soil type	0	0	0	0 Deep Peat	0 Deep Peat	0 Deep Peat	0 Deep Peat	0 Deep	0 Deep	0 Deep Peat	0 Deep Peat	0 Deep	0 Deep Peat	0 Deep Peat	0 Deep Peat	0 Deep Peat	0 Deep Peat	0 Deep Peat
Number of years replanted				Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40	Peat 40
forestry grown on site (years) Carbon in replanted forestry																		
when felled (tC ha ⁻¹) (Carbon : Biomass) ratio of				272		272	#N/A	#N/A	#N/A		#N/A	#N/A	#N/A	#N/A	#N/A		#N/A	
felled forestry Biomass weight (t)	0	0	0	0.0 0	0.0 0	0.0 0	0.0	0.0	0.0	0.0 0	0.0 0	0.0 0	0.0 0	0.0	0.0 0	0.0	0.0 0	0.0
Value of replanted forestry as a biomass fuel (MWh t ⁻¹)				0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
l=																		
Total biomass power value (MWh)				0		0	0	0	0		0	0	0	0	0		0	
Total biomass power value (MWh) Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹)	0.424	0.424	0.424				0 0.424	0 0.424	0.424		0.424	0.424	0.424	0.424	0 0.424		0.424	
Total biomass power value (MWh) Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹) Savings in CO ₂ emissions associated with using	0.424	0.424	0.424	0		0												
Total biomass power value (MWh) Fossil fuel-mix emission factor (t CO ₂ MWh ⁻¹) Savings in CO ₂ emissions associated with using replanted forestry as a biofuel (t CO ₂) Distance to nearest biomass				0 0.424 0	0 0.424 0	0 0.424 0	0.424 0	0.424	0.424	0.424 0	0.424 0	0.424	0.424 0	0.424	0.424 0	0.424 0	0.424	0.424
Total biomass power value (MWh) (MWh) (Fossil fuel-mix emission factor (t CO ₂ MWh ⁺) (Savings in CO ₂ emissions associated with using replanted forestry as a biofuel (t CO ₂) (Distance to nearest biomass power plant (km)	0.424	0.424	0.424	0 0.424		0 0.424	0.424	0.424	0.424		0.424	0.424	0.424	0.424	0.424		0.424	
Total biomass power value (MWh) Fossil fuel-mix emission factor (t CO ₂ MWh¹¹) Savings in CO ₂ emissions associated with using replanted foresty as a biofuel (t CO ₂) Distance to nearest biomass power plant (km) Emissions of CO ₂ associated with transportation (t CO ₂ Mr)				0 0.424 0	0 0.424 0	0 0.424 0	0.424 0	0.424	0.424	0.424 0	0.424 0	0.424	0.424 0	0.424	0.424 0	0.424 0	0.424	0.424
Total blomass power value (MWh) Fossil flee-mix emission factor (tCO, MWh)*) Savings in CO, emissions associated with using replanted forestry as a bioface (t CO ₂). Distance to nearest biomass power plant (wm) Emissions of CO ₂ associated with transportation (t CO ₂ km² ¹r² ¹).	0.0	0.0	0.0	0 0.424 0 0.0	0 0.424 0	0 0.424 0	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424	0.424
Total biomass power value (MWh) Fossil fuel-mix emission factor (EO, MWh) Savings in CO, emissions associated with using replanted forestry as a bubdate (EO). Distance to nearest biomass power plant (En) Emissions of CO, associated with transportation (EO; km 1°) Carbon equivalent of transportation (EO; km 1°) Tossil fuel equivalent	0.0	0.0	0.0	0 0.424 0 0.0	0 0.424 0 0.0	0 0.424 0 0.0 0.0	0.424 0 0.0 0.00	0.424	0.424	0.424 0 0.0 0.00	0.424	0.424	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424	0.424 0 0.0 0.00	0.424 0 0.0 0.00
Total biomass power value (MWh) Fosal fuel-mix emission factor (EO, MWh) Savings in CO, emissions associated with using replanted forestry as a biotical (EO ₂). Distance to nearest biomass power plant (En) Emissions of CO, associated with transportation (EO ₂ km ¹ L [*]) Carbon equivalent of transportation (EO ₂ km ¹ L [*]) Fosal fuel equivalent saving (t CO ₂).	0.00	0.00	0.0	0 0.424 0 0.0 0.00	0 0.424 0 0.0 0.0	0 0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00								
Total biomass power value (MWH) Fossif lace this emission factor (FCO, MWH) Savings in CO, emissions associated with using a biofuel (FCO). Distance to rearest biomass power plant (km) Emissions of CO, associated with transportation (CO ₂ km) 1° (Carbon equivalent of transportation (CO ₂ km) 7° (Sossif fuel equivalent saving (CO ₂). RESULTS Total Carbon loss associated with forest	0.00	0.00	0.0	0 0.424 0 0.0 0.00	0 0.424 0 0.0 0.0	0 0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00	0.424 0 0.0 0.00								
Total biomass power value (MWh) Fossi flue-inix emission factor (FCO, MWh) Savings in CO, emissions associated with using biofuel (FCO) Distance to nearest biomass power plant (km) Emissions of CO, associated with transportation (FCO, MWh) It (F) Carbon equivalent of transportation (FCO, MWh) Tossi fluel equivalent saving (FCO) RESULTS Total Carbon loss ssociated with forest management (FCO) MRSULTS Total Carbon loss ssociated with forest management (FCO) MADITION of the Company of the CO, MWh) MADITION of the CO, MWH, MWH, MWH, MWH, MWH, MWH, MWH, MWH	0.00 0.00 0	0.00 0.00 0	0.0 0.00 0	0 0.424 0 0.0 0.00 0 0 ment of fo	0 0.424 0 0.0 0.00 0 0 0 restry	0 0.424 0 0.0 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0								
Total biomass power value (MXVIII)—The mission factor (**CO ₂ MWh**) Savings in CO ₃ emissions are consistent of the construction of the constru	0.0 0.00 0 0	0.00 0.00 0	0.00 0.00 0 0 manage	0 0.424 0 0.0 0.00 0	0 0.424 0 0.00 0.00 0 0	0 0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0 0	0.424 0 0.00 0.00 0 0	0.424 0 0.00 0.00 0 0	0.424 0 0.00 0.00 0 0						
Total biomass power value (MWH) Fossif up (MWH) Fossif up (MWH) Fossif up (MWH) Sarings of Optimization (MWH) Sarings of Optimization (MWH) Sarings of Optimization (MWH) Sarings of Optimization (CO ₂) Distance to nearest biomass power plant (km) Emissions of CO ₂ associated with transportation (t CO ₂) km 1° t) Fossif up (CO ₂) Fossif up (CO ₂) RESULTS Total Carbon loss sassociated with forest Additional CO ₂ payback time Additional CO ₂ payback time Cool-fired description Cool-fired descripti	0.00 0.00 0	0.00 0.00 0	0.0 0.00 0	0 0.424 0 0.0 0.00 0 0 ment of fo	0 0.424 0 0.0 0.00 0 0 0 restry	0 0.424 0 0.0 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0	0.424 0 0.00 0.00 0								

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Values taken from input		Total		Fo	restry Arc	na 1	Fo	restry Are	a 2	Fo	restry Are	na 3	Fo	restry Are	a 4	Fo	orestry Ar	ea 5
sheet	Exp	Min	Max			Max	Exp	Min	Max	Exp		Max	Exp	Min	Max	Exp	Min	Max
Accumulated temperature (day-degrees > 5°C) Code number	(> 1050 deg.C)																	
Major Soil Sub Group	Deep Peat			Deep Peat	Deep	Deep	0	0	0			0	0	0	0	0	0	0
Code number	2					2		٥				0	0	0	0			
Species	Scots pine			Scots pine	Scots pine	Scots pine	0	0	0			0	0	0	0	0	0	0
Code number	1					1	۰						0	0	0			
Age of forestry when felled for windfarm (yr)	0					0	0	0	0			0	0	0	0	0	0	0
Lifetime of windfarm (years)	40	40	40			40	40	40	40			40	40	40	40	40	40	40
Years after felling when replanting occurs	0					0	0	0	0			0	0	0	0	0	0	0
Age of seedlings on planting (yr) Years when replanted						0	0	0	0			0	0	0	0	0	0	0
forestry will be grown on wind farm site	40					40	40	40	40			40	40	40	40	40	40	40
RESULTS																		
Calculated Net Primary Production	Exp	Total Min	Max	Exp	restry Are Min	a 1 Max	Exp	restry Are Min	a 2 Max	Exp	restry An Min	ea 3 Max	Exp	restry Are Min	a 4 Max	Fo Exp	orestry Ar Min	ea 5 Max
Net loss in forest primary production over lifetime of wind farm (t C ha ¹)	272	272	272			272	#N/A	#N/A	#N/A			#N/A						
Total forest net primary production at felling for wind farm (t C ha ¹)	6	6	6	6	6	6	#N/A											
replanted forestry assuming same species replanted and managed over lifespan of windfarm (t C ha ⁻¹)	272	272	272	272	272	272	#N/A											

				Spe	cies			lelected Valu	10	
Parameter			Units	Scots Pine	Sitka Spruce	Area 1	Area 2	Area 3	Area 4	Area 5
3PG module										
Average annual photosynther	scally active radiation	2880	MJ m ⁻² yr ⁻¹			2880	2880		2880	
Light extinction coefficient		0.5				0.5	0.5		0.5	
Specific leaf area			m² kg¹ C	6	8	6	8		8	
Leaf longevity			yes	4	7	4	7		7	
Fine root longevity		1	yes			1	1		1	
Maximum light-use efficiency			kg C MJ day 1	0.00152	0.00166	0.00152	0.001656		0.001656	0.001656
Total reduction factor for mis- effects	environmental					0.3679	an/A		ANIA	
Ratio of NPP to GPP		0.47	-			0.47	0.47		0.47	
Allocation to foliage		0.25	-			0.25	0.25		0.25	
Coefficient for allocation resp	onse to nitrogen	1.00	-			1.00	1.00		1.00	
Age for 50% reduction in light	yes	100	120	100	120		120			
Initial foliage biomass		kg C m ²			0.005	0.005	0.005	0.005	0.006	
Understorey module										
Understorey LAI		3.00				3.00	3.00	3.00	3.00	3.00
										,
Conversion Factors	Quantum yield efficiency (mal mal ⁻¹)	to	Light use efficiency (kgC MJ ⁻¹)			GPP Reduc	tion Factor L			
	0.05		0.00130		Soil type		Less than	nulated tempo 1050 to 1350 ° C yr	More then	
	Light use efficiency (kgC MJ ¹)	to	Quantum yield efficiency (mol mol ")			Code	1	2	3	
	0.00135		0.0489		Peaty Gley	1	0.3178	0.3551	0.3720	
gDM_mail	24				Deep Peat	2	0.3177	0.3569	0.3679	1
molPAR MJ	2.3									

Integration step (yrs)	1		Forestry Area 1		Forestry Area 2		Forestry Area 3	Forestry Area 4	Forestry Area 5
		State variables	Light interception	Primary production State va	light interception	Primary production	State variables Light interception Primary production	State variables Light interception Primary production	State variables Light interception Primary production
Age (years)	Thinning regime	WF-Foliage biomsss (kg C LAI - Leaf are	oper - oper Utilized Utilized Absorbed absorbed absorbed photosynth- photosynt	NPP town - NPP to Commissed Net primary Total net total net blorouse (to	d pau - d pau : Utilized Utilized Absorbed absorbed absorbed area index photosynth-	d NPP NPP XNPP Comulated total net	6 per - 1950 or Utilized Assorbed Sharched Assorbed And Phrs NPP - 21/NPp - 21/NP	dpas - dpas - Utilized Utilize	dpas
			eticaty active radiation of radiation radiation the the (MJ m² yr²) (MJ m² yr²) (MJ m² yr²)	bees production primary (m²) (cm²) (cm²)	(m ² m ³) etcatly active radiation of radiation the radiation the the radiation (ML m ² yr ³)	of trees production production production (kg C m ² yr ²) (t C ha ¹ yr ²) (t C ha ¹)	Cm ²) (n ² m ²) electry-scrive reduction of season of the season of th	$(m^2)^{(i)} = (m^2)^{(i)}$ (mixed) states and states of states o	Cm ²) (m ² m ²) estantination of malities of malities of malitims of maliti
0 1 2	0.00 0.00 0.00	0.0050 0.03 0.0078 0.05 0.0122 0.07	15.77 2204 811 24.56 2186 804 38.08 2157 793	0.0 5.9 6 0.0050 0.0 5.9 12 #NA 0.0 5.9 18 #NA	0.04 BNIA 2193 BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	0.0050 0.04 RNIA 2193 BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	0050 0.04 BRUA 2193 BRUA BRUA BRUA BRUA BRUA BRUA BRUA BRUA	0.0050 0.04 BNIA 2193 BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA
3 4 5	0.00	0.0190 0.11 0.0295 0.18 0.0455 0.27	Aug. 2 2 2 2 2 2 2 2 2	0.0 6.0 24 ENA 0.1 6.0 30 ENA 0.1 6.1 36 ENA	SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	Section	100 100	AUS
6 7 8	0.00 0.00 0.00	0.0583 0.35 0.0741 0.44 0.0933 0.56	169.96 1878 691 211.09 1792 659 258.53 1691 622	0.1 6.2 4.2 FINA 0.2 6.2 48 FINA 0.2 6.3 55 FINA	SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA SPLIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	STALA	2014 2014 2014 2014 2014 2014 2014 2014	SNIA SPUIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SN
9 10 11	0.00	0.1161 0.70 0.1427 0.86 0.1730 1.04	311.61 1579 581 369.01 1458 536 428.82 1332 400	0.2 6.4 61 ENA 0.3 6.5 67 ENA 0.3 6.6 74 ENA	SPACE	ALIAR ALIAR ALIAR ALIAR ALIAR ALIAR	##WA #PNIA #	ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA	#### #################################
12 13	0.00	0.2063 1.24 0.2420 1.45	488.82 1205 443 546.75 1082 398	0.3 6.7 81 ENA 0.4 6.8 87 ENA	ENGA ENGA ENJA ENJA ENGA ENGA ENJA ENJA	ANIA ANIA ANIA ANIA ANIA ANIA	STRUA	ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA	### AND #### AND ### AND #### AND #### AND ### AND #### AND ##### AND #### AND #### AND #### AND #### AND #### AND #### AND ##### AND #### AND #### AND #### AND #### AND #### AND #### AND ##### AND #### AND #### AND #### AND #### AND #### AND #### AND ##### AND #### AND #### AND #### AND #### AND #### AND #### AND ###### AND #### AND #### AND #### AND #### AND ##### AND ##########
15 16	0.00	0.3167 1.90 0.3535 2.12	649.40 865 318 692.12 775 285	0.5 8.9 101 ENVA 0.5 7.0 108 ENVA	SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA	ANIA ANIA ANIA ANIA ANIA ANIA	STVA STVIA S	NNA SNIA SNIA SNIA SNIA SNIA SNIA SNIA S	AVIS AVIS AVIS AVIS AVIS AVIS AVIS AVIS
18	0.00	0.4217 2.53 0.4520 2.71	750.68 631 232 785.40 577 212	0.5 7.1 122 ENVA 0.6 7.1 129 ENVA	SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA	ANIA ANIA ANIA ANIA ANIA ANIA	STVA STVIA S	NNA SNIA SNIA SNIA SNIA SNIA SNIA SNIA S	AVIS AVIS AVIS AVIS AVIS AVIS AVIS AVIS
21 22 22	0.00	0.4260 2.56 0.4558 2.73	762.86 623 229 787.69 570 210	0.5 7.1 143 ENA 0.6 7.1 151 ENA	SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA	ania ania ania ania ania ania	STUA STUA STUA STUA STUA STUA STUA STUA	BEGG BEGG BEGG BEGG BEGG BEGG BEGG BEGG	1004 1004 1004 1004 1004 1004 1004 1004
23 24 25	0.00	0.4825 2.90 0.5062 3.04 0.4355 2.61	824.70 490 180 769.64 606 223	0.6 7.2 165 ENA 0.6 7.2 165 ENA 0.5 7.1 172 ENA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	REGG STOCK S	STOCK
26 27 28	0.00	0.4896 2.94 0.5121 3.07	811.30 515 189 826.44 481 177	0.8 7.1 179 ENA 0.8 7.1 186 ENA 0.8 7.2 193 ENA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ania ania ania ania ania ania	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	RECA STOCA S	STUA STUA STUA STUA STUA STUA STUA STUA
30 31	0.17 0.00	0.4599 2.76 0.4854 2.91	786.50 563 207 806.06 522 192	0.8 7.1 208 ENA 0.8 7.1 215 ENA	SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA	ANA BALA BALA ANA BALA BALA ANA BALA	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	REGA STEGA STORA S	2014 2014 2014 2014 2014 2014 2014 2014
32 33 34	0.00	0.5078 3.05 0.5273 3.16 0.5441 3.26	819.97 488 179 831.81 460 169 841.10 437 161	0.6 7.1 222 ENA 0.6 7.2 229 ENA 0.6 7.2 236 ENA	SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA	ANA BALA BALA ANA BALA BALA ANA BALA	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	REGA STEGA STORA S	2014 2014 2014 2014 2014 2014 2014 2014
35 36 37	0.14 0.00 0.00	0.4813 2.89 0.5034 3.02 0.5225 3.14	797.43 528 194 811.81 494 182 823.08 467 172	0.6 7.1 243 ENA 0.6 7.1 250 ENA 0.6 7.1 258 ENA	ANIA BNIA BNIA BNIA ANIA BNIA BNIA ANIA BNIA BNIA	ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	AUGE AUGE AUGE AUGE AUGE AUGE AUGE AUGE
38 39 40	0.00 0.00 0.05	0.5389 3.23 0.5527 3.32 0.5363 3.22	831.76 444 163 838.26 426 157 826.31 448 165	0.6 7.1 265 ENA 0.6 7.1 272 ENA 0.6 7.1 279 ENA	SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA	ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR	STVA STVIA S	RNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA S	AUSE AUSE AUSE AUSE AUSE AUSE AUSE AUSE
41 42 43	0.00 0.00 0.00	0.5498 3.30 0.5610 3.37 0.5702 3.42	832.36 430 158 836.58 416 153 839.25 404 149	0.6 7.1 286 ENA 0.6 7.1 293 ENA 0.6 7.1 300 ENA	RNIA BRIA BNIA BNIA RNIA BRIA BNIA BNIA RNIA BRIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	STVÁ SPOLA STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ SPOLA STVÁ STVÁ SPOLA STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ STVÁ	REGA SEGA SENA SENA SENA SELA SELA SELA SELA SEGA SEGA SEGA SENA SENA SENA SENA SENA SENA SENA SEN	# # # # # # # # # # # # # # # # # # #
44 45 46	0.00 0.05 0.00	0.5775 3.47 0.5522 3.31 0.5612 3.37	840.61 396 146 823.57 427 157 825.77 415 153	05 70 100 MAN. 05 70 100 MAN. 05 70 100 MAN. 05 70 100 MAN. 05 71 100 MAN. 06 71 100 MAN. 06 71 100 MAN. 06 72 100 MAN. 06 72 100 MAN. 06 72 201 MAN. 06 71 202 MAN. 06 71 200 MAN.	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	SVA PNA RNA SNA PNA RNA RNA <td>REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN</td> <td>#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA</td>	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
47 48 49	000 000 000 000 000 000 000 000 000 00	0.0071 0.007	Aug. 2 18 18 18 18 18 18 18	0.6 7.0 328 #N/A 0.6 7.0 395 #N/A 0.6 6.9 342 #N/A	SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA SPAIGA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	Section Sect	REGA SEGA SENA SENA SENA SENA SENA SENA SENA SEN	Section
50 51 52	0.00			0.8 6.9 349 FNA 0.0 5.9 6 FNA 0.0 5.9 12 FNA	SNIA SNIA SNIA SNIA 0.04 SNIA 2193 SNIA SNIA SNIA SNIA SNIA	ania ania ania ania ania ania ania ania	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	RNA 8NA 8NA 8NA 8NA 8NA 8NA 8NA 8NA 8NA 8	0.0000 0.04 0000 0000 0000 0000
53 54 55	0.00	0.0122 0.07 0.0190 0.11 0.0295 0.18	15.77 2204 811 24.56 2166 804 38.08 2157 703 58.72 2113 777 80.71 2048 753 155.22 11502 718 160.99 1878 601 211.00 1702 609 296.53 1601 529 296.53 1601 529 390.01 1458 536 429.82 1322 400 488.82 1205 443 546.75 1002 308	0.0 6.0 24 ENA 0.1 6.0 30 ENA	BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ania ania ania ania ania ania	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	RECA STOCA S	STUA STUA STUA STUA STUA STUA STUA STUA
56 57 58	0.00	0.0455 0.27 0.0583 0.35 0.0741 0.44	195.22 1962 718 169.96 1878 691 211.09 1792 659	0.1 6.1 36 FNA 0.1 6.2 42 FNA 0.2 6.2 48 FNA	SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA	ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR ALFR	STVA STVIA S	RNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA S	AUSE AUSE AUSE AUSE AUSE AUSE AUSE AUSE
59 60 61	0.00 0.00 0.00	0.0933 0.56 0.1161 0.70 0.1427 0.86	258.53 1691 622 311.61 1579 581 369.01 1458 536	02 63 55 FNA 02 64 61 FNA 03 65 67 FNA	RNIA BRIA BNIA BNIA RNIA BRIA BNIA BNIA RNIA BRIA BNIA BNIA	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE	STVÁ STVÍA STVÍA STVÍA STVÍA STVÁ STVÍA ST	REGA SPECA S	AUSE ALLEE ALLEE ALGE ALGE AUGE AUGE AUGE AUGE AUGE AUGE AUGE AU
62 63 64	0.00 0.00 0.00	0.1730 1.04 0.2063 1.24 0.2420 1.45	428.82 1332 490 488.82 1205 443 546.75 1082 308	0.3 6.6 74 #NA 0.3 6.7 81 #NA 0.4 6.8 87 #NA	STOCA STOCA STATE STATE STOCA STACE STATE	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE	RIVIA RIVIA BINIA	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANNA RAMA BANA ANNA ANNA ANNA ANNA ANNA ANNA A
65 66 67	0.00 0.00 0.00	0.2792 1.68 0.3167 1.90 0.3535 2.12	600.72 968 356 649.40 865 318 692.12 775 285	0.4 6.8 94 #NA 0.5 6.9 101 #NA 0.5 7.0 108 #NA	STOCA STOCA STATE STATE STOCA STACE STATE	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE	STUA STUIA S	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANNA RAMA BANA ANNA ANNA ANNA ANNA ANNA ANNA A
68 69 70	0.000 0.000	0.0050 0.00 0.00 0.00 0.00 0.00 0.00 0.	200 200	0.5 7.0 115 INVA 0.5 7.1 122 INVA 0.6 7.1 129 INVA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	100	100 100	
71 72 73	0.00 0.00 0.00	0.3935 2.36 0.4260 2.56 0.4558 2.73	732.93 687 253 762.86 623 229 787.69 570 210	0.5 7.0 196 ANIA 0.5 7.1 143 ANIA 0.6 7.1 151 ANIA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
74 75 76	0.00 0.00 0.00	0.4825 2.90 0.5062 3.04 0.4355 2.61	808.08 526 194 824.70 490 180 769.64 606 223	0.6 7.2 158 #NA 0.6 7.2 165 #NA 0.5 7.1 172 #NA	STOCA STOCA STATE STATE STOCA STACE STATE	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE	RIVIA RIVIA BINIA	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANNA RAMA BANA ANNA ANNA ANNA ANNA ANNA ANNA A
77 78 79	0.00 0.00 0.00	0.4641 2.78 0.4896 2.94 0.5121 3.07	792.58 556 205 811.30 515 189 826.44 481 177	0.6 7.1 179 INVA 0.6 7.1 186 INVA 0.6 7.2 193 INVA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
80 81 82	0.00 0.00 0.00	0.5317 3.19 0.4599 2.76 0.4854 2.91	838.58 454 167 786.50 563 207 806.06 522 192	0.6 7.2 201 RNA 0.6 7.1 208 RNA 0.6 7.1 215 RNA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
83 84 85	0.00 0.00 0.00	0.5078 3.05 0.5273 3.16 0.5441 3.26	819.97 488 179 831.81 460 169 841.10 437 161	0.6 7.1 222 #NA 0.6 7.2 229 #NA 0.6 7.2 236 #NA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA BRUA BRUA BRUA BRUA BRUA BRUA BRUA BRU	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANYS ALMS ALMS ALMS ALMS ALMS ALMS ALMS ALM
86 87 88	0.00 0.00 0.00	0.4813 2.89 0.5034 3.02 0.5225 3.14	797.43 528 194 811.81 494 182 823.08 467 172	0.6 7.1 243 RNA 0.6 7.1 250 RNA 0.6 7.1 258 RNA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
89 90 91	0.00 0.00 0.00	0.5389 3.23 0.5527 3.32 0.5363 3.22	831.76 444 163 838.26 426 157 826.31 448 165	0.6 7.1 265 #NA 0.6 7.1 272 #NA 0.6 7.1 279 #NA	STOCA STOCA STATE STATE STOCA STACE STATE	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE	RIVIA RIVIA BINIA	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANNA RAMA BANA ANNA ANNA ANNA ANNA ANNA ANNA A
92 93 94	0.00 0.00 0.00	0.5498 3.30 0.5610 3.37 0.5702 3.42	832.36 430 158 838.58 416 153 839.25 404 149	0.6 7.1 286 RNA 0.6 7.1 293 RNA 0.6 7.1 300 RNA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
95 96 97	0.00 0.00 0.00	0.5775 3.47 0.5522 3.31 0.5612 3.37	840.61 396 146 823.57 427 157 825.77 415 153	0.6 7.0 307 #N/A 0.6 7.0 314 #N/A 0.6 7.0 321 #N/A	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA BRUA BRUA BRUA BRUA BRUA BRUA BRUA BRU	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANYS ALMS ALMS ALMS ALMS ALMS ALMS ALMS ALM
98 99 100	0.00 0.00 0.00	0.5684 3.41 0.5739 3.44 0.5780 3.47	825.77 415 153 826.60 407 150 826.24 400 147 824.85 395 145	0.6 7.0 328 #NA 0.6 7.0 335 #NA 0.6 6.9 342 #NA	RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA RNIA	ania ania ania ania ania ania ania ania	#NVA #NVA #NVA #NVA #NVA #NVA #NVA #NVA	INIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	# # # # # # # # # # # # # # # # # # #
101 102 103	0.00 0.00 0.00 0.00 0.00	0.0050 0.03 0.0078 0.05 0.0122 0.07	15.77 2204 811 24.56 2186 804 38.08 2157 793 58.72 2113 777 89.71 2048 753	0.0 59 6 FNA 0.0 59 12 FNA 0.0 59 18 FNA	0.04 INVA 2193 INVA INVA INVA INVA INVA INVA INVA INVA INVA INVA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	00000 0.64 RVA 2123 RVA RNA RVA RVA RNA 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000 0.04 88VA 2193 88VA 88VA 88VA 88VA 88VA 88VA 88VA 88V	0.0050 0.04 8NA 2193 8NA
104 105 106	0.00 0.00 0.00	0.0190 0.11 0.0295 0.18 0.0455 0.27	135.22 1952 718	0.0 6.0 24 #NA 0.1 6.0 30 #NA 0.1 6.1 36 #NA	STOCA STOCA STATE STATE STOCA STACE STATE	ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE ALIFE		REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANNA RAMA BANA ANNA ANNA ANNA ANNA ANNA ANNA A
107 108 109	0.00 0.00 0.00	0.0583 0.35 0.0741 0.44 0.0933 0.56	169.96 1878 691 211.09 1792 659 258.53 1691 622	0.1 6.2 42 RNA 0.2 6.2 48 RNA 0.2 6.3 55 RNA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
110 111 112	0.00 0.00 0.00	0.1161 0.70 0.1427 0.86 0.1730 1.04	311.61 1579 581 369.01 1458 536 428.82 1332 490	0.2 6.4 61 RNA 0.3 6.5 67 RNA 0.3 6.6 74 RNA	SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA SPOIA	ANA ANA ANA ANA ANA ANA ANA ANA ANA	RIVA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SNI	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANYS ALVES A
113 114 115	0.00 0.00 0.00	0.2063 1.24 0.2420 1.45 0.2792 1.68	488.82 1205 443 546.75 1062 398 600.72 968 356	0.3 6.7 81 RNA 0.4 6.8 87 RNA 0.4 6.8 94 RNA	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SINA SINA SINA SINA SINA SINA SINA SIN	#NIA #NIA #NIA #NIA #NIA #NIA #NIA #NIA
116 117 118	0.00 0.00 0.00	0.3167 1.90 0.3535 2.12 0.3887 2.33	649.40 865 318 692.12 775 285 728.78 697 256	0.5 6.9 101 #N/A 0.5 7.0 108 #N/A 0.5 7.0 115 #N/A	SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA SPECA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RIVIA SINIA	REGA SEGA SEGA SEGA SEGA SEGA SEGA SEGA S	ANYS ALMS ALMS ALMS ALMS ALMS ALMS ALMS ALM
119 120 121	0.00 0.00 0.00	0.4217 2.53 0.4520 2.71 0.3935 2.36	759.68 631 232 785.40 577 212 732.93 687 253	0.5 7.1 122 #NA 0.8 7.1 129 #NA 0.5 7.0 198 #NA	ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	#NA	RNIA ERVIA BINA BINA BINA BINA BINA BINA BINA BI	ANIA RAME ANIA BANA ANIA ANIA ANIA ANIA ANIA ANIA
122 123 124	0.00 0.00 0.00	0.4260 2.56 0.4558 2.73 0.4825 2.90	762.86 623 229 787.69 570 210 808.08 526 194	0.5 7.1 143 #NA 0.6 7.1 151 #NA 0.6 7.2 158 #NA	SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA SINIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	### #### #### #### #### #### #### ##### ####	RNIA SNIA BNIA SNIA SNIA SNIA SNIA SNIA SNIA SNIA S	#NUA #NUA #NUA #NUA #NUA #NUA #NUA #NUA
125 126 127	0.00 0.00 0.00	0.5062 3.04 0.4355 2.61 0.4841 2.78	824.70 490 180 769.64 606 223 792.58 556 205	0.6 7.2 165 #NA 0.5 7.1 172 #NA 0.6 7.1 179 #NA	ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA ENCIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	#NA	RNIA ERVIA BINA BINA BINA BINA BINA BINA BINA BI	ANIA RAME ANIA BANA ANIA ANIA ANIA ANIA ANIA ANIA
128 129 130	0.00 0.00 0.00	0.4896 2.94 0.5121 3.07 0.5317 3.19	811.30 515 189 826.44 481 177 838.58 454 167	0.6 7.1 186 #N/A 0.6 7.2 193 #N/A 0.6 7.2 201 #N/A	RNIA RNIA BNIA BNIA RNIA RNIA BNIA BNIA RNIA RNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	## ## ## ## ## ## ## ## ## ## ## ## ##	RNIA STUA SINA SINA SINA SINA SINA SINA SINA SIN	SPUA (SPUA SPUA SPUA SPUA SPUA SPUA SPUA SPUA
131 132 133	0.00 0.00 0.00	0.4599 2.76 0.4854 2.91 0.5078 3.05	786.50 563 207 806.06 522 192 819.97 488 179	0.6 7.1 208 RNA 0.6 7.1 215 RNA 0.6 7.1 222 RNA	RNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	SPUA SPUA SPUA SPUA SPUA SPUA SPUA SPUA	RNIA STNIA	SPUA SPUA SPUA SPUA SPUA SPUA SPUA SPUA
134 135 136	0.00 0.00 0.00	0.5273 3.16 0.5441 3.26 0.4813 2.89	831.81 460 169 841.10 437 161 797.43 528 194	0.6 7.2 229 #N/A 0.6 7.2 236 #N/A 0.6 7.1 243 #N/A	RNIA INIA INIA INIA RNIA INIA INIA INIA RNIA INIA INIA INIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	AND	RNIA RNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA RNIA BNIA BNIA BNIA BNIA BNIA BNIA BNIA RNIA BNIA BNIA BNIA BNIA BNIA BNIA	AUSE AUSE AUSE ANNS AUSE AUSE AUSE AUSE AUSE AUSE AUSE AUS
137 138 139	0.00 0.00 0.00	0.5034 3.02 0.5225 3.14 0.5389 3.23	811.81 494 182 823.08 467 172 831.76 444 163	0.6 7.1 250 #NA 0.6 7.1 258 #NA 0.6 7.1 265 #NA	RICA BRIA BRIA BRIA RICA BRIA BRIA RICA BRIA BRIA BRIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	## ## ## ## ## ## ## ## ## ## ## ## ##	RPUA BRUA BANA BANA BANA BANA BANA BANA BANA RPUA BANA BANA BANA BANA BANA BANA BANA BA	#FUA BYLA BYLA BYNA BANA BANA BANA BANA BANA BANA BYNA BYLA BYLA BANA BANA BANA BANA BANA BANA BANA BYLA BYLA BANA BANA BANA BANA BANA BANA
140 141 142	0.00 0.00 0.00	0.5527 3.32 0.5363 3.22 0.5498 3.30	838.26 426 157 826.31 448 165 832.36 430 158	0.6 7.1 272 #N/A 0.6 7.1 279 #N/A 0.6 7.1 286 #N/A	STOR STOR SINIA SINIA STOR STOR SINIA SINIA STOR STOR SINIA SINIA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	RVLA RVLA BRUA BNIA BNIA BNIA BNIA BNIA BNIA BNIA BNI	RNA SNIA SNIA SNIA SNIA SNIA SNIA SNIA SN	APOLA BRUGA
143 144 145	0.00 0.00 0.00	0.0751 0.49 0.99 0.00 0.00 0.00 0.00 0.00 0.00	836.58 416 153 839.25 404 149 840.61 396 146	0.0	MA	Section Sect	Section	Mart	
107 108 108 108 108 108 108 108 108 108 108	0.000	0.0551 0.56 0.56 0.56 0.56 0.56 0.56 0.56 0.56	1997 1997	0.0 0.0	ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA ENGA	ANIA ANIA ANIA ANIA ANIA ANIA ANIA ANIA	Section	Mart	Miles
149	0.00	0.5739 3.44	626 24 400 147	0/6 7.0 335 #N/A	ATOM BRIA BRIA BRIA	ANYA ANYA ANYA	ATEX ATEX STEEL ST	FROM BRIA BNIA BNIA BNIA BNIA BNIA BNIA	ATON ATON AND AND AND AND AND AND AND

Californ sequestration in Ireas

Employee swinter of the SPC month (press) and a 2009. This vertice, these "troppes dende due or ne-special environmental resolute in a constant investor of the SPC month (press) and the second constant investor of the SPC month (press) and the second constant investor of the second co

Carbon sequestration in soil under trees

Note. More data needed. This should be the respiration from newly felled and disturbed soil, so as to include respiration from fresh plant inputs, from background soil organic matter decomposition, and from the disturbance of soil resulting in the release of additional C from soil aggregates. Different types of management disturbance should be considered. This information is not yet available, but will become available following experiments to be done by Milke Perks during 2009-2012. As an interim measure, C sequestration in soil under trees is used, so including background respiration from soil organic matter decomposition and respiration from fresh plant input.

Carbon Sequestration in Soil

Under Trees: Lookup

<u>Table</u>

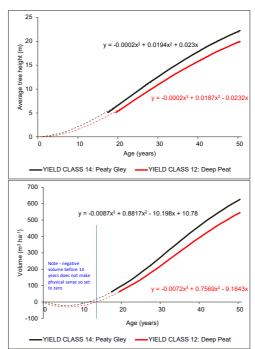
Peaty Gley	Deep Peat (t
(t C ha ⁻¹ yr ⁻¹)	C ha ⁻¹ yr ⁻¹)
3.98	5.00

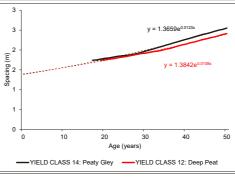
STAND_ID ForestGALES SPECIES Sitka Spruce

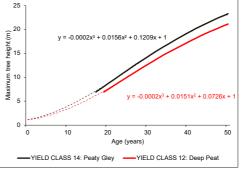
YIELD	CLASS	14: F	Peatv	Glev

Yield class	Initial Spacing (m)	Age (years)	Average tree height (m)	Volume m³ ha -1	Spacing (m)	Maximum tree height (m)
14	1.7	0	0.00	0.0	1.37	1.00
14	1.7	1	0.04	0.0	1.38	1.14
14	1.7	2	0.12	0.0	1.40	1.30
14	1.7	3	0.24	0.0	1.42	1.50
14	1.7	4	0.39	0.0	1.43	1.72
14	1.7	5	0.58	0.0	1.45	1.97
14	1.7	6	0.79	0.0	1.47	2.24
14	1.7	7	1.04	0.0	1.49	2.54
14	1.7	8	1.32	0.0	1.51	2.86
14	1.7	9	1.63	0.0	1.53	3.21
14	1.7	10	1.97	0.0	1.54	3.57
14	1.7	11	2.33	0.0	1.56	3.95
14	1.7	12	2.72	0.0	1.58	4.35
14	1.7	13	3.14	0.0	1.60	4.77
14	1.7	14	3.58	6.2	1.62	5.20
14	1.7	15	4.04	16.1	1.64	5.65
14	1.7	16	4.52	26.9	1.66	6.11
14	1.7	17	5.08	62	1.74	6.9
14 14	1.7	18 19	5.68	76.4	1.75	7.48
	1.7		6.29	90.8	1.77	8.06
14 14	1.7	20	6.90	105.2	1.79	8.64
14	1.7 1.7	21 22	7.51 8.11	119.6 134	1.8 1.82	9.22 9.8
14		23				
14	1.7 1.7	23 24	8.72 9.33	151.8 169.6	1.84 1.85	10.38 10.96
14	1.7	24 25	9.33	187.4	1.85	11.54
14	1.7	26	10.54	205.2	1.87	12.12
14	1.7	27	11.15	203.2	1.89	12.12
14	1.7	28	11.71	242.6	1.03	13.24
14	1.7	29	12.28	262.2	1.94	13.24
14	1.7	30	12.20	281.8	1.97	14.32
14	1.7	31	13.41	301.4	2	14.86
14	1.7	32	13.41	321	2.03	15.4
14	1.7	33	14.50	340.4	2.06	15.4
14	1.7	34	15.02	359.8	2.09	16.4
14	1.7	35	15.54	379.2	2.12	16.9
14	1.7	36	16.07	398.6	2.15	17.4
14	1.7	37	16.59	418	2.18	17.9
14	1.7	38	17.07	435.8	2.21	18.36
14	1.7	39	17.55	453.6	2.24	18.82
14	1.7	40	18.04	471.4	2.27	19.28
14	1.7	41	18.52	489.2	2.3	19.74
14	1.7	42	19.00	507	2.33	20.2
14	1.7	43	19.42	522.6	2.36	20.6
14	1.7	44	19.84	538.2	2.39	21
14	1.7	45	20.25	553.8	2.41	21.4
14	1.7	46	20.67	569.4	2.44	21.8
14	1.7	47	21.09	585	2.47	22.2
14	1.7	48	21.47	598.6	2.5	22.56
14	1.7	49	21.85	612.2	2.52	22.92
14	1.7	50	22.22	625.8	2.55	23.28

Yield class	Initial Spacing (m)	Age (years)	Average tree height (m)	Volume m³ ha -1	Spacing (m)	Maximum tree height (m)
12	1.7	0	0.00	0.0	1.38	1.00
12	1.7	1	0.00	0.0	1.40	1.09
12	1.7	2	0.03	0.0	1.41	1.20
12	1.7	3	0.09	0.0	1.43	1.35
12	1.7	4	0.19	0.0	1.45	1.52
12	1.7	5	0.33	0.0	1.46	1.72
12	1.7	6	0.49	0.0	1.48	1.94
12	1.7	7	0.69	0.0	1.49	2.18
12	1.7	8	0.91	0.0	1.51	2.44
12	1.7	9	1.16	0.0	1.53	2.73
12	1.7	10	1.44	0.0	1.54	3.04
12	1.7	11	1.74	0.0	1.56	3.36
12	1.7	12	2.07	0.0	1.58	3.70
12	1.7	13	2.42	0.0	1.59	4.06
12	1.7	14	2.79	0.3	1.61	4.43
12	1.7	15	3.18	8.5	1.63	4.81
12	1.7	16	3.60	17.6	1.65	5.21
12	1.7	17	4.03	27.6	1.66	5.62
12	1.7	18	4.47	38.3	1.68	6.03
12	1.7	19	5.08	63	1.74	6.9
12	1.7	20	5.64	76.2	1.75	7.44
12	1.7	21	6.21	89.4	1.77	7.98
12	1.7	22	6.77	102.6	1.78	8.52
12	1.7	23	7.34	115.8	1.8	9.06
12	1.7	24	7.90	129	1.82	9.6
12	1.7	25	8.45	145.2	1.83	10.12
12	1.7	26	8.99	161.4	1.85	10.64
12	1.7	27	9.54	177.6	1.87	11.16
12	1.7	28	10.08	193.8	1.89	11.68
12	1.7	29	10.62	210	1.91	12.2
12	1.7	30	11.15	227.6	1.92	12.7
12	1.7	31	11.67	245.2	1.94	13.2
12	1.7	32	12.19	262.8	1.96	13.7
12	1.7	33	12.72	280.4	1.97	14.2
12	1.7	34	13.24	298	1.99	14.7
12	1.7	35	13.70	315.2	2.02	15.14
12	1.7	36	14.16	332.4	2.04	15.58
12	1.7	37	14.62	349.6	2.07	16.02
12	1.7	38	15.08	366.8	2.1	16.46
12	1.7	39	15.54	384	2.13	16.9
12	1.7	40	15.98	399.8	2.15	17.32
12	1.7	41	16.42	415.6	2.18	17.74
12	1.7	42	16.86	431.4	2.2	18.16
12	1.7	43	17.30	447.2	2.23	18.58
12	1.7	44	17.74	463	2.26	19
12	1.7	45	18.12	477	2.28	19.36
12	1.7	46	18.50	491	2.31	19.72
12	1.7	47	18.87	505	2.33	20.08
12	1.7	48	19.25	519	2.36	20.44
12	1.7	49	19.63	533	2.39	20.8
12	1.7	50	19.96	544.8	2.41	21.12



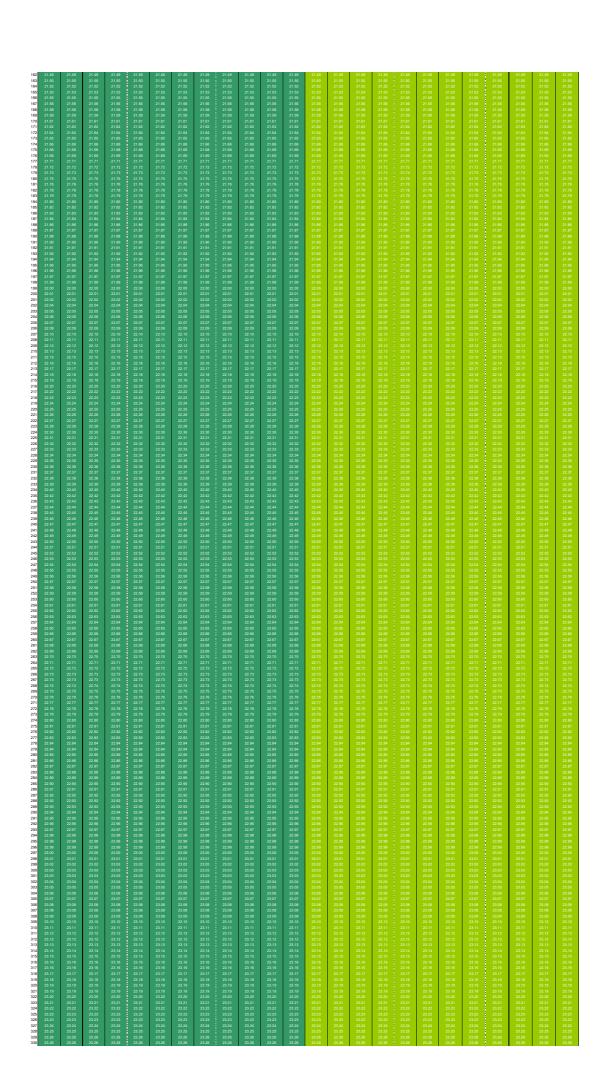


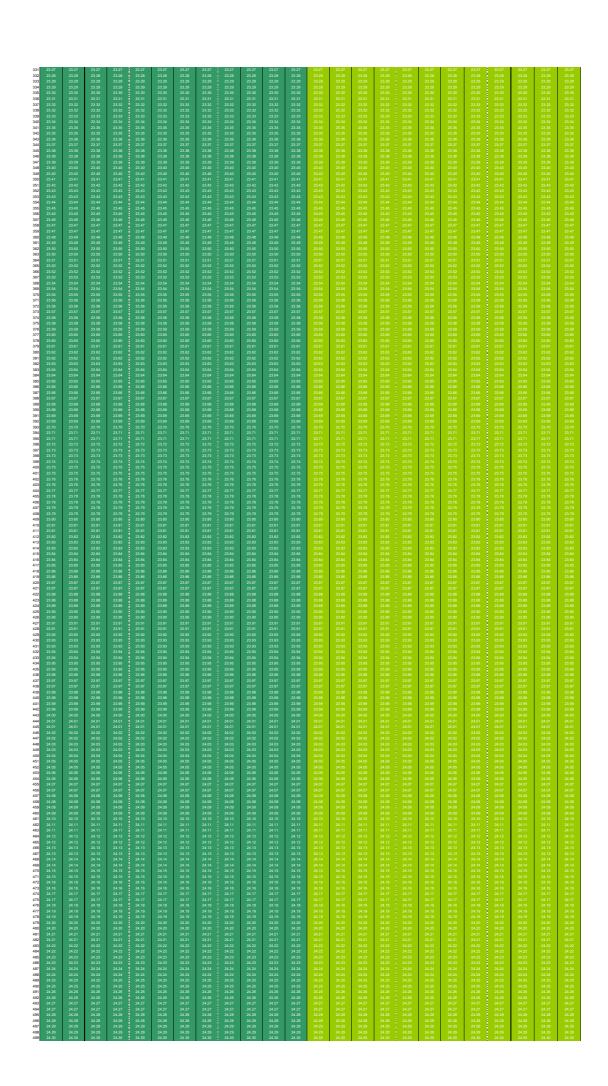


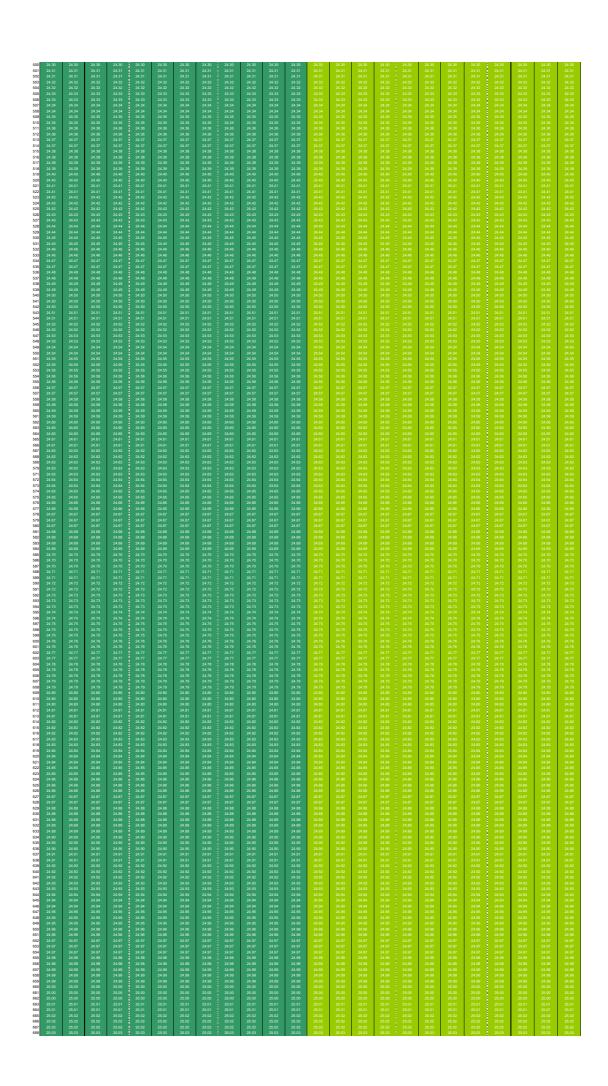
<u>Calculation of wind speed ratios</u>
Note: Wind speed ratios derived from WINDFLOW model (Gardiner, 2004)

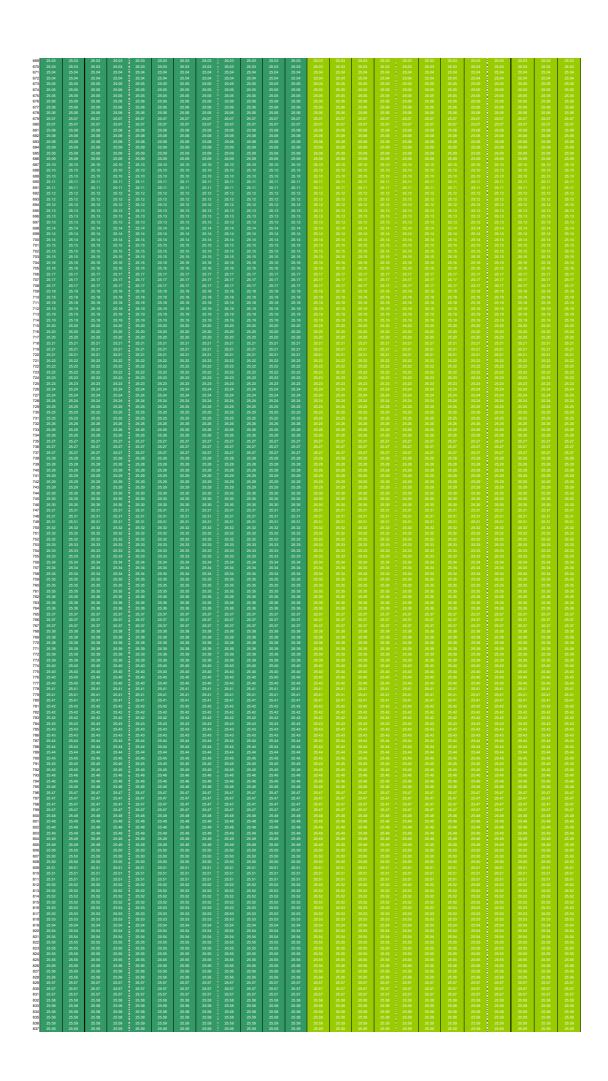
Values taken from input sheet	Fo	restry Are		Fo			Fo	restry Are	a 3	Fo	restry Are		Forestry Area 5			
sneet	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	
Age of forestry when felled for windfarm (yr)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Years after felling when replanting occurs		0	0	0	0	0	0			0	0	0	0	0		
Age of seedlings on planting (yr)		0	0	0	0	0	0			0	0	0	0	0		
Life time of wind farm (years)		40	40	40	40	40	40			40	40	40	40	40		
Area felled around each turbine (ha)		0	0	0	0	0	0			0	0	0	0	0		
Width of forest around felled area (m)		0	0	0	0	0	0			0	0	0	0	0		
Height of turbines (m)		0	0	0	0	0	0	0	0	0	0	0	0	0	0	
Forest dimensions	F.	restry Are	n 1	E.	restry Are	2.2		restry Are	- 2	- F.	restry Are	2.4	E.	restry Are		
rorest dimensions	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	
Width of forest around felled area (m) Width of felled forestry		0	0	0	0	0	0	0	0	0	0	0	0	0	0	
around turbine (m)		0	0	0	0	0	0			0	0	0	0	0		
Tree height at construction of windfarm (m)		0.00	0.00	0.00	0.00	0.00	0.00			0.00	0.00	0.00	0.00	0.00		
Final Height of replanted forestry (m)		18.04	18.04	18.04	18.04	18.04	18.04			18.04	18.04	18.04	18.04	18.04		
Tree height at end of windfarm life (m)	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	18.04	
Wind speed	Forestry Area 1			Forestry Area 2				Forestry Area 3			Forestry Area 4			Forestry Area 5		
	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	
Wind speed upwind from forestry at hub height (m s ⁻²)		nwind of fo	owind of for	wind of fo	wind of for	nwind of fo	owind of fo	wind of fo	wind of for	wind of fo	wind of fo	nwind of fo	wind of fo	wind of for	wind of	
Wind speed at back of forest at hub height (m s ⁻²)		back of fo	back of for	back of fo	back of fo	back of fo	back of fo	back of fo	back of for	back of fo	back of fo	back of fo	back of fo	back of for	back of	
Wind speed over felled bare ground at hub height (m s ⁻²)		d in felled	d in felled g	d in felled (d in felled o	in felled	d in felled o	d in felled (d in felled g	d in felled (d in felled (d in felled	cd in felled o	d in felled o	d in felle	
Wind speed over replanted forestry at hub height (m s ⁻²)		replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replanted	replant	
RESULTS Wind													ı			
speed ratios (used in worksheet 1)		restry Are		Forestry Area 2			Forestry Area 3			Forestry Area 4			Forestry Area 5			
Standard Forestry Practice	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	Exp	Min	Max	
No felling	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE	#VALUE!	#VALUE!	#VAL	
Felled	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE	#VALUE!	#VALUE!	#VALU	
Felled & replanted	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE	#VALUE!	#VALUE!	#VALU	

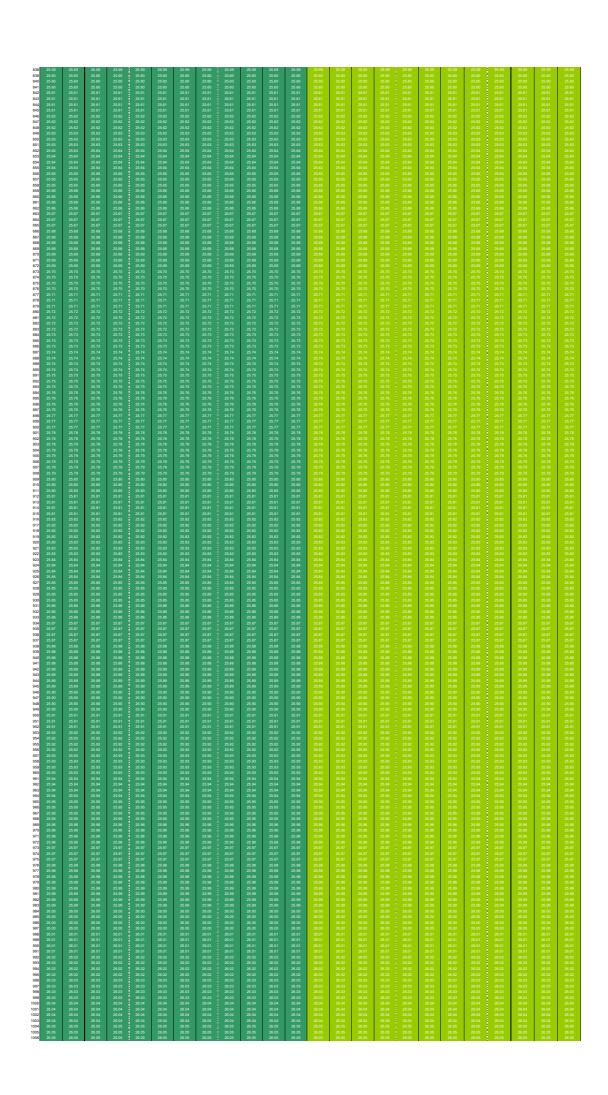
Parameters	F	orestry Area	1	F	orestry Area	2	F	orestry Area	3	F	orestry Area	4	Forestry Area 5		
Parameters	Exp	Min	Max	Exp	Min	Max									
Roughness of upstream ground (m)				0.03	0.03	0.03			0.03	0.03	0.03	0.03			0.03
Roughness of ground in gap (m)				0.03	0.03	0.03			0.03	0.03	0.03	0.03			0.03
Roughness of forest (m)				1.35	1.35	1.35			1.35	1.35	1.35	1.35			1.35
Roughness of SRF (m)				1.35	1.35	1.35			1.35	1.35	1.35	1.35			1.35
Zero plane displacement over forest (m)				11.72	11.72	11.72			11.72	11.72	11.72	11.72			11.72
Zero plane displacement over SRF (m)				11.72	11.72	11.72			11.72	11.72	11.72	11.72			11.72
Exponential decay factor for wind profile in forest (alpha)				4	4	4			4	4	4	4			4
Maximum height of top of boundary layer (m)				5000	5000	5000	5000	5000	5000	5000	5000	5000	5000	5000	5000
Von Karman's constant				0.4	0.4	0.4			0.4	0.4	0.4	0.4			0.4
Intermediate Calculations															
Height of the new internal boundary layer over forest (m)				12	12	12			12	12	12	12			12
Height of the new internal boundary layer over felled area (m)				0	0	0			0	•	0	0			0
Height of the new internal boundary layer over replanted area (m)				12	12	12			12	12	12	12			12
Windspeed at internal boundary layer over forest (m s ⁻¹)				15	15	15			15	15	15	15			15
Windspeed at internal boundary layer over felled area (m s 1)	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!	#VALUE!									
Windspeed at internal boundary layer over replanted area (m s ¹)				15	15	15			15	15	15	15			15

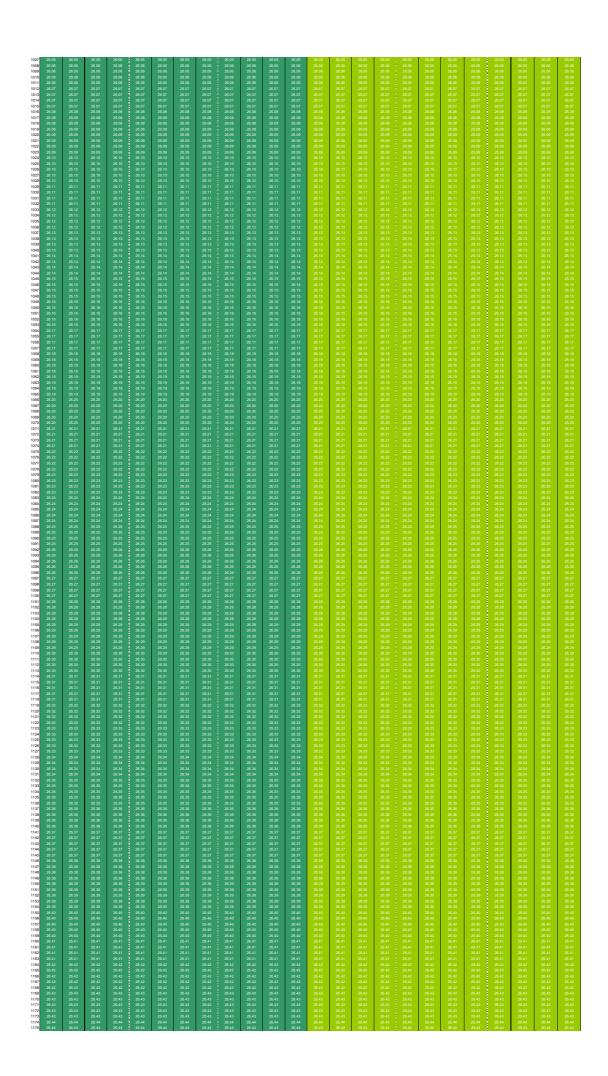


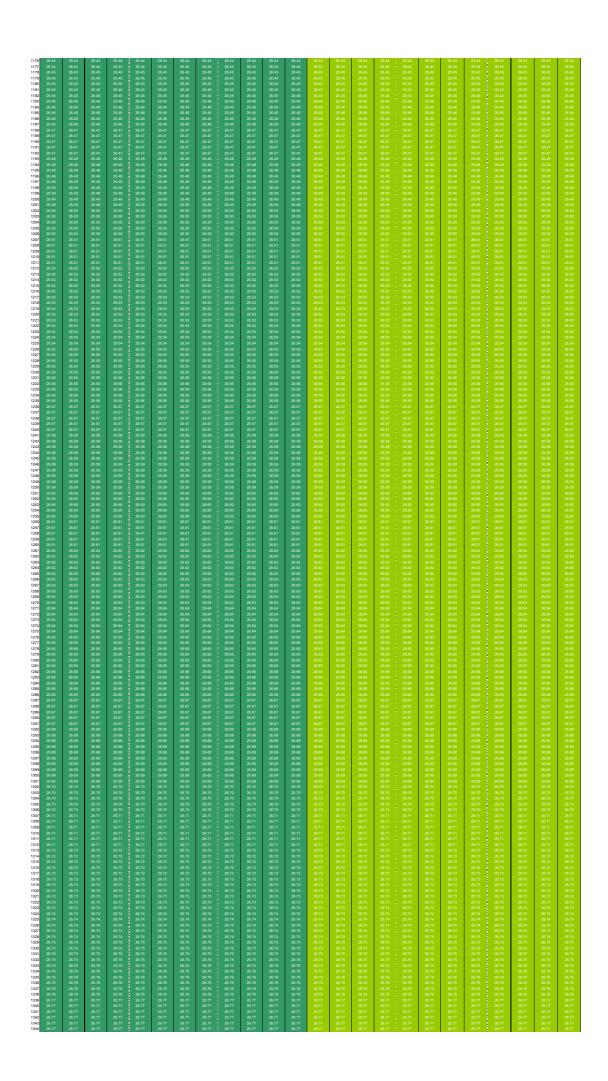


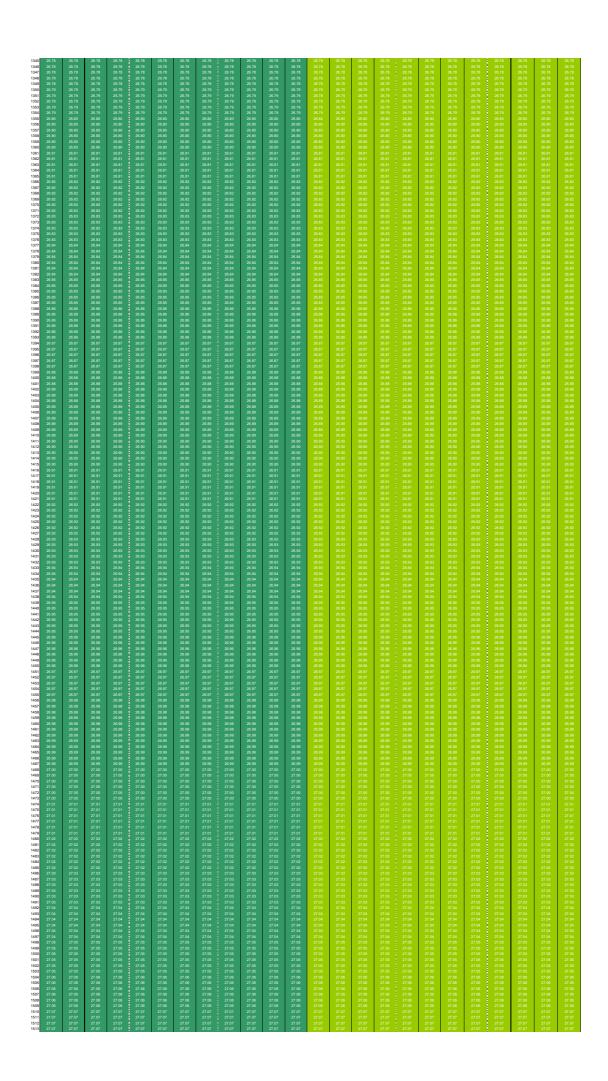


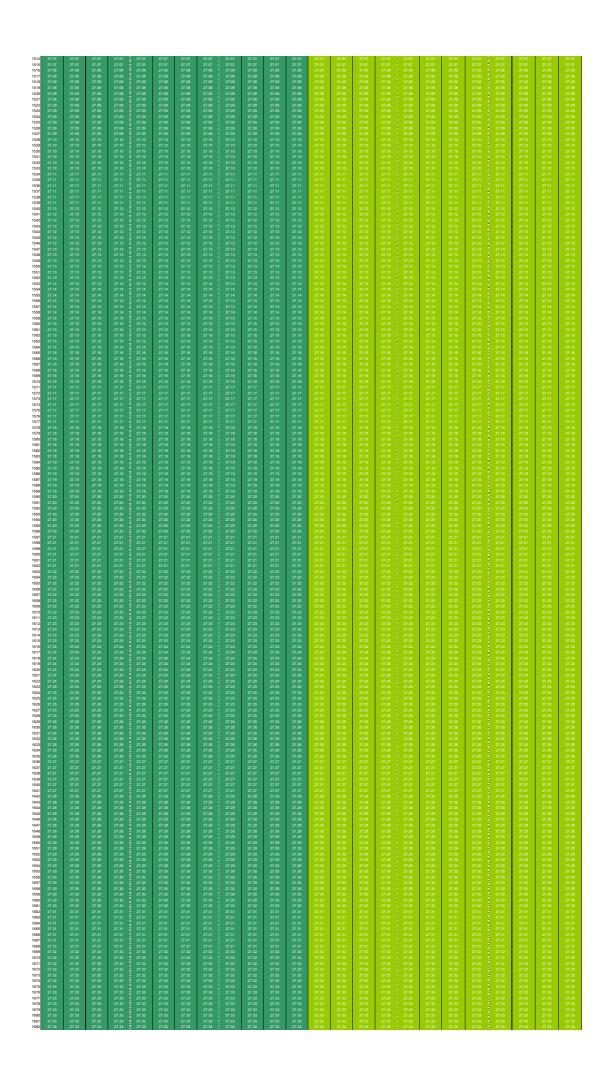


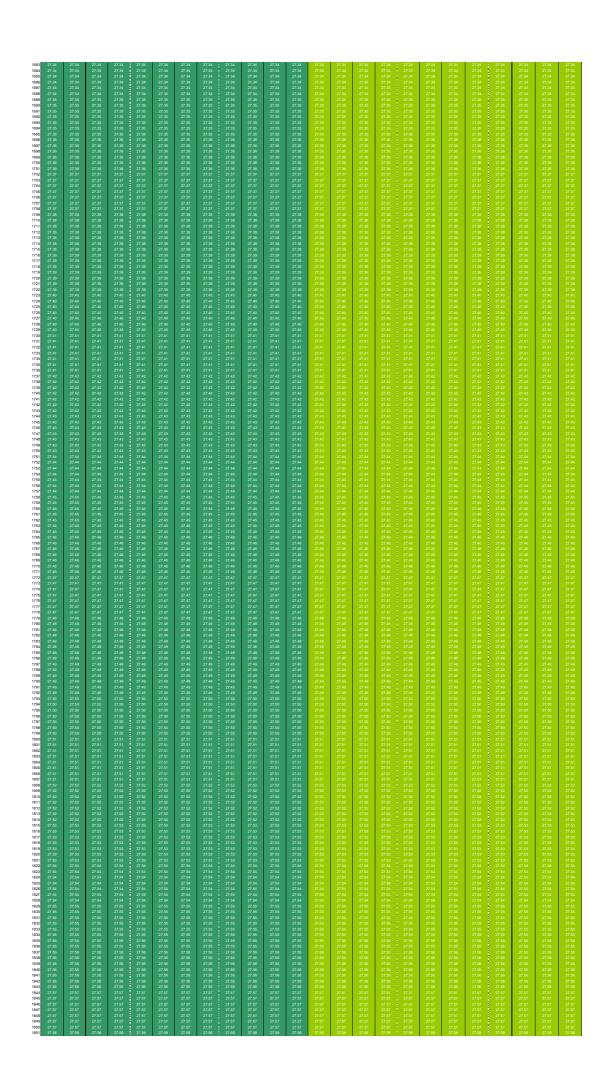


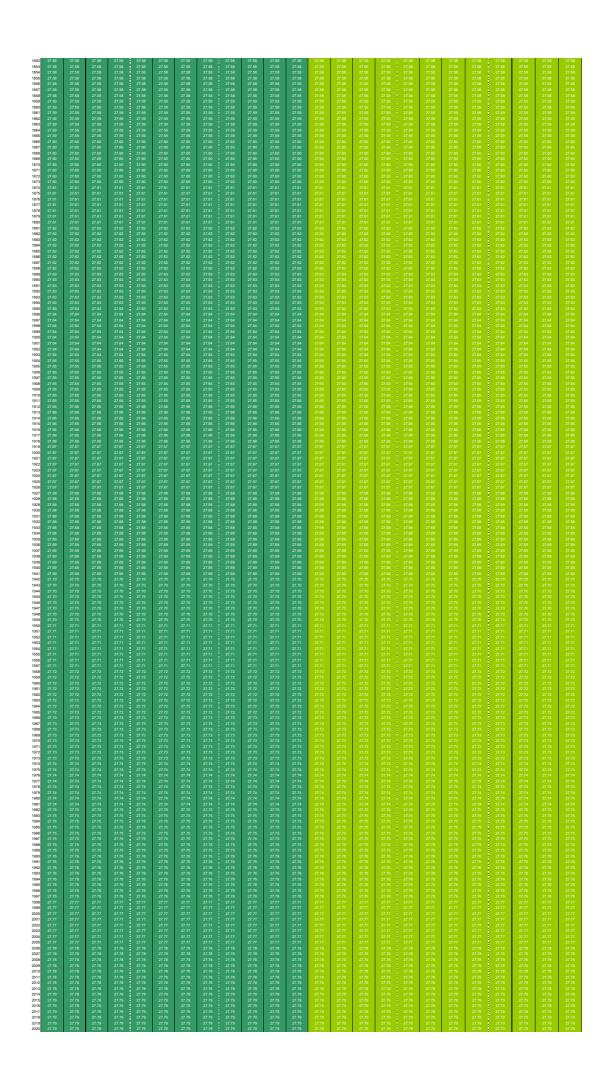


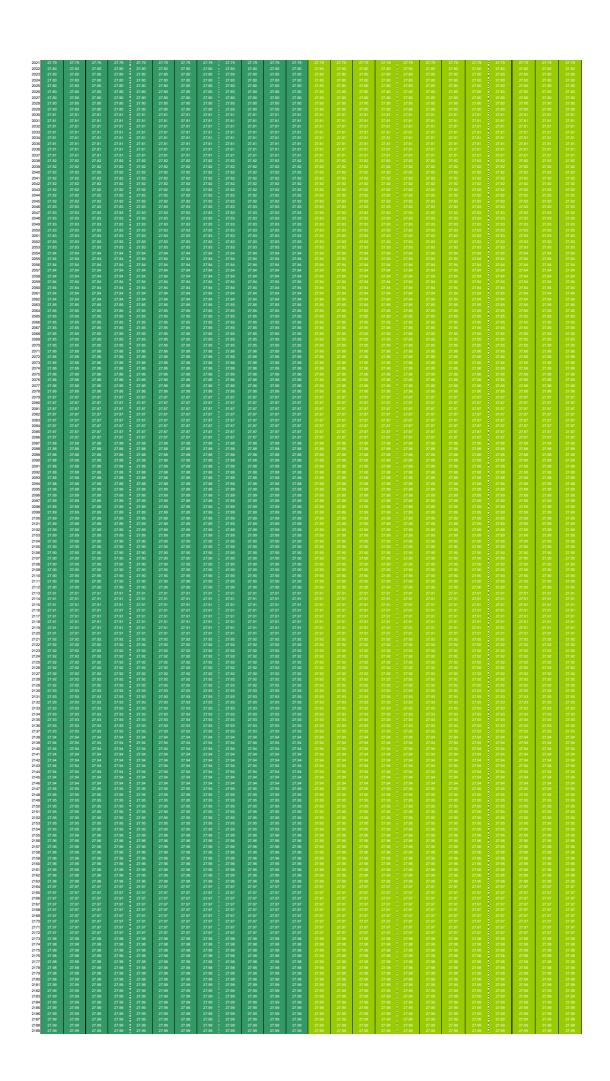


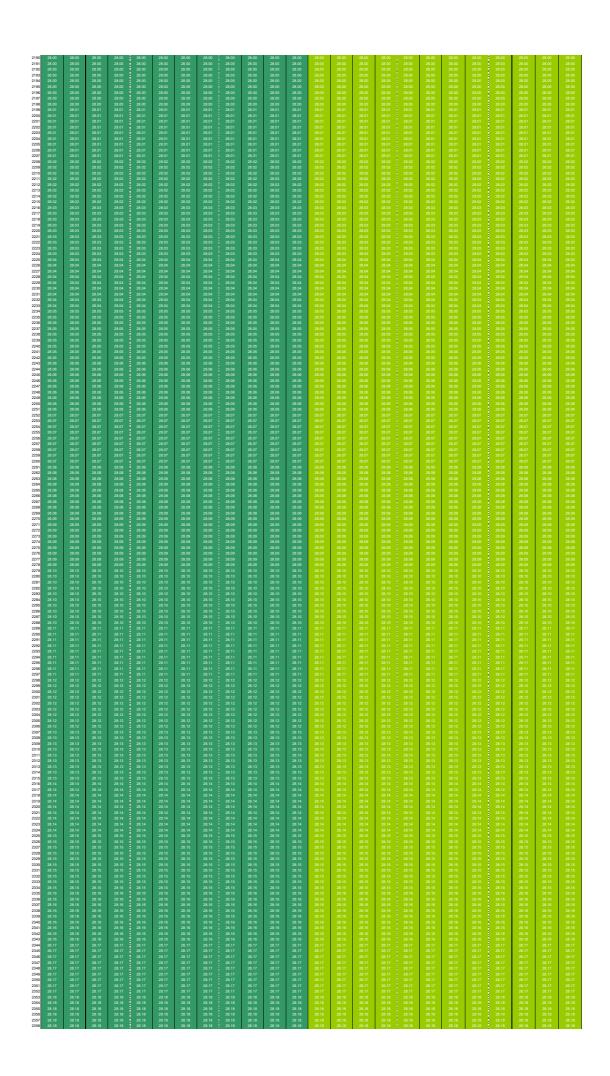


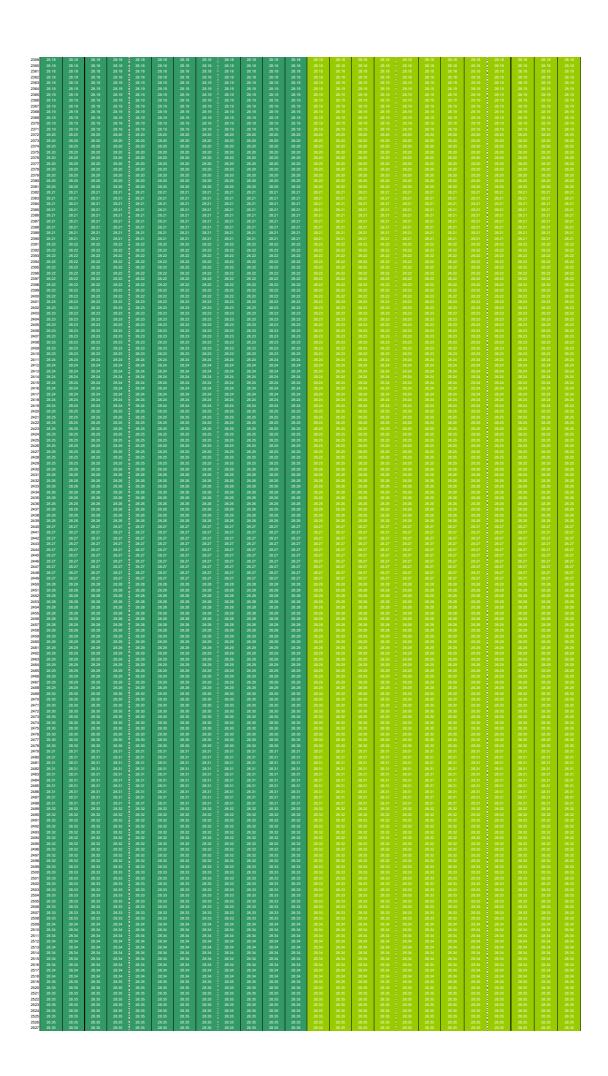


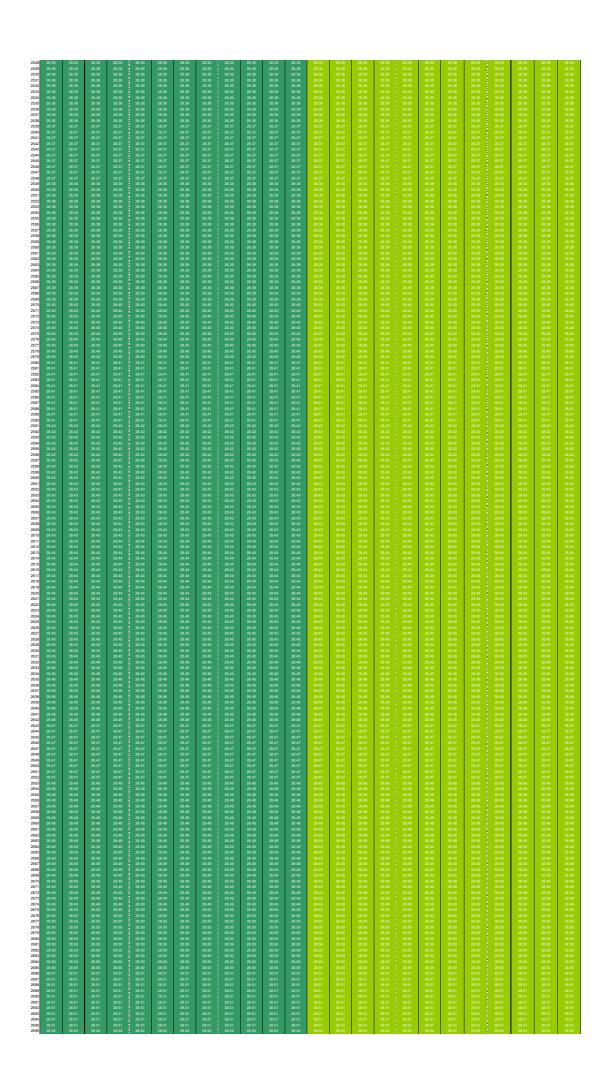


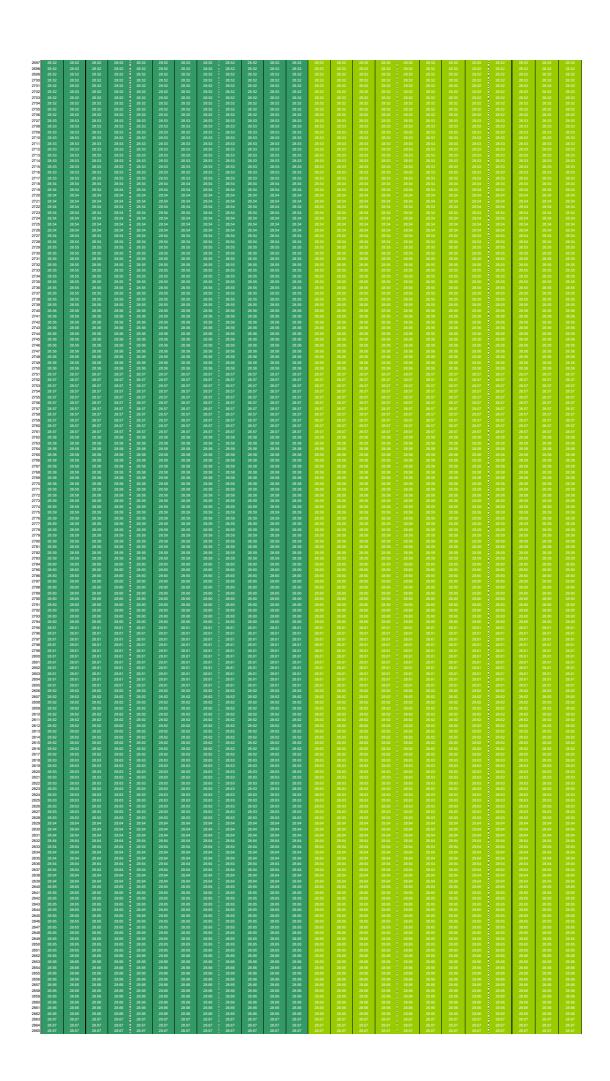


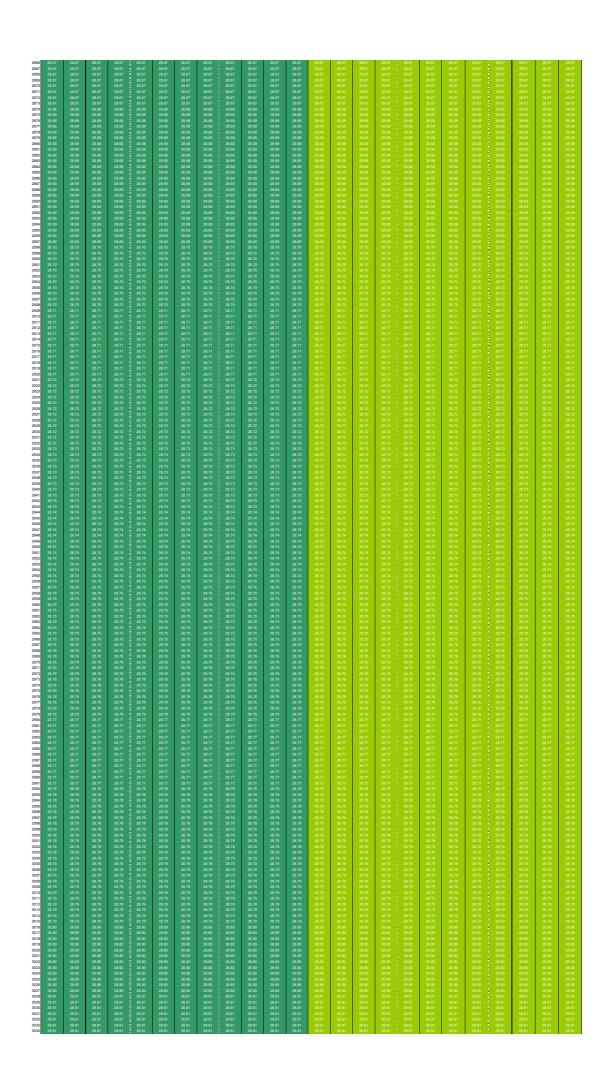


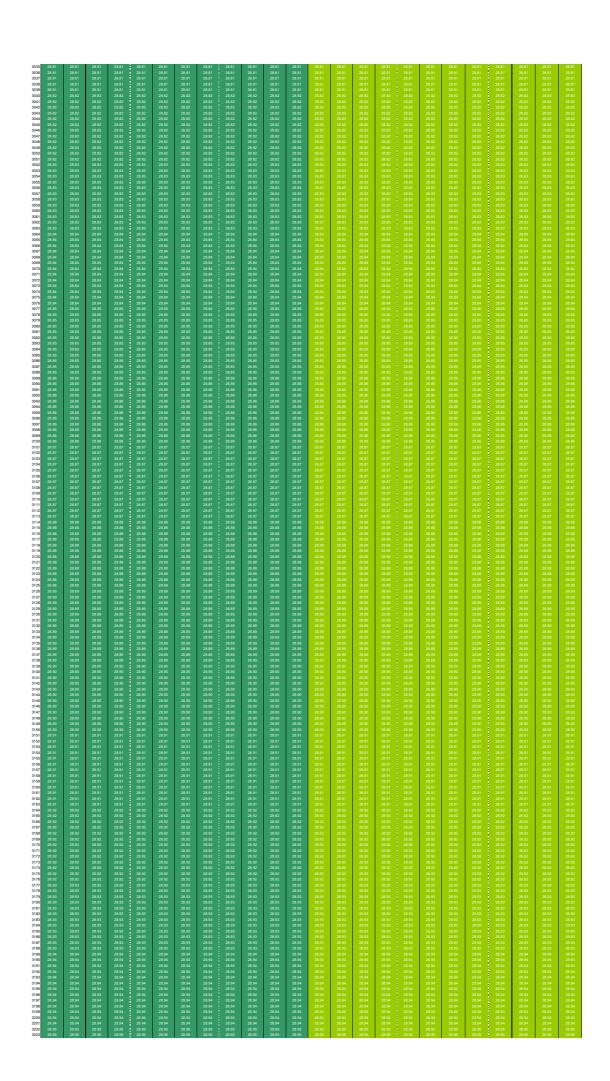


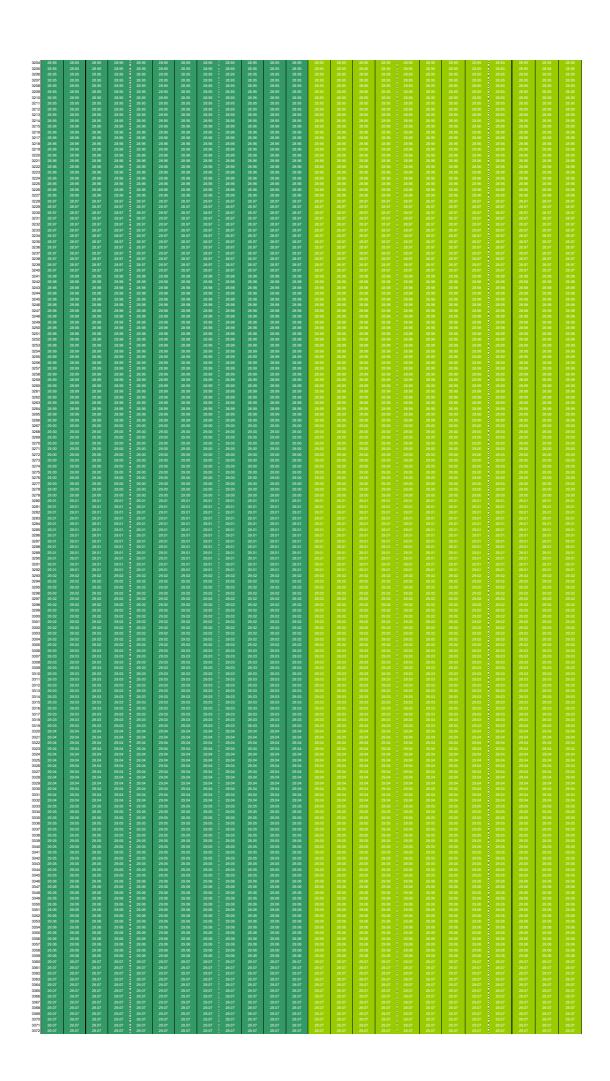


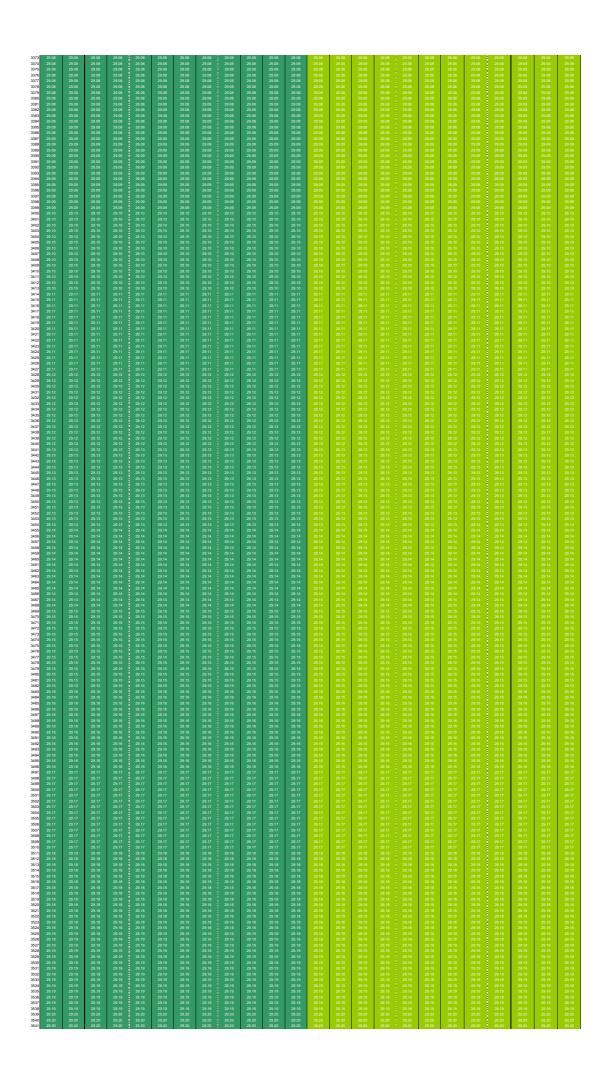


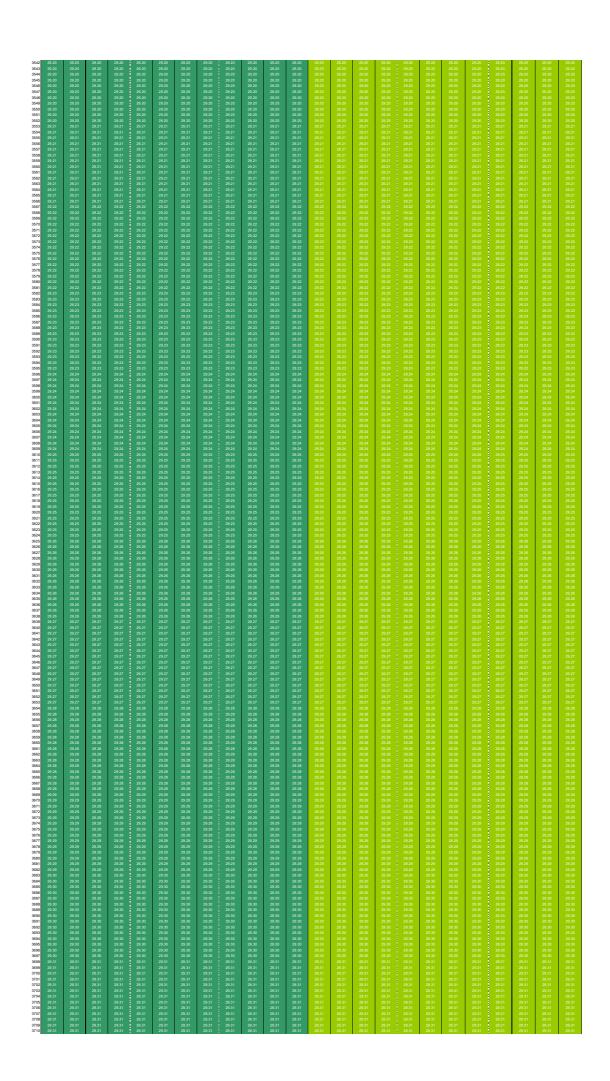


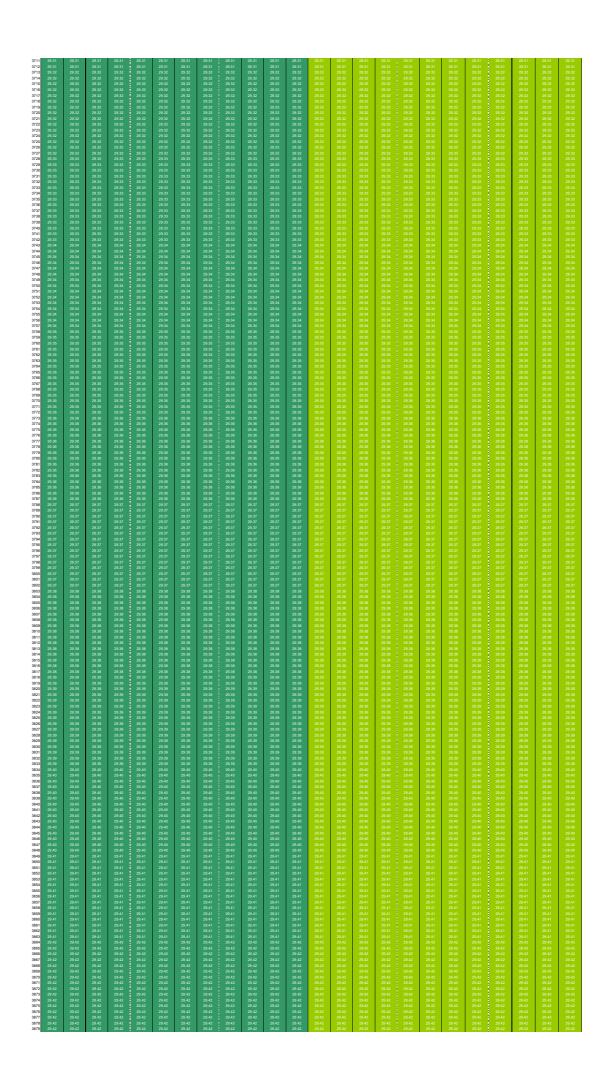


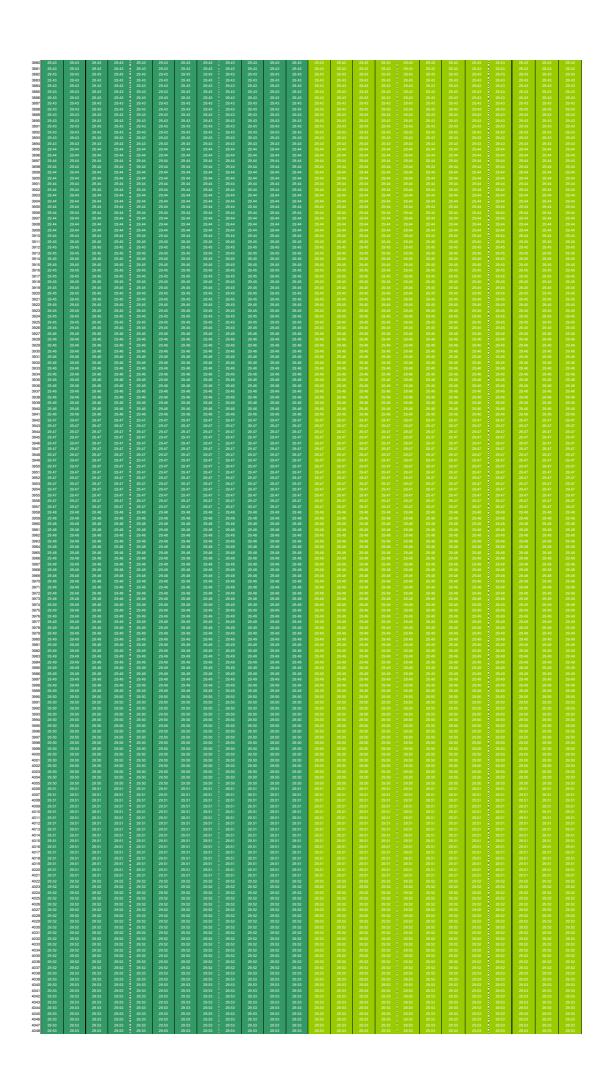


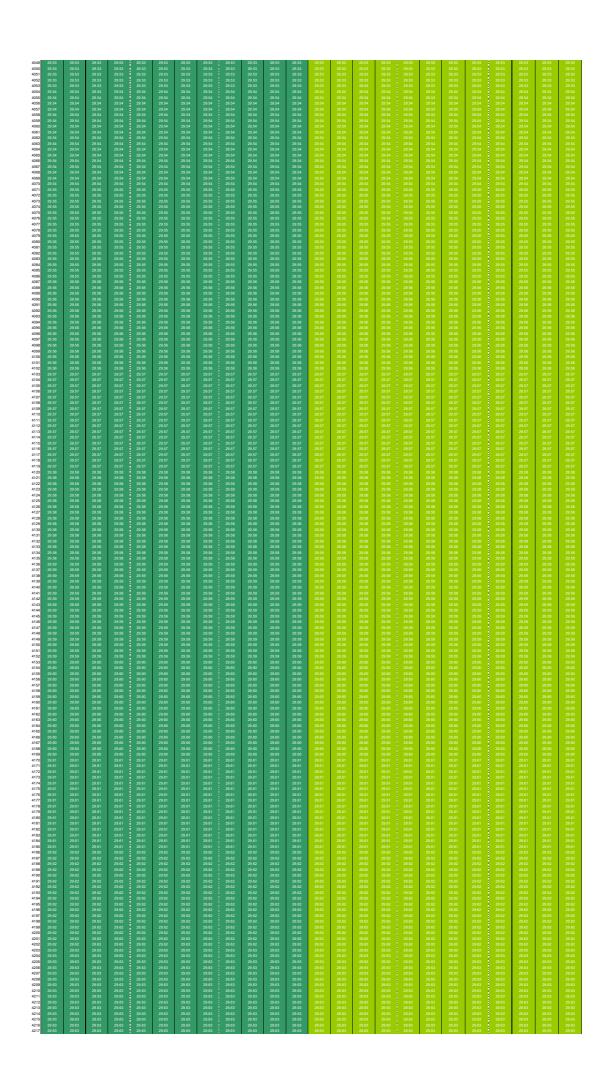


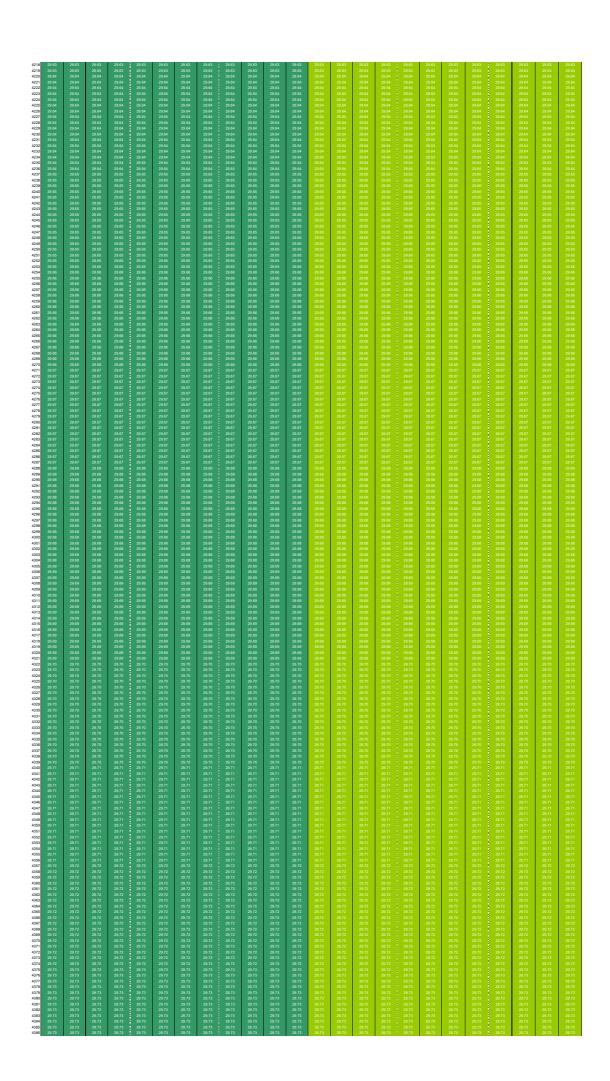


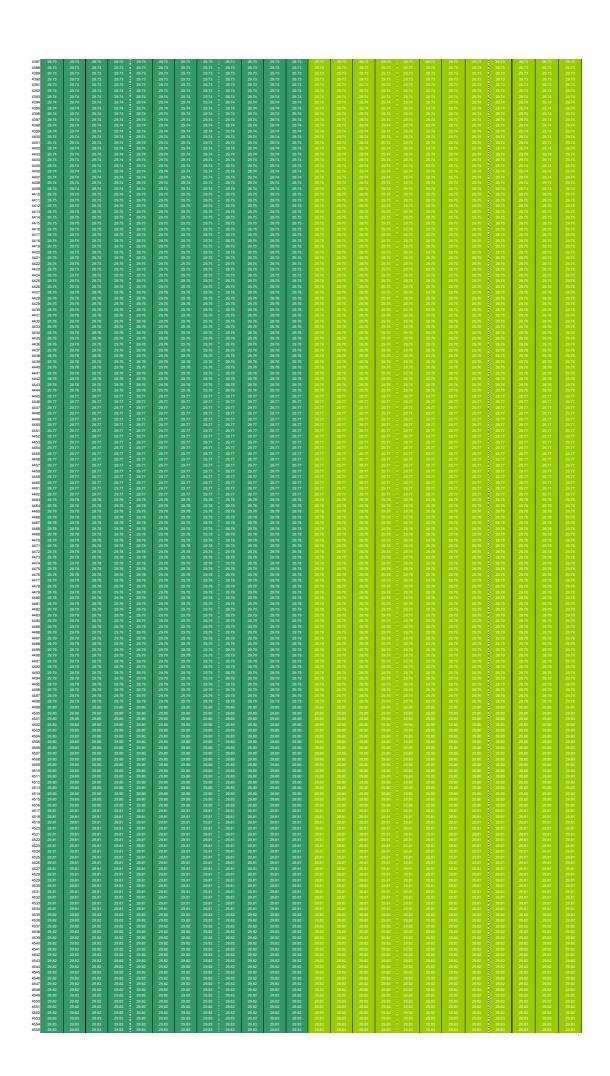


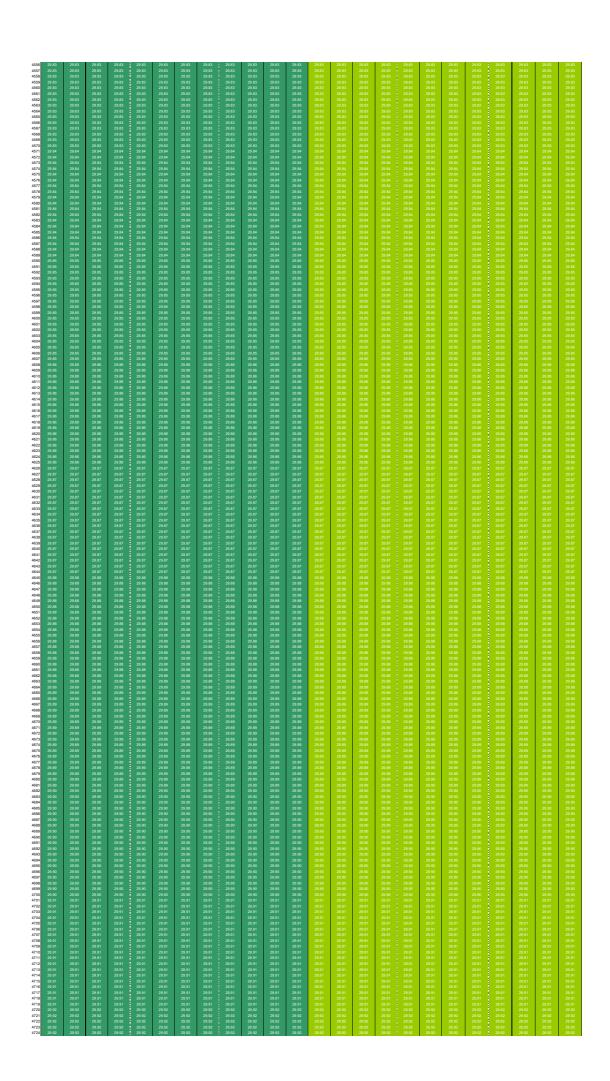


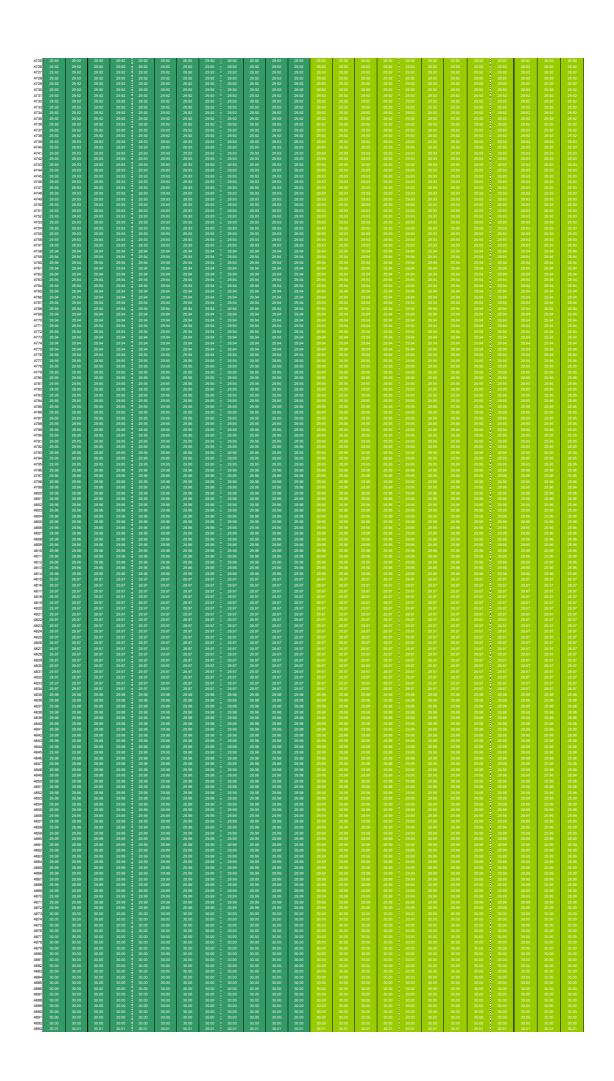






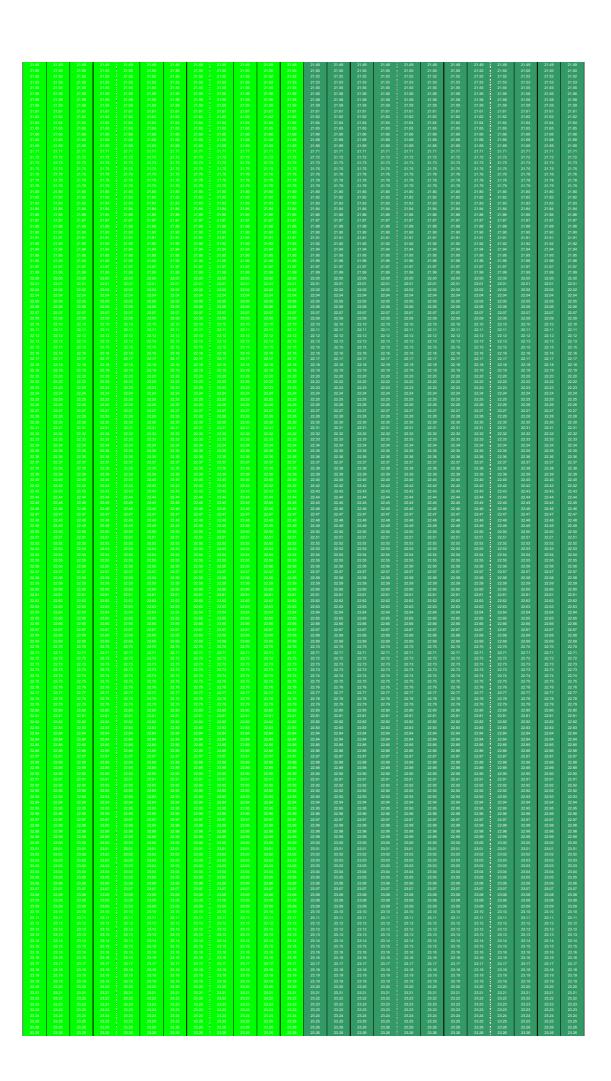




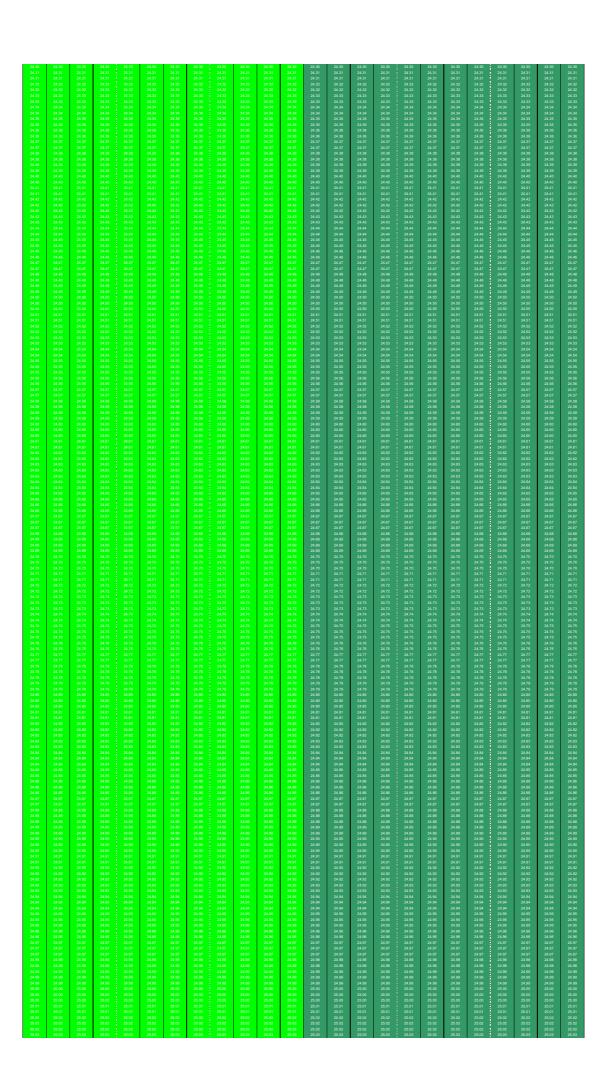


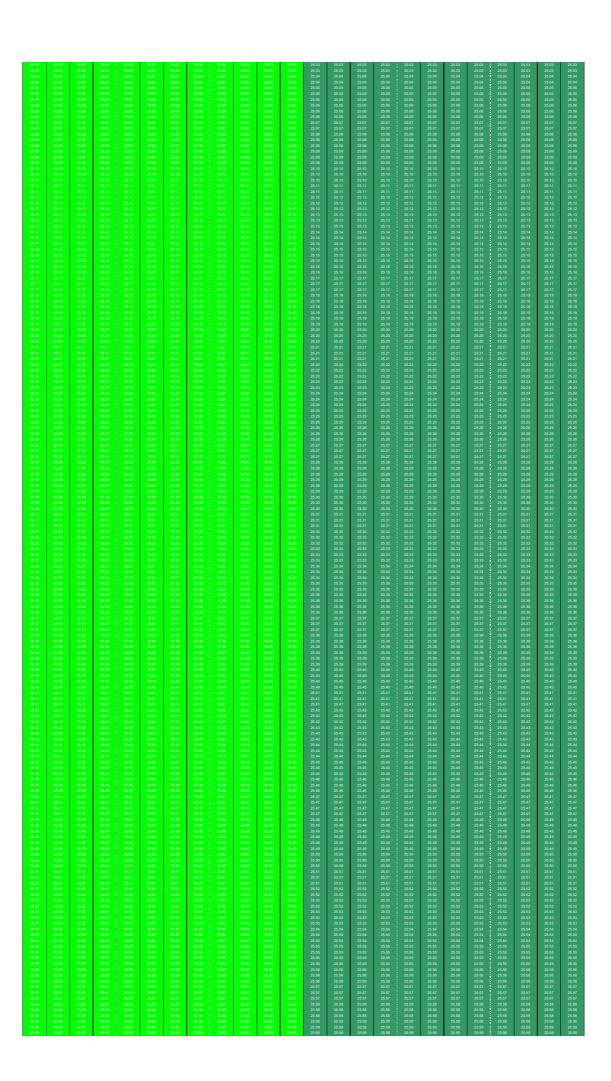
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4895 4896	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01	30.01 30.01		30.01 30.01		30.01 30.01		30.01 30.01 30.01 30.01	30.01	30.01 30.01	30.01 30.01
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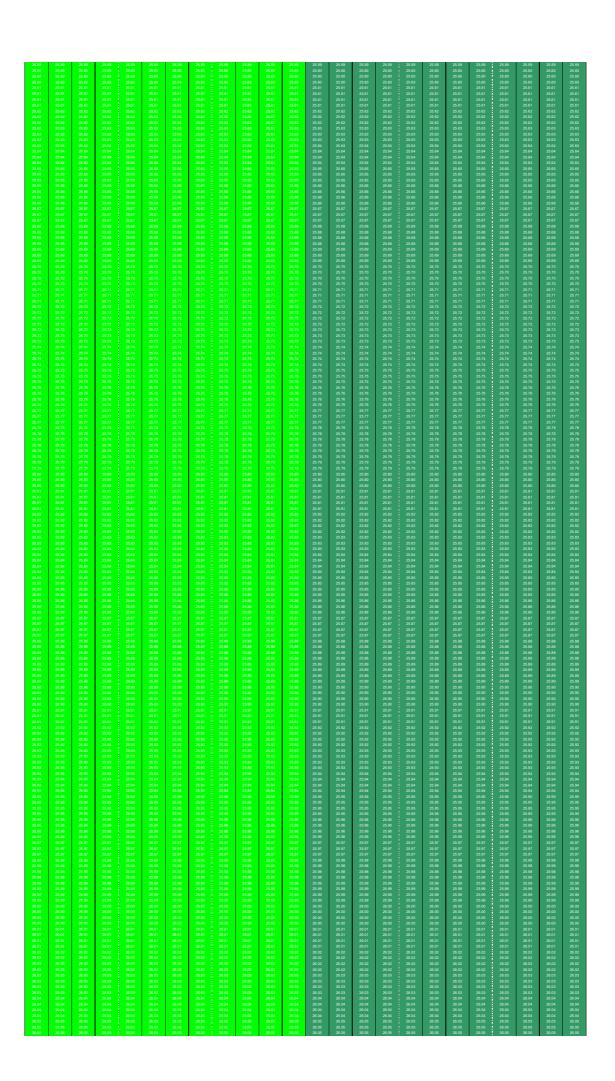
	E	хр			Forestr M	y Area 3 lin			м.	ox			E)	up.			Forestr M	y Area 4 lin			м	ax	
Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m s ⁻¹)	Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m s ⁻¹)	Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m s ⁻¹)	Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m s ⁻¹)	Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m. s ⁻¹)	Wind speed upwind of forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	Wind speed over replanted forestry (m s ⁻¹)
8.77 10.50 11.51 12.23 12.79 13.25	#NUME #NUME #NUME #NUME #NUME #NUME	#NUM! #NUM! #NUM! #NUM! #NUM!	-2.10 2.71 5.53 7.52 9.07		#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	-2.10 2.71 5.53 7.52 9.07	8.77 10.50 11.51 12.23 12.79	#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	-2.10 2.71 5.53 7.52 9.07	8.77 10.50 11.51 12.23 12.79	MUN# MUN# MUN# MUN#	#NUM! #NUM! #NUM! #NUM! #NUM!	-2.10 2.71 5.53 7.52 9.07	8.77 10.50 11.51 12.23 12.79	#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	-2:10 2:71 5:53 7:52 9:07	8.77 10.50 11.51 12.23 12.79	#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	-2.10 2.71 5.53 7.52 9.07 10.33
13.63 13.96 14.26	#NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	9.07 10.33 11.40 12.33 13.15		#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	9.07 10.33 11.40 12.33 13.15		#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	9.07 10.33 11.40 12.33 13.15	12.79 13.25 13.63 13.96 14.26	#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM! #NUM!	10.33 11.40 12.33 13.15	12.79 13.25 13.63 13.96 14.26	#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	9.07 10.33 11.40 12.33 13.15	12.79 13.25 13.63 13.96 14.26	#NUM! #NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM! #NUM!	10.33 11.40 12.33 13.15 13.88
14.52 14.76 14.98 15.18 15.36 15.54	#NUM! #NUM! 14.98 15.18 15.36	#NUM! #NUM! 14.98 15.18 15.36	13.88 14.54 14.98 15.18 15.36		#NUM! 14.98 15.18	#NUM! 14.98 15.18	13.88 14.54 14.98 15.18 15.36		#NUM! #NUM! 14.98 15.18 15.36	#NUM! 14.98 15.18	13.88 14.54 14.98 15.18 15.36	14.52 14.76 14.98 15.18 15.36	#NUM! #NUM! 14.98 15.18 15.36	#NUM! 14.98 15.18	13.88 14.54 14.98 15.18 15.36	14.52 14.76 14.98 15.18 15.36	#NUM! #NUM! 14.98 15.18 15.36	#NUM! #NUM! 14.98 15.18 15.36	13.88 14.54 14.98 15.18 15.36	14.52 14.76 14.98 15.18 15.36	#NUM! #NUM! 14.98 15.18 15.36	#NUM! 14.98 15.18	13.88 14.54 14.98 15.18 15.36 15.54
15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99		15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99		15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.36 15.54 15.70 15.85 15.99	15.70 15.85
16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61		16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61		16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61	16.13 16.26 16.38 16.49 16.61
16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01		16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01		16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01	16.71 16.81 16.91 17.01
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17.51 17.58 17.65	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73		17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73		17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65 17.73	17.51 17.58 17.65
17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05		17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05		17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05	17.79 17.86 17.93 17.99 18.05
18.11	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34		18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34		18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28	18.11 18.17 18.23 18.28	18.11 18.17 18.23 18.28	18.11 18.17 18.23 18.28	18.11 18.17 18.23 18.28	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28 18.34	18.11 18.17 18.23 18.28	18.17 18.23 18.28	18.11 18.17 18.23
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18.60 18.64 18.69 18.74 18.78	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74		18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74	18.60 18.64 18.69 18.74 18.78
18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92	18.78 18.83 18.87 18.92 18.96		18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96	18.78 18.83 18.87 18.92 18.96
19.00 19.04	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12		19.00 19.04 19.08 19.12	18.96 19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12		19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	18.96 19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12	19.00 19.04 19.08 19.12
19.08 19.12 19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28		19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28		19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28	19.16 19.20 19.24 19.28
19.32 19.35 19.39 19.42 19.46 19.49	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46		19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46		19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46	19.32 19.35 19.39 19.42 19.46 19.49
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19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87		19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.78 19.81 19.84 19.87		19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87	19.75 19.78 19.81 19.84 19.87
19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02		19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02		19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02	19.90 19.93 19.96 19.99 20.02
20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12		20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12		20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12	20.04 20.07 20.10 20.12
20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25		20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20:15 20:18 20:20 20:23 20:25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25	20.15 20.18 20.20 20.23 20.25
20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35		20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35		20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35	20.28 20.30 20.33 20.35
20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47		20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47		20.38 20.40 20.42 20.45 20.47	20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47	20.38 20.40 20.42 20.45 20.47
20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56		20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56		20.49 20.52 20.54 20.56 20.58	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.47 20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56 20.58	20.49 20.52 20.54 20.56	20.47 20.49 20.52 20.54 20.56 20.58	20.49 20.52 20.54 20.56 20.58	20.49 20.52 20.54 20.56	20.49 20.52 20.54 20.56
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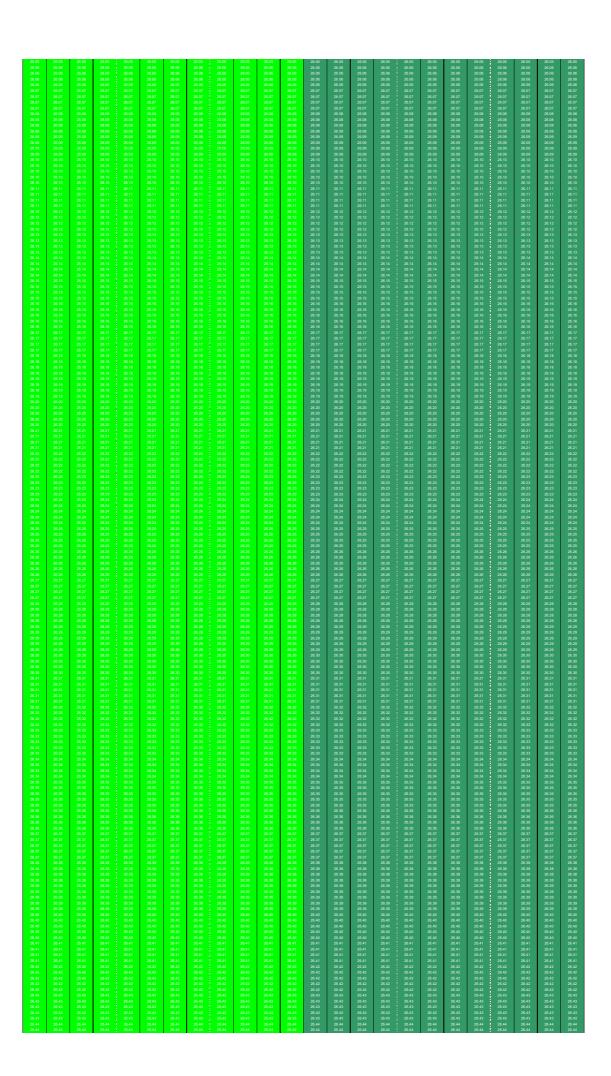


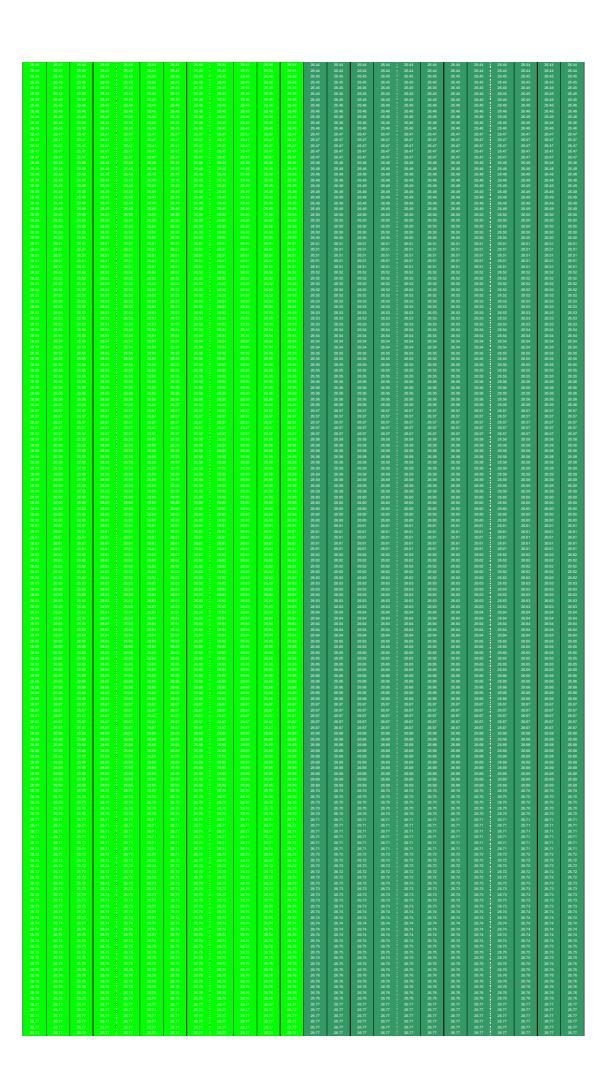
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		23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63 23.64 23.64	23.62 23.62 23.63	23.61 23.62 23.62 23.63 23.64 23.64		23.61 23.62 23.62 23.63 23.64 23.64	23.62 23.62 23.63	23.61 23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.62 23.62 23.63 23.63	23.62 23.62 23.63	23.62 23.62 23.63	23.62 23.62 23.63
		23.64 23.64 23.65	23.64 23.64 23.65		23.64 23.64 23.65	23.64 23.64 23.65	23.64 23.64 23.65		23.64 23.64 23.65	23.64 23.64 23.65	23.64 23.64 23.65	23.64 23.64	23.64 23.64	23.64 23.64	23.64 23.64	23.64 23.64	23.64 23.64	23.64 23.64 23.65	23.64 23.64 23.64 23.64 23.65 23.65	23.64 23.64 23.65	23.64 23.64	23.64 23.64
		23.66	23.66 23.66	23.66 23.66	23.66 23.66	23.66 23.66	23.66 23.66		23.66 23.66	23.66 23.66	23.66	23.65 23.66 23.66	23.65 23.66 23.66 23.67	23.65 23.66 23.66	23.65 23.66 23.66	23.65 23.66 23.66	23.65 23.66 23.66	23.66 23.66	23.66 23.66 23.66 23.66	23.66 23.66	23.65 23.66 23.66	23.65 23.66 23.66 23.67
23.67 23.68 23.68		23.67 23.68 23.68 23.69 23.69	23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68 23.69 23.69	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68 23.69 23.69	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.67 23.68 23.68 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68	23.67 23.68 23.68
		23.69 23.69	23.69 23.69		23.68 23.68 23.69 23.69	23.68 23.68 23.69 23.69	23.69 23.69	23.68 23.68 23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69	23.68 23.68 23.69 23.69 23.70 23.71	23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69 23.69 23.69	23.69 23.69	23.69 23.69	23.69 23.69
		23.70 23.71 23.71 23.72	23.70 23.71 23.71		23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71 23.72		23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71 23.72		23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71		23.70 23.71 23.71	23.70 23.71 23.71	23.70 23.71 23.71
		23.72 23.73 23.73	23.72 23.73 23.73		23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73		23.72 23.73 23.73	23.72 23.73 23.73	23.71 23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73	23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.72 23.73 23.73 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73	23.72 23.73 23.73
		23.74 23.75	23.74 23.75		23.74 23.75 23.75	23.74 23.75	23.74 23.75		23.74 23.75	23.74 23.75	23.74 23.75 23.75	23.74 23.75	23.74 23.75	23.74 23.75	23.74 23.75	23.74 23.75	23.74 23.75	23.74 23.75	23.74 23.74 23.75 23.75	23.74 23.75	23.74	23.74
		23.75 23.76 23.76	23.75 23.76 23.76		23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76		23.75 23.76 23.76	23.75 23.76 23.76	23.76	23.75 23.76 23.76	23.73 23.74 23.75 23.75 23.76 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.75 23.76 23.76 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76	23.75 23.76 23.76
		23.77 23.78 23.78 23.79	23.77 23.78		23.77 23.78	23.77 23.78	23.77 23.78 23.78 23.79		23.77	23.77 23.78	23.77 23.78 23.78 23.79	23.77 23.78	23.77 23.78	23.77 23.78	23.77 23.78	23.77 23.78	23.77 23.78	23.77 23.78	23.77 23.77 23.78 23.78	23.77 23.78	23.77 23.78	23.77 23.78
		23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80		23.78 23.79 23.79 23.80	23.78 23.79 23.79	23.78 23.79 23.79 23.80		23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.78 23.79 23.79 23.79 23.79 23.80 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79
		23.80 23.81 23.81	23.80 23.81 23.81		23.80 23.81 23.81	23.79 23.80 23.81 23.81	23.80 23.81 23.81		23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.79 23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.80 23.81 23.81 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.79 23.80 23.81 23.81
		23.82	23.82 23.83		23.82 23.83	23.82 23.83	23.82	23.82 23.83	23.82	23.82 23.83	23.82	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.82 23.83 23.83	23.82 23.83	23.82 23.83	23.82 23.83
	23.83 23.84 23.84	23.83 23.84 23.84 23.85	23.83 23.84 23.84		23.83 23.84 23.84 23.85	23.83 23.84 23.84	23.84 23.84 23.85		23.83 23.84 23.84 23.85	23.83 23.84 23.84	23.83 23.83 23.84 23.84 23.85	23.83 23.84 23.84	23.83 23.84 23.84 23.85	23.83 23.84 23.84	23.83 23.84 23.84	23.83 23.84 23.84	23.83 23.84 23.84	23.83 23.84 23.84	23.83 23.83 23.84 23.84 23.84 23.84	23.83 23.84 23.84	23.83 23.84 23.84	23.83 23.84 23.84 23.85
		23.86	23.84 23.85 23.86		23.86	23.84 23.85 23.86	23.86		23.86	23.84 23.85 23.86	23.86	23.84 23.85 23.86	23.85 23.86 23.86	23.84 23.85 23.86 23.86	23.84 23.85 23.86 23.86	23.84 23.85 23.86	23.84 23.85 23.86	23.84 23.85 23.86	23.84 23.84 23.85 23.85 23.86 23.86	23.84 23.85 23.86	23.84 23.85 23.86 23.86	23.85 23.86 23.86
		23.86 23.87 23.87	23.86 23.87 23.87		23.86 23.87 23.87	23.86 23.87 23.87	23.86 23.87 23.87		23.86 23.87 23.87	23.86 23.87 23.87	23.86 23.87 23.87	23.86 23.87 23.87	23.87 23.87	23.87 23.87	23.87 23.87	23.86 23.87 23.87	23.86 23.87 23.87	23.86 23.87 23.87	23.86 23.86 23.87 23.87 23.87 23.87	23.86 23.87 23.87	23.87 23.87	23.87 23.87
		23.88 23.88	23.88 23.88	23.88 23.88	23.88 23.88	23.88	23.88 23.88	23.88 23.88	23.88 23.88	23.88 23.88	23.88 23.88	23.88 23.88 23.89	23.88 23.88	23.88 23.88 23.89	23.88 23.88 23.89	23.88 23.88 23.89	23.88 23.88 23.89	23.88 23.88 23.89	23.88 23.88 23.88 23.88 23.89 23.89	23.88 23.88 23.89	23.88 23.88 23.89	23.88 23.88
		23.89 23.90 23.90	23.89 23.90 23.90		23.89 23.90 23.90	23.89 23.90 23.90 23.91	23.89 23.90 23.90		23.89 23.90 23.90	23.89 23.90 23.90	23.89 23.90 23.90	23.90 23.90	23.89 23.90 23.90	23.90 23.90	23.90 23.90	23.90 23.90	23.90 23.90	23.90 23.90	23.90 23.90 23.90 23.90	23.90 23.90	23.90 23.90	23.89 23.90 23.90
		23.91 23.91 23.92	23.91 23.91 23.92		23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92		23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.91 23.91 23.92 23.92	23.91 23.91 23.92	23.91 23.91 23.92	23.91 23.91 23.92
23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.92 23.93 23.93 23.94	23.92 23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.93 23.93 23.94 23.94	23.93 23.93 23.94	23.93 23.93 23.94	23.93 23.93 23.94
		23.94 23.95	23.94 23.95		23.94 23.95	23.94 23.95	23.94 23.95		23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.95	23.94 23.94 23.95 23.95	23.94 23.95	23.94 23.95	23.94 23.95
		23.95 23.96 23.97	23.95 23.96 23.97		23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97		23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.95 23.96 23.96 23.97 23.97	23.95 23.96 23.97	23.95 23.96 23.97	23.95 23.96 23.97
23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98		23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98		23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.97 23.98 23.98 23.98 23.98	23.97 23.98 23.98	23.97 23.98 23.98	23.97 23.98
		23.99 23.99	23.99 23.99		23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.98 23.98 23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99	23.99 23.99 23.99 23.99	23.99 23.99	23.99 23.99	23.98 23.99 23.99
		24.00 24.01 24.01	24.00 24.01 24.01		24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01		24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.00 24.01 24.01 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01	24.00 24.01 24.01
		24.02 24.02	24.02 24.02 24.03	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02		24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02 24.02 24.02	24.02 24.02	24.02 24.02	24.02 24.02
		24.03 24.03 24.04 24.05	24.03 24.04		24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05		24.03 24.03 24.04 24.05	24.03 24.03 24.04	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.03 24.03 24.04 24.04 24.05 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05
		24.05 24.06	24.05 24.05 24.06		24.05 24.05 24.06	24.05 24.05 24.06	24.05 24.06		24.05 24.05 24.06	24.05 24.05 24.06	24.05 24.05 24.06	24.05 24.05 24.06	24.05 24.06	24.05 24.05 24.06	24.05 24.05 24.06	24.05 24.06	24.05 24.05 24.06	24.05 24.06	24.05 24.05 24.06 24.06	24.05 24.05 24.06	24.05 24.06	24.05 24.06
		24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.07	24.06 24.06 24.07 24.07	24.06 24.07	24.06 24.07	24.06 24.07
		24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09		24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09		24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.07 24.08 24.08 24.08 24.08 24.09 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09
		24.09 24.09 24.10	24.09 24.09 24.10		24.09 24.09 24.10	24.09 24.10	24.09 24.09 24.10		24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.10	24.09 24.10	24.09 24.09 24.10 24.10	24.09 24.09 24.10	24.09 24.10	24.09 24.10
		24.11 24.11	24.11 24.11 24.12		24.11 24.11	24.11 24.11	24.11 24.11		24.11 24.11	24.11 24.11	24.11 24.11		24.11 24.11			24.11 24.11				24.11 24.11	24.11 24.11	24.11 24.11
		24.12 24.12 24.13	24.12 24.13		24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13		24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.12 24.12 24.13 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13
		24.13 24.14 24.14	24.13 24.14 24.14		24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14		24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.13 24.14 24.14 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14
		24.15 24.15	24.15 24.15		24.15 24.15	24.15 24.15	24.15 24.15		24.15 24.15	24.15 24.15	24.15 24.15		24.14 24.15 24.15 24.16	24.15 24.15	24.15 24.15	24.15 24.15	24.15 24.15		24.15 24.15 24.15 24.15	24.15 24.15	24.15 24.15	24.15 24.15
		24.16 24.16 24.17 24.17 24.18	24.16 24.16 24.17		24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17		24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17 24.17 24.18	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.16 24.16 24.17 24.17	24.16 24.16 24.17	24.16 24.16 24.17	24.16 24.16 24.17
		24.17 24.18 24.19	24.17 24.18 24.19		24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19		24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.17 24.18 24.18 24.19 24.19	24.17 24.18 24.19	24.17 24.18	24.17 24.18 24.19
		24.19 24.20	24.19 24.20		24.19 24.20	24.19 24.20	24.19 24.20		24.19 24.20	24.19 24.20	24.19 24.20	24.19 24.20	24.19 24.19 24.20 24.20	24.19 24.20	24.19 24.20	24.19 24.20	24.19 24.20	24.19 24.20	24.19 24.19 24.20 24.20	24.19 24.20	24.19 24.19 24.20	24.19 24.20
		24.20 24.21 24.21	24.20 24.21 24.21		24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21		24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.20 24.21 24.21 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21	24.20 24.21 24.21
		24.22 24.22	24.22 24.22		24.22 24.22	24.22 24.22	24.22 24.22		24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22 24.22 24.22	24.22 24.22	24.22 24.22	24.22 24.22
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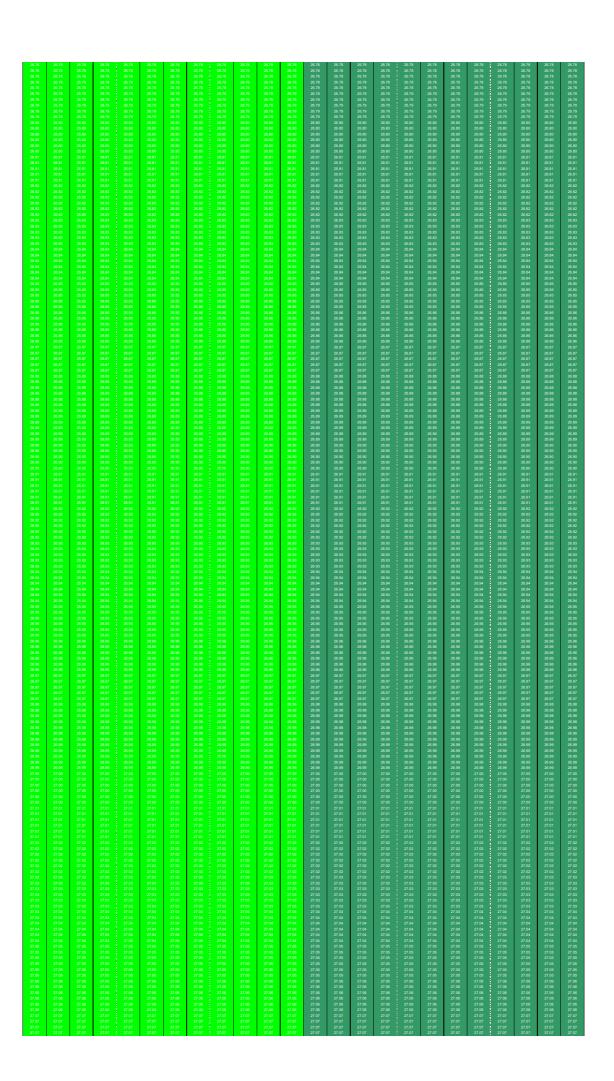




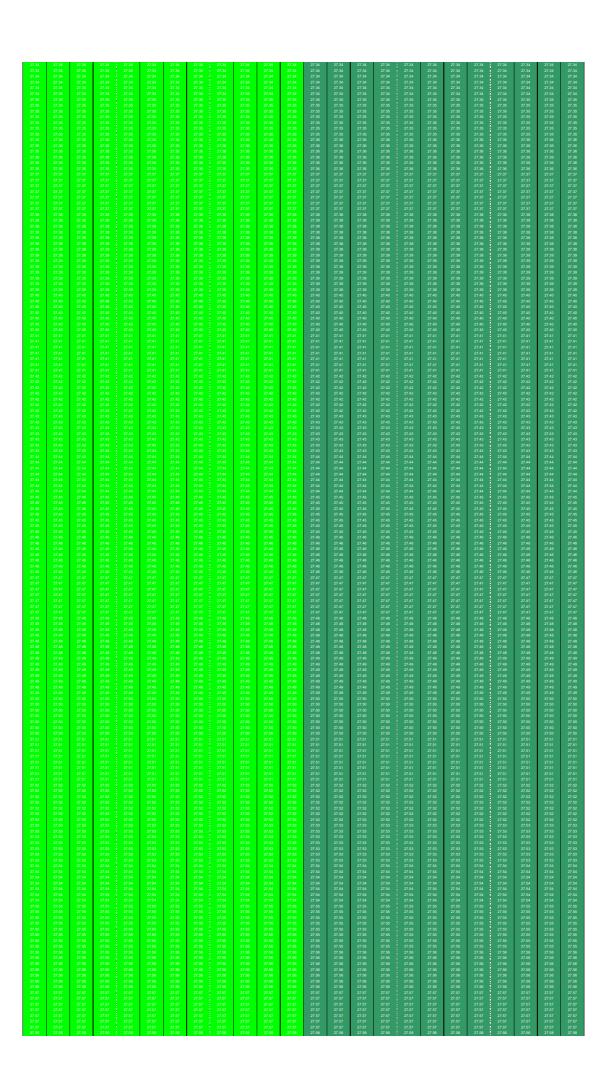






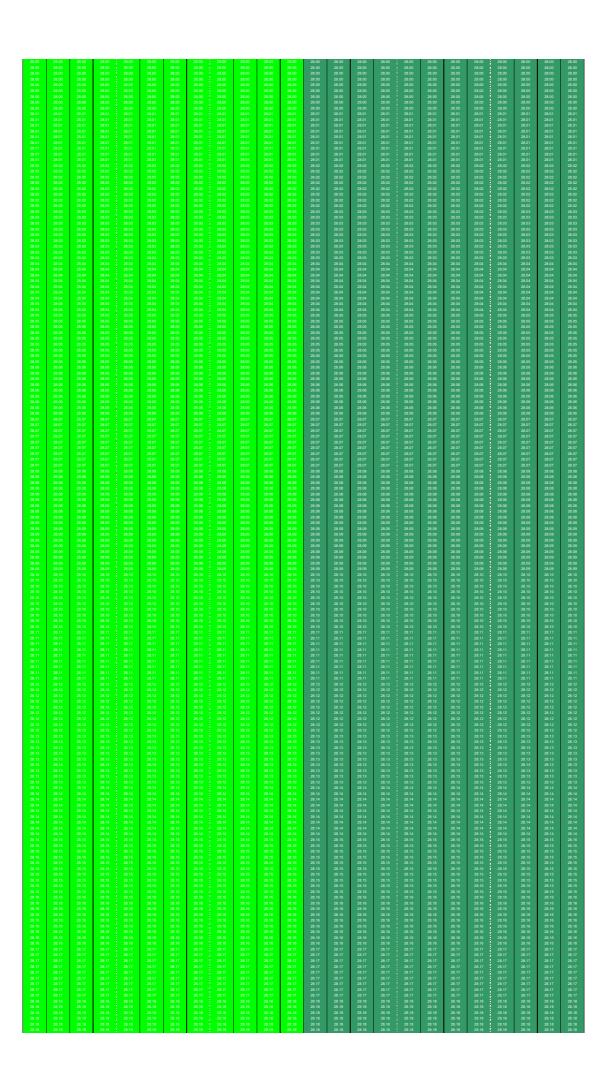


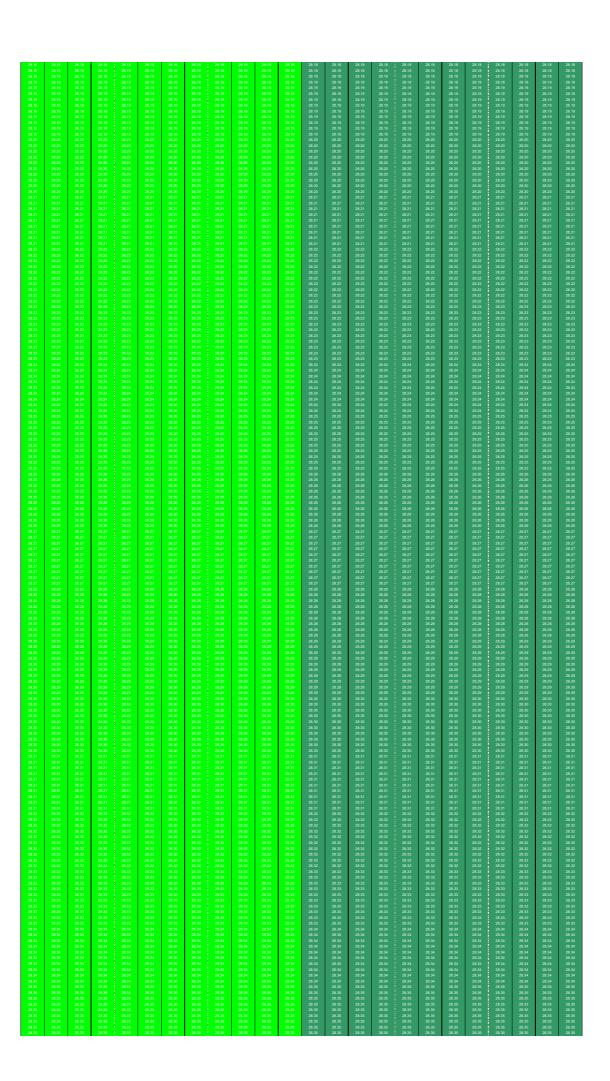
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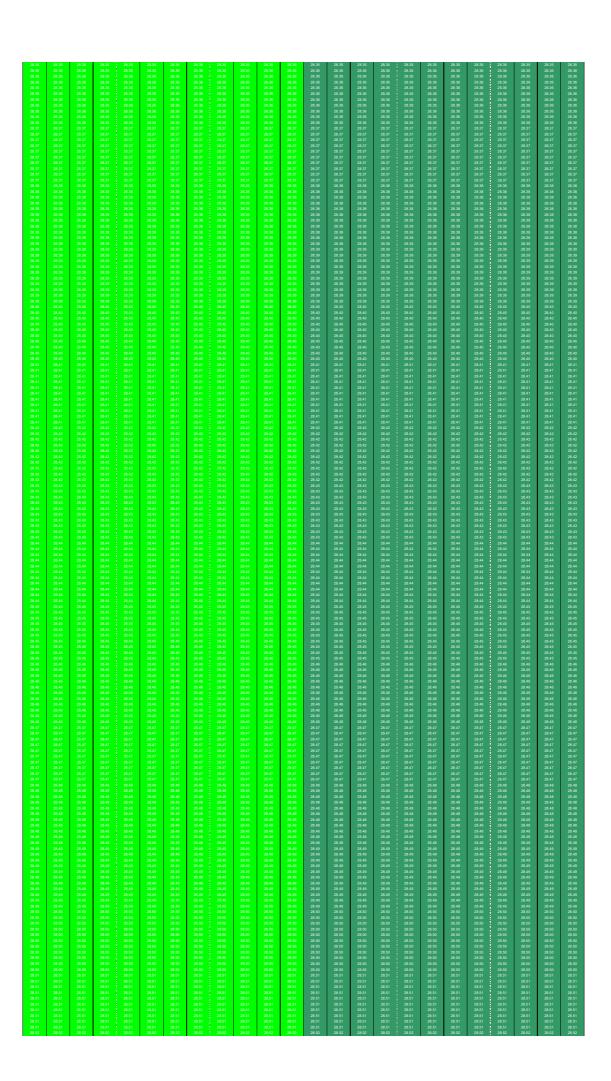


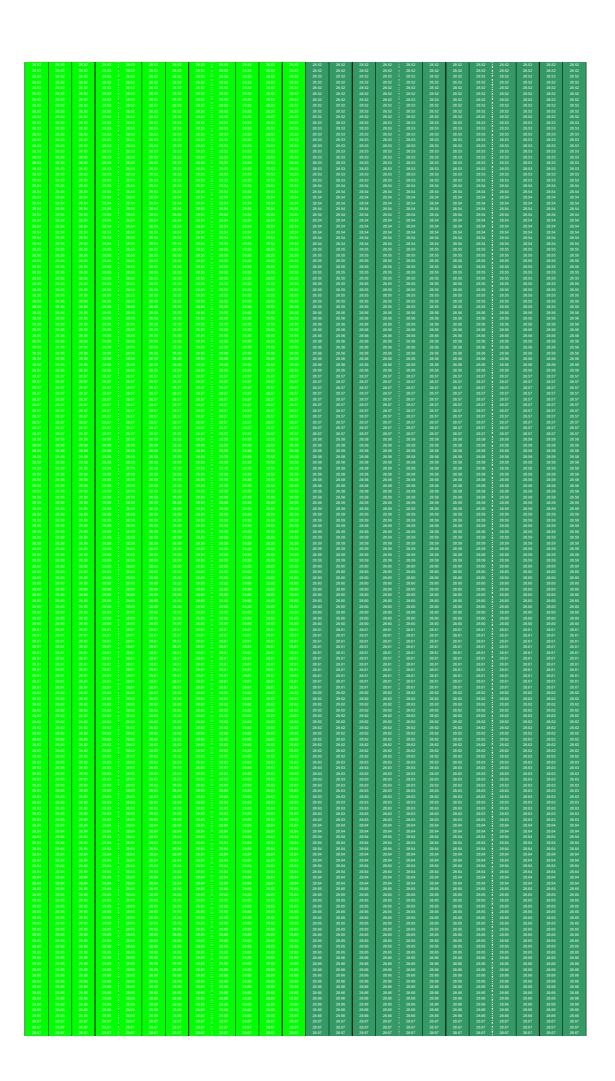
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	27.71 27.71 27.71	27.71 27.71 27.71	27.71 27.71 27.71		27.71 27.71 27.71	27.71 27.71 27.71 27.71	27.71 27.71 27.71 27.71		27.71 27.71 27.71		27.71 27.71 27.71 27.71					27.71 27.71 27.71 27.71	27.71 27.71 27.71			27.71 27.71 27.71	27.71 27.71 27.71	27.71 27.71 27.71 27.71
	27.71 27.71 27.71 27.72	27.71 27.71 27.71 27.72	27.71 27.71 27.71 27.72		27.71 27.71 27.71 27.72	27.71 27.71 27.71 27.72	27.71 27.71 27.71 27.72		27.71 27.71 27.71 27.72		27.71 27.71 27.71 27.72	27.71 27.71 27.71	27.71		27.71 27.71	27.71	27.71 27.71 27.71		27.71 27.71 27.71 27.71 27.71 27.71	27.71 27.71 27.71	27.71 27.71 27.71	27.71
	27.72 27.72 27.72 27.72	27.72 27.72 27.72	27.72 27.72 27.72		27.72 27.72 27.72 27.72	27.72 27.72 27.72	27.72 27.72 27.72		27.72 27.72 27.72		27.72 27.72 27.72				27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72		27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72
	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72		27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72		27.72 27.72 27.72 27.72		27.72 27.72				27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72			27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72	27.72 27.72 27.72 27.72
	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73		27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73		27.72 27.73 27.73 27.73		27.72 27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73		27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.72 27.73 27.73 27.73 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73	27.72 27.73 27.73 27.73
	27.73 27.73	27.73 27.73	27.73 27.73 27.73		27.73 27.73 27.73	27.73 27.73	27.73 27.73		27.73 27.73		27.73 27.73		27.73 27.73	27.73 27.73	27.73 27.73	27.73 27.73	27.73 27.73 27.73		27.73 27.73 27.73 27.73	27.73 27.73	27.73 27.73	27.73 27.73
	27.73 27.73 27.73 27.74	27.73 27.73 27.73 27.74	27.73 27.73 27.74		27.73 27.73 27.74	27.73 27.73 27.73 27.74 27.74	27.73 27.73 27.73 27.74		27.73 27.73 27.73 27.74		27.73 27.73 27.73 27.74				27.73	27.73 27.73 27.73 27.74	27.73 27.73 27.74		27.73 27.73 27.73 27.73 27.74 27.74	27.73 27.73 27.73 27.74	27.73 27.73 27.73 27.74	27.73 27.73 27.73 27.74
	27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74		27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74		27.74 27.74 27.74 27.74		27.74 27.74 27.74 27.74				27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74			27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74	27.74 27.74 27.74 27.74
	27.74 27.74 27.74	27.74 27.74 27.74 27.74 27.75	27.74 27.74 27.74		27.74 27.74	27.74 27.74	27.74 27.74 27.74 27.74 27.75		27.74 27.74		27.74 27.74	27.74 27.74		27.74 27.74		27.74 27.74 27.74 27.74 27.75	27.74 27.74	27.74 27.74	27.74 27.74 27.74 27.74	27.74 27.74	27.74 27.74 27.74 27.74 27.75	27.74 27.74 27.74 27.74 27.75
	27.75 27.75 27.75	27.75 27.75	27.75 27.75 27.75		27.74 27.75 27.75 27.75	27.74 27.75 27.75 27.75	27.75 27.75		27.74 27.75 27.75 27.75		27.74 27.75 27.75 27.75		27.75 27.75		27.75 27.75	27.75 27.75	27.74 27.75 27.75 27.75			27.74 27.75 27.75 27.75	27.75 27.75	27.75 27.75
	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75		27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75		27.75 27.75 27.75		27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75 27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75	27.75 27.75 27.75
	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76		27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76 27.76	27.75 27.75 27.76 27.76		27.75 27.75 27.76 27.76		27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.75 27.75 27.76 27.76 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76	27.75 27.75 27.76 27.76
	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76		27.76 27.76 27.76	27.76 27.76	27.76 27.76 27.76		27.76 27.76 27.76		27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76	27.76 27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76 27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76 27.76
	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76		27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76		27.76 27.76 27.76		27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76	27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76 27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76 27.76	27.76 27.76
	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77		27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77		27.77 27.77 27.77 27.77		27.77 27.77 27.77 27.77		27.76 27.76 27.77 27.77 27.77 27.77		27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77			27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77
	27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77		27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77		27.77 27.77 27.77		27.77 27.77 27.77 27.77		27.77 27.77		27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77 27.77			27.77 27.77 27.77 27.77	27.77 27.77 27.77 27.77	27.77 27.77
	27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78		27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78		27.77 27.78 27.78 27.78		27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.77 27.77 27.78 27.78 27.78 27.78 27.78 27.78	27.77 27.78 27.78 27.78	27.78 27.78	27.77 27.77 27.78 27.78 27.78
	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78		27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78		27.78 27.78 27.78 27.78		27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78 27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78	27.78 27.78 27.78 27.78
	27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79		27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79		27.78 27.78 27.79		27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79 27.79 27.79	27.78 27.78 27.79 27.79 27.79	27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.78 27.78 27.79 27.79	27.78 27.78 27.79	27.78 27.78 27.79	27.78 27.78 27.79 27.79 27.79
	27.79 27.79 27.79	27.79 27.79 27.79	27.79 27.79 27.79		27.79 27.79 27.79	27.79 27.79 27.79 27.79	27.79 27.79 27.79		27.79 27.79 27.79		27.79 27.79 27.79 27.79			27.79 27.79 27.79 27.79	27.79 27.79	27.79 27.79 27.79 27.79	27.79 27.79 27.79 27.79		27.79 27.79 27.79 27.79 27.79 27.79	27.79 27.79 27.79	27.79 27.79 27.79 27.79	27.79 27.79 27.79 27.79
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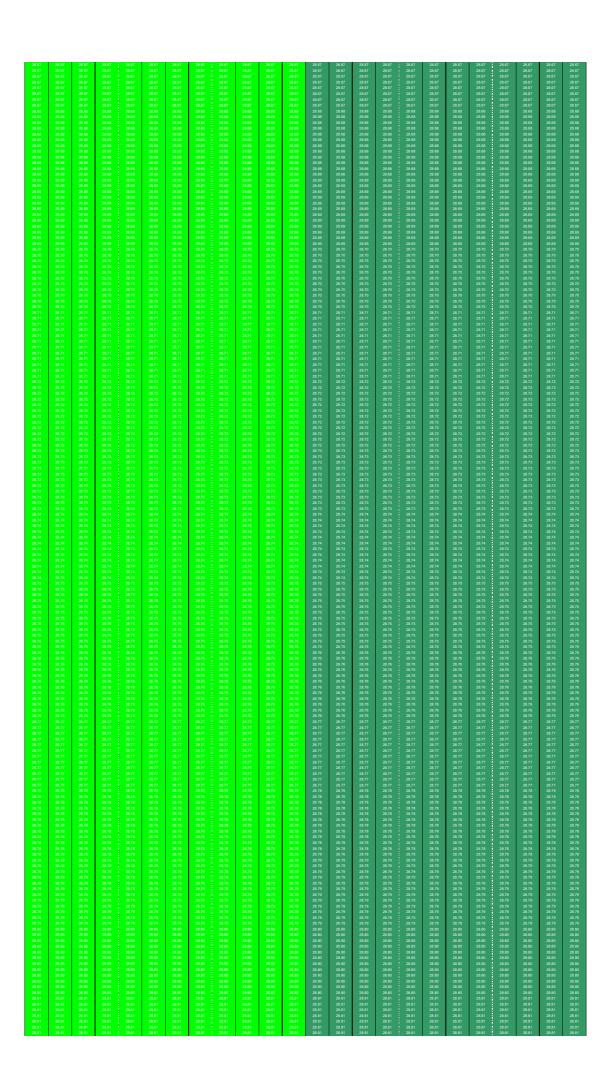
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		27.80 27.81 27.81 27.81	27.80 27.81 27.81 27.81		27.80 27.81 27.81 27.81	27.80 27.81 27.81 27.81	27.80 27.81 27.81 27.81		27.80 27.81 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81 27.81	27.80 2 27.81 2 27.81 2 27.81 2	7.81	27.80 27.81 27.81	27.80 27.81 27.81	27.80 27.81 27.81
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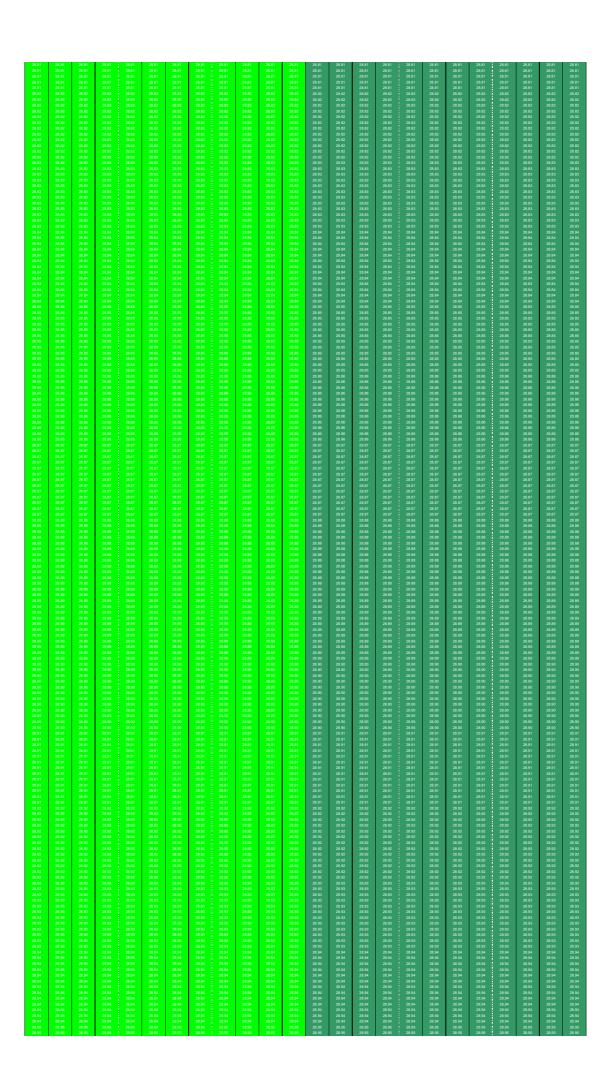


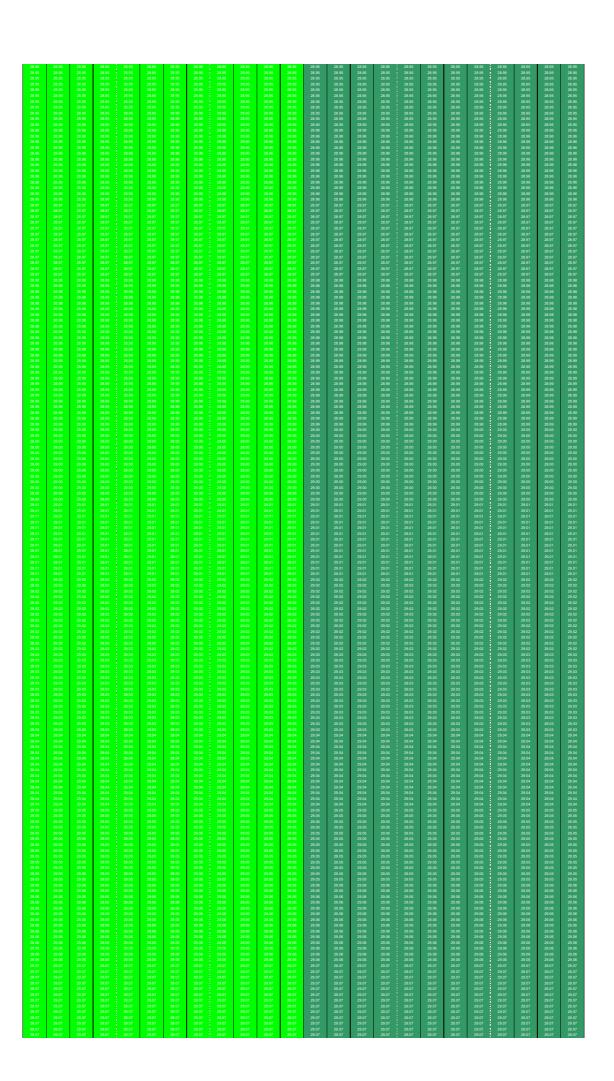


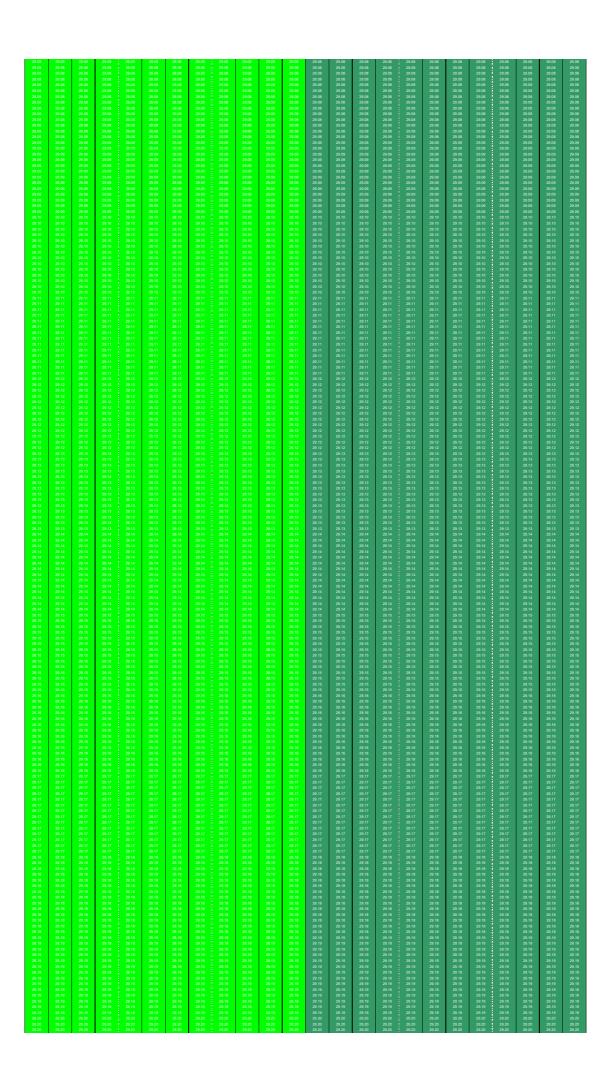




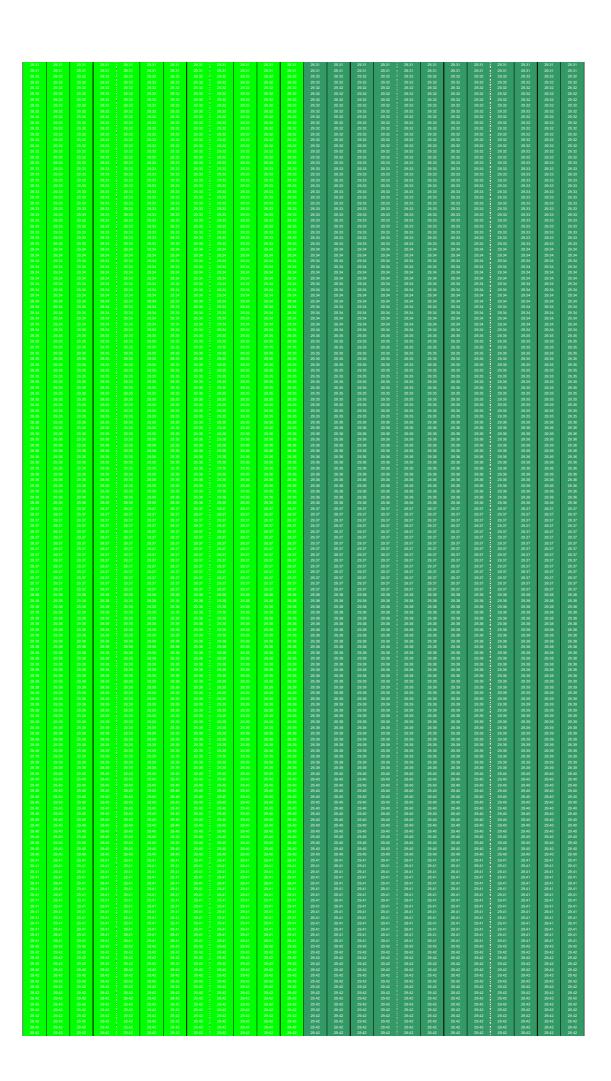




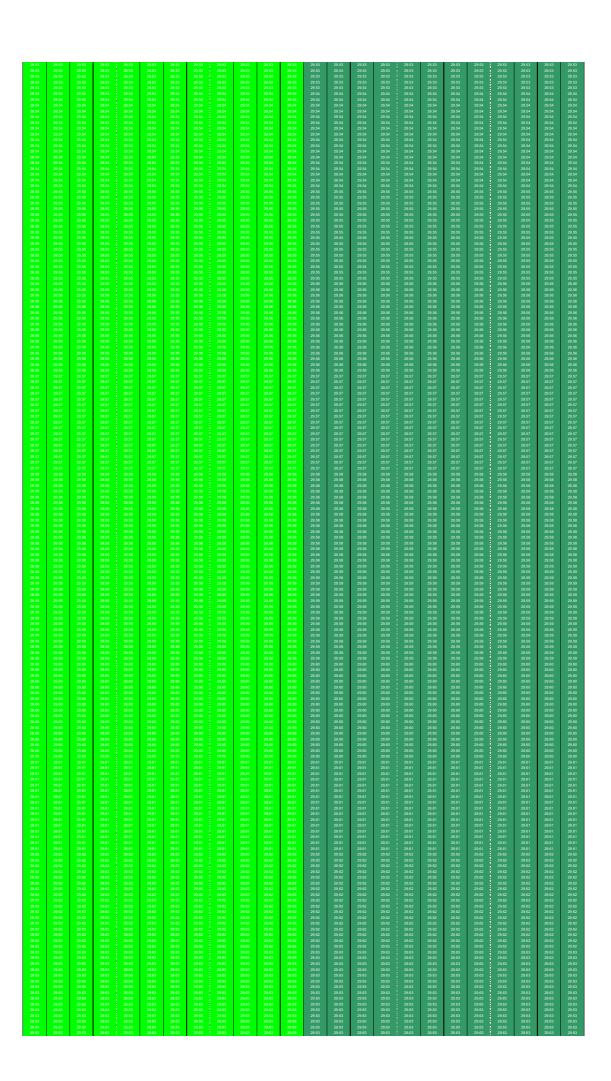


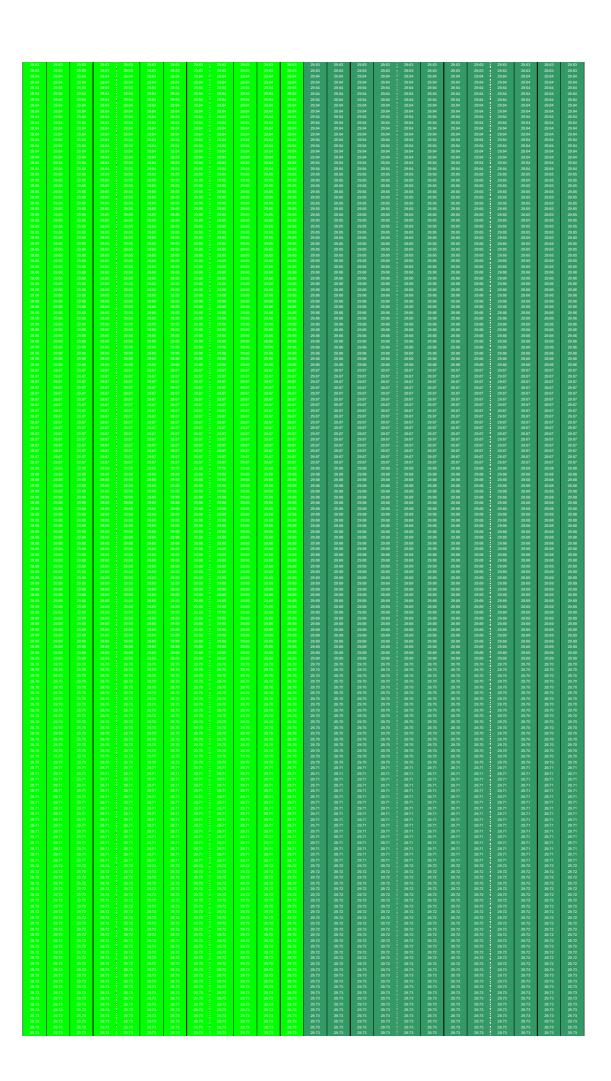


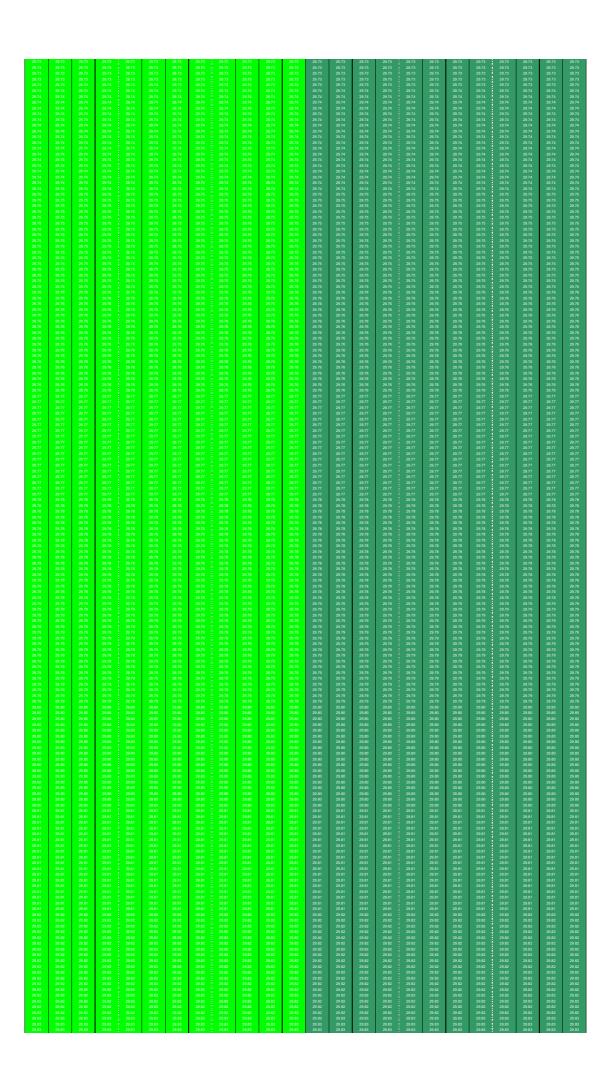
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	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22	29.22 29.22	29.22	29.22 29.22	29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22	29.22 29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22
	29.22 29.22	29.22	29.22 29.22		29.22 29.22	29.22 29.22	29.22	29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22
	29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22	29.22 29.22 29.22
	29.22 29.22 29.22	29.22 29.22	29.22		29.22 29.22	29.22 29.22	29.22 29.22	29.22 29.22		29.22 29.22 29.22	29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22	29.22 29.22 29.22 29.22	29 22 29 22 29 22 29 22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22 29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22	29.22 29.22 29.22 29.22
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	29.23 29.23	29.23 29.23	29.23 29.23		29.22 29.23 29.23 29.23	29.23 29.23 29.23	29.22 29.23 29.23 29.23	29.23 29.23 29.23		29.23 29.23	29.22 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23
	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23		29.23 29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23		29.23 29.23 29.23	29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23	29.23	29.23 29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23 29.23 29.23 29.23	29.23	29.23	29.23
	29.23 29.23	29.23	29.23 29.23		29.23	29.23 29.23	29.23 29.23	29.23 29.23		29.23 29.23	29.23 29.23	29.23 29.23 29.23	29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23		29.23 29.23	29.23 29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23
	29.23 29.23	29.23 29.23 29.23 29.23	29.23 29.23		29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23 29.23 29.23		29.23 29.23	29.23 29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23 29.23 29.23	29.23 29.23	29.23 29.23	29.23 29.23
	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23 29.23 29.23 29.23 29.24	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29:23 29:23 29:23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23 29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23	29.23 29.23 29.23
	29.23 29.23 29.24	29.23 29.23 29.24	29.23 29.23 29.24		29.23 29.23 29.24	29.23 29.23 29.24	29.23 29.24	29.23 29.23 29.24		29.23 29.23 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24	29.23 29.23 29.23 29.23 29.24 29.24 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24	29.23 29.23 29.24 29.24
	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24		29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24		29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24	29.23 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24 29.24	29.24 29.24	29.24 29.24 29.24	29.24 29.24	29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24 29.24 29.24 29.24	29.24 29.24	29.24 29.24	29.24
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	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24	29.24 29.24 29.24 29.24	29.24	29.24	29.24 29.24 29.24	29.24 29.24 29.24 29.24 29.24 29.24	29.24	29.24	29.24 29.24 29.24
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	29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.25
	29.25 29.25	29.25 29.25 29.25	29.25 29.25		29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25	29 25 29 26 29 26	29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25
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	29.25 29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25 29.25		29.25	29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25		29.25 29.25 29.25	29.25 29.25	29.25 29.25	29.25 29.25 29.26	29.25 29.25	29.25 29.25	29.25	29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25 29.25 29.25 29.25	29.25 29.25	29.25 29.25 29.25 29.25 29.25	29.25 29.25 29.25 29.25
	29.25 29.25	29.25	29.25 29.25		29.25 29.25 29.25	29.25 29.25	29.25	29.25 29.25		29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25	29.25 29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25	29.25 29.25 29.25
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	29.26 29.26 29.26	29.25 29.26 29.26 29.26 29.26 29.26	29.26 29.26 29.26		29.26 29.26 29.26 29.26 29.26	29.26 29.26 29.26 29.26 29.26	29.25 29.26 29.26 29.26 29.26 29.26	29.25 29.26 29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.25 29.25 29.26 29.26 29.26 29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26	29.26	29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26 29.26 29.26 29.26	29.26 29.26	29.26	29.26
	29.26 29.26	29.26	29.26 29.26	29.26 29.26	29.26	29.26	29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26	29.26 29.26	29.26 29.26
	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26		29.26 29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26 29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26
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29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26 29.26 29.26		29.26 29.26 29.26 29.26	29.26 29.26 29.26 29.26 29.27	29.26 29.26 29.26 29.26	29.26 29.26 29.26 29.26		29.26 29.26 29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26	29.26 29.26	29.26 29.26 29.26 29.26	29.26 29.26 29.26	29.26 29.26	29.26 29.26
29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27		29.27 29.27	29.27	29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27	29.26 29.27 29.27	29.26 29.27 29.27
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	29.27 29.27 29.27	29.27 29.27	29.27 29.27		29.27 29.27	29.27 29.27	29.27 29.27 29.27	29.27 29.27		29.27 29.27 29.27	29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27
	29.27 29.27	29.27 29.27	29.27 29.27		29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27		29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27	29.27 29.27	29.27 29.27
	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27		29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27		29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27
	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27		29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27		29.27 29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27	29.27 29.27 29.27 29.27
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	29.28 29.28	29.28 29.28	29.28 29.28		29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28		29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28 29.28 29.28	29.28 29.28	29.28 29.28	29.28 29.28
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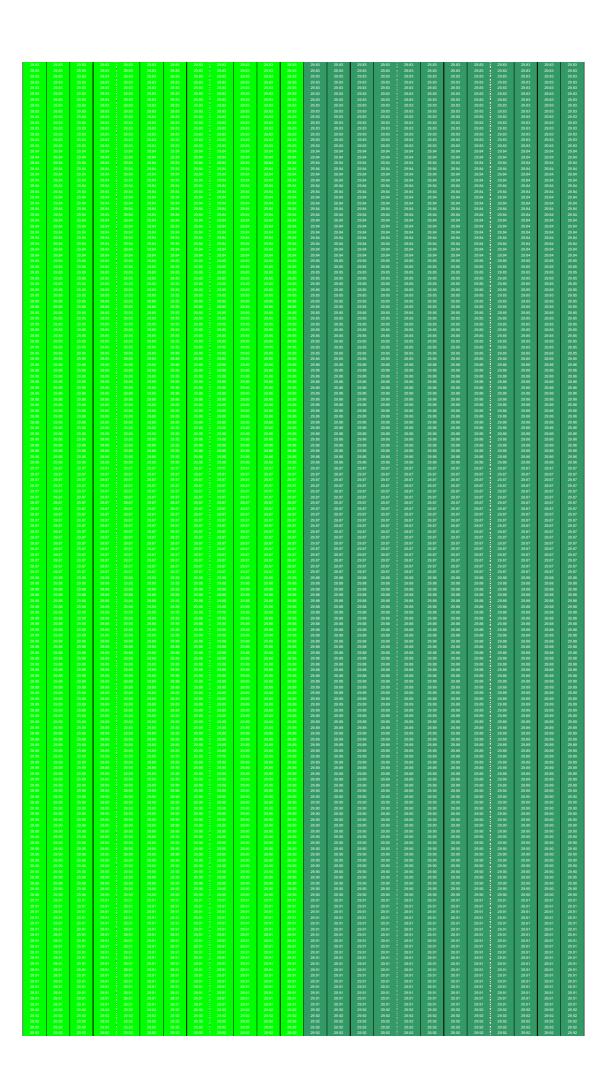


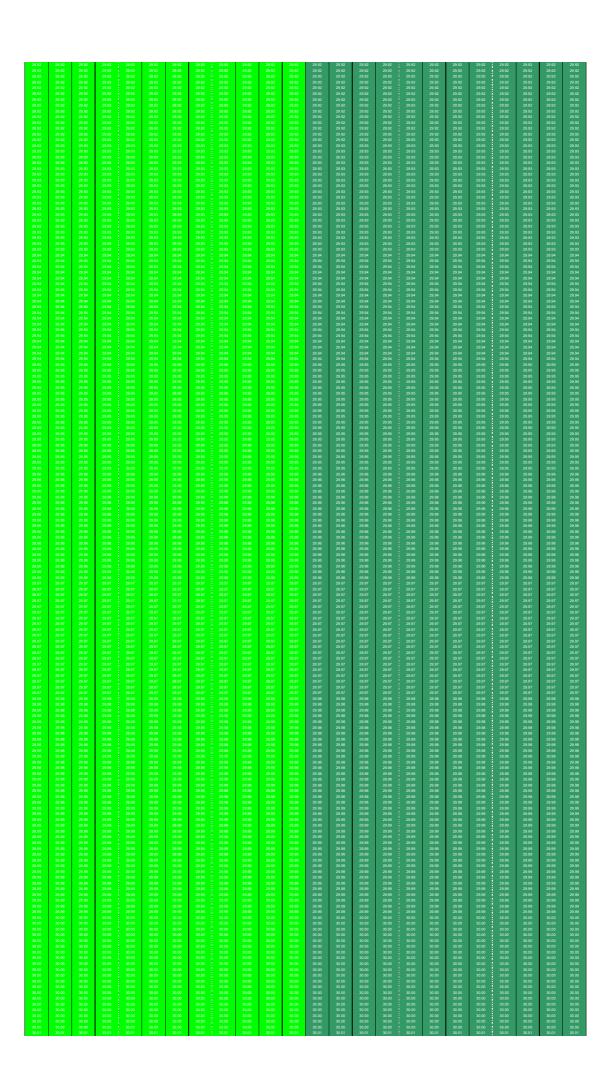
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14		29.47 29.47 29.47		29.47 29.47 29.47	29.47	29.47 29.47 29.47	29.47	29.47 29.47 29.47	29.47 29.47 29.47	29.47 29.47 29.47	29.47	29.47	29.47 29.47 29.47	29.47 29.47 29.47 29.47 29.47 29.47	29.47	29.47	29.47						
		29.48	29.48	29.48		29.48	29.48	29.48		29.48	29.48	29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48		29.48	29.48 29.48	29.48 29.48 29.48 29.48	29.48	29.48	29.48
14		29.48	29.48	29.48 29.48	29.48 29.48	29.48	29.48	29.48		29.48 29.48	29.48	29.48		29.48 29.48 29.48	29.48	29.48		29.48	29.48		29.48	29.48	29.48
Mart	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48	29.48	29.48 29.48	29.48 29.48 29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48										
Mart	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48		29.48	29.48	29.48	29.48 29.48 29.48	29.48	29.48	29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48	29.48 29.48 29.48	29.48 29.48 29.48 29.48 29.48 29.48	29.48	29.48	29.48
14		29.48 29.48	29.48 29.48	29.48 29.48		29.48	29.48 29.48	29.48 29.48		29.48 29.48	29.48 29.48	29.48		29.48 29.48	29.48	29.48		29.48 29.48	29.48	29.48 29.48 29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48
14		29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48	29.48 29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48		29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48	29.48 29.48	29.48 29.48	29.48 29.48 29.48	29.48 29.48 29.48 29.48	29.48	29.48	29.48
14		29.48 29.49	29.48 29.49	29.48 29.49		29.48 29.49	29.48 29.49	29.48 29.49		29.48 29.49	29.48 29.49	29.48 29.49	29.48	29.48 29.49	29.48	29.48	29.48 29.49	29.48 29.49	29.48	29.48 29.48	29.48	29.48 29.49	29.48
14		29.49 29.49	29.49 29.49 29.49	29.49	29.49 29.49 29.49	29.49	29.49 29.49	29.49		29.49	29.49	29.49 29.49	29.49 29.49 29.49	29.49 29.49 29.49 29.49 29.49 29.49	29.49 29.49 29.49	29.49	29.49						
May		29.49 29.49	29.49	29.49		29.49	29.49 29.49	29.49		29.49	29.49	29.49 29.49	29.49 29.49 29.49 29.49	29.49 29.49	29.49 29.49	29.49 29.49							
Dec. 100													29.49		29.49	29.49		29.49	29.49	29.49 29.49	29.49	29.49 29.49	29.49
14		29.49	29.49	29.49		29.49	29.49	29.49		29.49	29.49	29.49			29.49	29.49		29.49	29.49		29.49	29.49	29.49
100 200	29.49 29.49	29.49 29.49 29.49 29.49	29.49 29.49	29.49 29.49	29.49 29.49																		
180 280		29.49	29.49	29.49		29.49	29.49	29.49		29.49	29.49	29.49 29.49	29.49	29.49 29.49	29.49	29.49	29.49	29.49	29.49	29.49 29.49	29.49	29.49	29.49
100		29.50	29.50	29.50		29.50	29.50	29.50		29.50	29.50 29.50	29.50		29.50 29.50	29.50	29.50		29.50	29.50		29.50	29.50	29.50
150		29.50	29.50	29.50		29.50	29.50	29.50		29.50	29.50	29.50			29.50	29.50		29.50	29.50		29.50	29.50	29.50
100 100		29.50 29.50	29.50	29.50 29.50		29.50	29.50 29.50	29.50 29.50		29.50 29.50	29.50 29.50	29.50	29.50 29.50		29.50 29.50	29.50		29.50 29.50	29.50 29.50	29.50 29.50 29.50 29.50	29.50 29.50	29.50	29.50 29.50
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No. 196 296		29.50 29.50	29.50 29.50	29.50 29.50		29.50 29.50	29.50 29.50	29.50 29.50		29.50 29.50	29.50 29.50 29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50									
251 251		29.50 29.50	29.50 29.50	29.50 29.50		29.50 29.50	29.50 29.50	29.50 29.50		29.50 29.50	29.50 29.50	29.50	29.50 29.50	29.50 29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50 29.50 29.50	29.50 29.50	29.50 29.50	29.50 29.50
241 241		29.51	29.51	29.51		29.51	29.51	29.51		29.51	29.51	29.51 29.51		29.51	29.51	29.51		29.51	29.51		29.51	29.51	29.51
251 251		29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51 29.51 29.51 29.51	29.51 29.51	29.51 29.51	29.51 29.51									
Part		29.51 29.51		29.51 29.51	29.51 29.51 29.51 29.51	29.51 29.51	29.51 29.51	29.51 29.51															
18		29.51 29.51	29.51	29.51 29.51		29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51 29.51	29.51	29.51 29.51	29.51 29.51	29.51 29.51	29.51		29.51 29.51	29.51 29.51	29.51 29.51 29.51 29.51	29.51 29.51	29.51 29.51	29.51 29.51
15		29.51 29.51		29.51 29.51	29.51 29.51 29.51 29.51		29.51 29.51	29.51 29.51															
15		29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51 29.51	29.51 29.51	29.51 29.51		29.51 29.51	29.51		29.51 29.51	29.51 29.51	29.51 29.51 29.51 29.51	29.51 29.51	29.51 29.51	29.51 29.51
Mail		29.51 29.52	29.51	29.51 29.52		29.51 29.52	29.51 29.52	29.51 29.52		29.51 29.52	29.51 29.52	29.51	29.51 29.52	29.51	29.51 29.52	29.51		29.51 29.52	29.51 29.52	29.51 29.51 29.52 29.52	29.51 29.52	29.51 29.52	29.51 29.52
Mail		29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52 29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52						
The color The		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52 29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52									
18		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52						
32		29.52	29.52	29.52		29.52	29.52	29.52		29.52	29.52	29.52 29.52		29.52 29.52	29.52	29.52	29.52	29.52	29.52	29.52 29.52 29.52 29.52	29.52	29.52	29.52
32		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52 29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52									
950 953 755 755 755 755 755 755 755 755 755 7		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52	29.52 29.52		29.52 29.52	29.52 29.52 29.52 29.52	29.52 29.52	29.52 29.52	29.52 29.52									
250 751 755 755 755 755 755 755 755 755 755		29.53 29.53	29.53 29.53	29.53 29.53		29.53 29.53	29.53 29.53	29.53 29.53		29.53 29.53	29.53 29.53 29.53 29.53	29.53 29.53	29.53 29.53	29.53 29.53									
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		29.53 29.53	29.53	29.53 29.53 29.53		29.53 29.53 29.53	29.53 29.53 29.53	29.53 29.53 29.53		29.53 29.53 29.53	29.53 29.53	29.53 29.53 29.53			29.53	29.53 29.53 29.53	29.53 29.53 29.53	29.53	29.53	29.53 29.53 29.53 29.53 29.53 29.53	29.53 29.53	29.53	29.53











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30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.06	30.05 30.06	30.06	30.06	30.06

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					Forestr	y Area 5					
Wind speed upwind of	Wind speed	xp Wind speed	Wind speed over	Wind speed	Wind speed at back of	Ϊ	Wind speed over	Wind speed upwind of	Wind speed	l	Wind speed over
forestry (m s ⁻¹)	forest (m s ⁻¹)	in felled gap (m s ⁻¹)	replanted forestry (m s ⁻¹)	forestry (m s ⁻¹)	forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	replanted forestry (m s ⁻¹)	forestry (m s ⁻¹)	Wind speed at back of forest (m s ⁻¹)	Wind speed in felled gap (m s ⁻¹)	replanted forestry (m s ⁻¹)
8.77 10.50	#NUM! #NUM! #NUM!	#NUM! #NUM! #NUM!	-2.10 2.71 5.53	8.77 10.50 11.51	#NUM! #NUM!	#NUM! #NUM! #NUM!	-2.10 2.71 5.53	8.77 10.50 11.51	#NUM! #NUM!	#NUM! #NUM! #NUM!	-2.10 2.71 5.53
11.51 12.23 12.79 13.25	#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	5.53 7.52 9.07 10.33	12.23 12.79 13.25	#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	7.52 9.07 10.33	12.23 12.79 13.25	#NUM! #NUM! #NUM! #NUM!	#NUM! #NUM! #NUM! #NUM!	7.52 9.07 10.33
13.63	#NUM!	#NUM!	11.40	13.63	#NUM!	#NUM!	11.40	13.63	#NUM!	#NUM!	11.40
13.96	#NUM!	#NUM!	12.33	13.96	#NUM!	#NUM!	12.33	13.96	#NUM!	#NUM!	12.33
14.26	#NUM!	#NUM!	13.15	14.26	#NUM!	#NUM!	13.15	14.26	#NUM!	#NUM!	13.15
14.52	#NUM!	#NUM!	13.88	14.52	#NUM!	#NUM!	13.88	14.52	#NUM!	#NUM!	13.88
14.76	#NUM!	#NUM!	14.54	14.76	#NUM!	#NUM!	14.54	14.76	#NUM!	#NUM!	14.54
14.98	14.98	14.98	14.98	14.98	14.98	14.98	14.98	14.98	14.98	14.98	14.98
15.18	15.18	15.18	15.18	15.18	15.18	15.18	15.18	15.18	15.18	15.18	15.18
15.36	15.36	15.36	15.36	15.36	15.36	15.36	15.36	15.36	15.36	15.36	15.36
15.54	15.54	15.54	15.54	15.54	15.54	15.54	15.54	15.54	15.54	15.54	15.54
15.70	15.70	15.70	15.70	15.70	15.70	15.70	15.70	15.70	15.70	15.70	15.70
15.85	15.85	15.85	15.85	15.85	15.85	15.85	15.85	15.85	15.85	15.85	15.85
15.99	15.99	15.99	15.99	15.99	15.99	15.99	15.99	15.99	15.99	15.99	15.99
16.13	16.13	16.13	16.13	16.13	16.13	16.13	16.13	16.13	16.13	16.13	16.13
16.26 16.38	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38 16.49	16.26 16.38	16.26 16.38 16.49
16.49 16.61 16.71 16.81	16.49 16.61 16.71 16.81	16.49 16.61 16.71	16.49 16.61 16.71 16.81	16.49 16.61 16.71 16.81	16.49 16.61 16.71	16.49 16.61 16.71 16.81	16.49 16.61 16.71 16.81	16.49 16.61 16.71 16.81	16.49 16.61 16.71 16.81	16.49 16.61 16.71	16.49 16.61 16.71
16.91 17.01	16.91 17.01	16.81 16.91 17.01	16.91 17.01	16.91 17.01	16.81 16.91 17.01	16.91 17.01	16.91 17.01	16.91 17.01	16.91 17.01	16.81 16.91 17.01	16.81 16.91 17.01
17.10 17.18 17.27 17.35	17.10 17.18 17.27 17.35		17.10 17.18 17.27 17.35		17.10 17.18 17.27 17.35	17.10 17.18 17.27 17.35	17.10 17.18 17.27 17.35				
17.35	17.35	17.35	17.35	17.35	17.35	17.35	17.35	17.35	17.35	17.35	17.35
17.43	17.43	17.43	17.43	17.43	17.43	17.43	17.43	17.43	17.43	17.43	17.43
17.51	17.51	17.51	17.51	17.51	17.51	17.51	17.51	17.51	17.51	17.51	17.51
17.58	17.58	17.58	17.58	17.58	17.58	17.58	17.58	17.58	17.58	17.58	17.58
17.65	17.65	17.65	17.65	17.65	17.65	17.65	17.65	17.65	17.65	17.65	17.65
17.73	17.73	17.73	17.73	17.73	17.73	17.73	17.73	17.73	17.73	17.73	17.73
17.79	17.79	17.79	17.79	17.79	17.79	17.79	17.79	17.79	17.79	17.79	17.79
17.86	17.86	17.86	17.86	17.86	17.86	17.86	17.86	17.86	17.86	17.86	17.86
17.93	17.93	17.93	17.93	17.93	17.93	17.93	17.93	17.93	17.93	17.93	17.93
17.99	17.99	17.99	17.99	17.99	17.99	17.99	17.99	17.99	17.99	17.99	17.99
18.05	18.05	18.05	18.05	18.05	18.05	18.05	18.05	18.05	18.05	18.05	18.05
18.11 18.17 18.23	18.11 18.17 18.23	18.11 18.17 18.23	18.11 18.17 18.23	18.11 18.17 18.23	18.11 18.17 18.23	18.11 18.17	18.11 18.17 18.23			18.11 18.17 18.23	18.11 18.17 18.23
18.28 18.34	18.28 18.34	18.28 18.34	18.28 18.34	18.28 18.34	18.28 18.34	18.23 18.28 18.34	18.28 18.34	18.23 18.28 18.34	18.23 18.28 18.34	18.28 18.34	18.28 18.34
18.39	18.39	18.39	18.39	18.39	18.39	18.39	18.39	18.39	18.39	18.39	18.39
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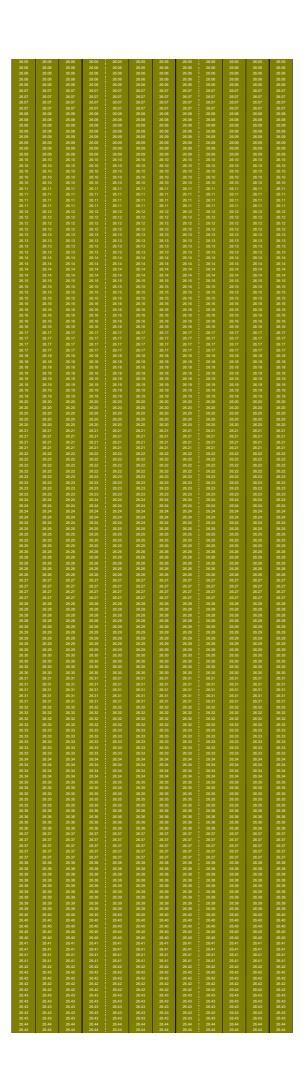
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		21.75 21.76						21.75 21.76	21.75 21.76		21.75 21.76	21.75 21.76
	21.82 21.83	21.82 21.83			21.82 21.83		21.82 21.83	21.82 21.83	21.82 21.83	21.82 21.83	21.82 21.83	
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2007 2007	23.04 23.05											
2.00 2.00		23.07						23.07				23.07
2311 2311												23.09
2.16 2.26	23.11 23.12	23.11 23.12	23.11 23.12	23.11 23.12	23.11 23.12	23.11	23.11 23.12	23.11 23.12	23.11 23.12	23.11 23.12	23.11 23.12	23.11 23.12
2.16 2.26	23.13					23.12 23.13 23.14	23.13	23.12 23.13 23.14	23.12 23.13 23.14			23.13
2417 2418 2418								23.15 23.16 23.16				23.16
210 2219 2	23.17 23.18											
2221 2221 2221 2221 2221 2221 2221 222	23.19 23.19 23.20	23.19 23.19 23.20	23.19 23.19	23.19 23.19	23.19 23.19		23.19 23.19 23.20	23.19 23.19 23.20	23.19 23.19 23.20	23.19 23.19	23.19 23.19 23.20	23.19 23.19
224 225	23.21 23.22	23.21	23.21 23.22	23.21 23.22	23.21 23.22	23.21	23.21 23.22	23.21	23.21 23.22	23.21 23.22	23.21	23.21 23.22
23.25 23.25	23.23 23.24	23.23 23.23 23.24	23.23 23.24			23.23 23.23 23.24	23.23 23.24			23.23 23.24	23.23 23.23 23.24	23.23 23.24
	23.25 23.26	23.25 23.26 23.26	23.25 23.26	23.25 23.26 23.26			23.25 23.26	23.25 23.26 23.26		23.25 23.26	23.25 23.26 23.26	23.25 23.26

23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29	23.27 23.28 23.29
23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31	23.29 23.30 23.31
23.32 23.32 23.33 23.34	23.32 23.32 23.33	23.32 23.32 23.33	23.32 23.32 23.33	23.32 23.32 23.33 23.34	23.32 23.32 23.33 23.34	23.32 23.32 23.33 23.34	23.32 23.32 23.33	23.32 23.32 23.33 23.34	23.32 23.32 23.33	23.32 23.32 23.33	23.32 23.32 23.33
23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35	23.34 23.35 23.35
23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38	23.36 23.37 23.38
23.38 23.39 23.40	23.38 23.39 23.40	23.38 23.39	23.38 23.39	23.38 23.39 23.40	23.38 23.39	23.38 23.39	23.38 23.39	23.38 23.39 23.40	23.38 23.39	23.38 23.39	23.38 23.39
23.40 23.41	23.40 23.41	23.40 23.40 23.41	23.40 23.40 23.41	23.40 23.41	23.40 23.40 23.41	23.40 23.40 23.41	23.40 23.40 23.41	23.40 23.41	23.40 23.40 23.41	23.40 23.40 23.41	23.40 23.40 23.41
23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43	23.42 23.43 23.43
	23.44 23.45 23.45	23.44 23.45 23.45	23.44 23.45 23.45		23.44 23.45 23.45	23.44 23.45 23.45	23.44	23.44 23.45 23.45 23.46 23.47	23.44 23.45 23.45	23.44 23.45 23.45	23.44 23.45 23.45
23.45 23.45 23.46 23.47	23.46 23.47	23.46 23.47	23.46 23.47	23.45 23.45 23.46 23.47	23.46 23.47	23.46 23.47	23.45 23.45 23.46 23.47 23.47	23.46 23.47	23.46 23.47	23.46 23.47	23.46 23.47
23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49	23.47 23.48 23.49
23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51	23.50 23.50 23.51
23.52 23.52 23.53	23.52 23.52 23.53	23.52 23.52 23.53	23.52 23.52 23.53	23.51 23.52 23.52 23.53	23.52 23.52 23.53	23.51 23.52 23.52 23.53	23.52 23.52 23.53	23.51 23.52 23.52 23.53	23.52 23.52 23.53	23.52 23.52 23.53	23.52 23.52 23.53
23.54 23.54	23.54 23.54 23.55	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54	23.54 23.54
23.55 23.56 23.56	23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56	23.55 23.56 23.56
23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58	23.57 23.58 23.58
23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60	23.59 23.60 23.60
23.61 23.62	23.61 23.62 23.62	23.61 23.62	23.61 23.62 23.62	23.61 23.62	23.61 23.62	23.61 23.62	23.61 23.62	23.61 23.62	23.61 23.62 23.62	23.61 23.62	23.61 23.62 23.62
23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.63 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.62 23.63 23.64 23.64	23.63 23.64
23.64 23.65 23.66	23.64 23.65 23.66	23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66	23.64 23.65 23.66
23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67	23.66 23.67 23.68	23.66 23.67	23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67 23.68	23.66 23.67 23.68
23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69	23.68 23.69 23.69
23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71	23.70 23.71
23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73	23.71 23.72 23.73
23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75	23.73 23.74 23.75
23.75 23.76 23.76	23.75 23.76	23.75 23.76	23.75 23.76 23.76	23.75 23.76	23.75 23.76	23.75 23.76 23.76	23.75 23.76	23.75 23.76	23.75 23.76	23.75 23.76	23.75 23.76
23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78	23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78	23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78	23.76 23.77 23.78
23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80	23.78 23.79 23.79 23.80
23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81	23.80 23.81 23.81
23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83	23.82 23.83
23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85	23.83 23.84 23.84 23.85
23.86 23.86	23.86 23.86	23.85 23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.86 23.86	23.85 23.86 23.86
23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88	23.87 23.87 23.88
23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89 23.90 23.90	23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89	23.88 23.89
23.90 23.90 23.91	23.90 23.90 23.91 23.91	23.90 23.90 23.91	23.90 23.90 23.91		23.90 23.90 23.91	23.90 23.90 23.91 23.91	23.90 23.90 23.91	23.90 23.90 23.91	23.90 23.90 23.91 23.91	23.90 23.90 23.91 23.91	23.90 23.90 23.91
23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93	23.91 23.92 23.93
23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.93 23.94 23.94 23.95	23.94 23.94 23.95
23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96	23.95 23.95 23.96
23.97 23.97	23.97 23.97 23.98	23.97 23.97 23.98	23.97 23.97 23.98	23.97 23.97	23.97 23.97	23.97 23.97	23.97 23.97	23.97 23.97	23.97 23.97 23.98	23.97 23.97	23.97 23.97 23.98
23.98 23.98 23.99 23.99	23.98 23.99 23.99	23.98 23.99 23.99	23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.99 23.99	23.98 23.98 23.99 23.99	23.98 23.99 23.99
24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01	24.00 24.01
24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02	24.01 24.02 24.02
24.03 24.03 24.04 24.05	24.03 24.03	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05	24.03 24.03 24.04 24.05
24.05	24.04 24.05 24.05	24.05	24.05			24.05	24.05				24.05
24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07	24.06 24.06 24.07
24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09	24.07 24.08 24.08 24.09
24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10	24.09 24.09 24.10
24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11 24.11	24.11
24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13	24.12 24.12 24.13 24.13 24.14
24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.13 24.14 24.14	24.14
24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16	24.15 24.15 24.16
24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17	24.16 24.17
24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19	24.17 24.18 24.19 24.19
24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.19 24.20 24.20	24.20 24.20
24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21 24.22 24.22	24.21 24.21	24.21 24.21	24.21 24.21	24.21 24.21
24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23	24.22 24.22 24.23 24.23
24.24 24.24	24.24 24.24	24.24 24.24 24.25	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24	24.24 24.24
24.25 24.25 24.26	24.25 24.25 24.26	24.25 24.26	24.25 24.25 24.26 24.26 24.27	24.25 24.25 24.26 24.26 24.27	24.25 24.25 24.26	24.25 24.25 24.26	24.25 24.25 24.26 24.26 24.27	24.25 24.25 24.26	24.25 24.25 24.26	24.25 24.25 24.26	24.25 24.25 24.26
24.26 24.27 24.27	24.26 24.27 24.27	24.26 24.27 24.27	24.27		24.26 24.27 24.27	24.26 24.27 24.27	24.27	24.26 24.27 24.27	24.26 24.27 24.27	24.26 24.27 24.27	24.26 24.27 24.27
24.28 24.28 24.29	24.28 24.28	24.28 24.28	24.28 24.28 24.29	24.28 24.28 24.29	24.28 24.28 24.29	24.28 24.28 24.29	24.28 24.28	24.28 24.28	24.28 24.28 24.29	24.28 24.28 24.29	24.28 24.28 24.29
24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.29 24.30	24.29 24.30	24.29 24.29 24.30

24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31	24.30 24.31 24.31
	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32	24.31 24.32 24.32
24.32 24.33 24.33	24.32 24.33 24.33	24.33 24.33	24.32 24.33 24.33	24.33 24.33 24.33	24.33 24.33	24.33 24.33	24.32 24.33 24.33	24.33 24.33	24.33 24.33	24.33 24.33	24.32 24.33 24.33
24.34 24.34 24.35	24.34 24.34	24.34 24.34	24.34 24.34	24.34 24.34 24.35	24.34 24.34 24.35	24.34 24.34	24 24		24.34 24.34	24.34 24.34	24.34 24.34
24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.34 24.35 24.35 24.36	24.34 24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36	24.35 24.35 24.36
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24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87	24.86 24.86 24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87	24.87 24.87
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	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92	24.92 24.92
24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93	24.92 24.93 24.93
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24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95	24.94 24.95
24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96	24.95 24.95 24.96
24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.97 24.97	24.96 24.96 24.97 24.97	24.96 24.96 24.97 24.97
24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98	24.97 24.97 24.98
24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.98 24.99 24.99	24.98 24.99	24.98 24.99	24.98 24.99	24.98 24.99
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25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02	25.02 25.02 25.02
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25.06 25.06 25.06	25.06 25.06	25.06 25.06	25.06 25.06	25.06 25.06 25.06	25.06 25.06 25.06	25.06 25.06	25.06 25.06	25.06 25.06 25.06	25.06 25.06	25.06 25.06	25.06 25.06
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25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08	25.07 25.07 25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08	25.08 25.08
25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09	25.08 25.09
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25.19 25.19	25.19 25.19	25.19 25.19	25.19 25.19	25.19 25.19 25.19	25.19 25.19	25.19 25.19	25.18 25.18 25.19 25.19 25.19 25.20	25.19 25.19	25.19 25.19	25.19 25.19	25.19 25.19
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25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.53 25.53 25.54 25.54 25.54 25.55 25.55 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55 25.55 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55	25.54 25.54 25.54 25.55
25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55	25.55 25.55 25.55
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25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70	25.70 25.70 25.70
25.70 25.71	25.70 25.71	25.70 25.71	25.70 25.71		25.70 25.71	25.70 25.71	25.70 25.71 25.71	25.70 25.71	25.70 25.71	25.70 25.71	25.70 25.71
25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72	25.71 25.71 25.72
25.72 25.72	25.72 25.72	25.72 25.72	25.72 25.72	25.72 25.72 25.72	25.72 25.72	25.72 25.72	25.71 25.72 25.72 25.72 25.72 25.72 25.73	25.72 25.72	25.72 25.72	25.72 25.72	25.72 25.72
25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73	25.72 25.73 25.73
25.73 25.74	25.73 25.74	25.73 25.74	25.73 25.74	25.73 25.74	25.73 25.74	25.73 25.74	25.73	25.73 25.74	25.73 25.74	25.73 25.74	25.73 25.74
25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74 25.74 25.75 25.75	25.74 25.74	25.74 25.74	25.74 25.74	25.74 25.74
25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75	25.74 25.75 25.75
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25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86	25.85 25.86 25.86 25.86	25.86 25.86 25.86	25.85 25.85 25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86 25.86	25.86 25.86 25.86
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25.91 25.92	25.91 25.92	25.91 25.92	25.91 25.92	25.91 25.92	25.91 25.92 25.92	25.91 25.92 25.92	25.91 25.92	25.91 25.92	25.91 25.92 25.92	25.91 25.92 25.92	25.91 25.92
25.92 25.92 25.92 25.93 25.93	25.92 25.92 25.92	25.92 25.92 25.92	25.92 25.92 25.92	25.92 25.92 25.92	25.92 25.92	25.92 25.92	25.92 25.92 25.92	25.92 25.92 25.92 25.93 25.93	25.92 25.92	25.92 25.92	25.92 25.92 25.92
25.93 25.93	25.93 25.93	25.93 25.93	25.93 25.93	25.92 25.92 25.93 25.93 25.93 25.93	25.93 25.93	25.93 25.93	25.92 25.92 25.93 25.93 25.93 25.93	25.93 25.93	25.93 25.93	25.93 25.93	25.93 25.93
25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94	25.93 25.93 25.94
25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94	25.94 25.94 25.94
25.94 25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.94 25.95 25.95 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.94 25.95 25.95 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95	25.94 25.95 25.95
25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95	25.95 25.95
	25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96 25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96	25.96 25.96
25.96 25.96 25.96 25.97 25.97 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97 25.97 25.97 25.98 25.98	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97	25.96 25.96 25.97
25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97 25.97 25.98 25.98	25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97	25.97 25.97
25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98	25.98 25.98
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25.99 25.99 25.99 25.99	25.99 25.99 25.99	25.99 25.99 25.99	25.99 25.99 25.99 25.99	25.99 25.99 25.99 25.99 26.00	25.99 25.99 25.99 25.99	25.99 25.99 25.99 25.99	25.99 25.99 25.99 25.99	25.99 25.99 25.99 25.99	25.99 25.99 25.99 25.99	25.99 25.99 25.99	25.99 25.99 25.99 25.99
25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00	25.99 26.00 26.00
26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00	26.00 26.00
26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01	26.01 26.01
26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02	26.01 26.01 26.02
26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02	26.02 26.02
26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03	26.02 26.03
26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03	26.03 26.03 26.03
26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04	26.03 26.04 26.04
26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05	26.04 26.04 26.05
26.05 26.05 26.05	26.05 26.05	26.05 26.05	26.05 26.05	26.05 26.05 26.05	26.05 26.05	26.05 26.05	26.05 26.05 26.05	26.05 26.05	26.05 26.05	26.05 26.05	26.05 26.05 26.05



26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44
26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44	26.44
26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45	26.44 26.45 26.45 26.45
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26.45	26.45	26.45	26.45	26.45	26.45	26.45	26.45	26.45	26.45	26.45	26.45
26.46	26.46	26.46	26.46	26.46	26.46	26.46	26.46	26.46	26.46	26.46	26.46
26.46 26.46 26.46 26.46	26.46 26.46	26.46 26.46	26.46 26.46	26.46 26.46 26.46 26.46	26.46 26.46	26.46 26.46 26.46 26.46	26.46 26.46 26.46 26.46	26.46 26.46 26.46 26.46	26.46 26.46 26.46 26.46	26.46 26.46	26.46 26.46 26.46 26.46
26.46 26.47	26.46 26.46 26.47	26.46 26.46 26.47	26.46 26.46 26.47	26.46 26.47	26.46 26.46 26.47	26.46 26.47	26.46 26.47	26.46 26.47	26.46 26.47	26.46 26.46 26.47	26.46 26.47
26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47	26.47 26.47 26.47
26.47 26.47 26.48	26.47 26.47	26.47 26.47	26.47 26.47	26.47	26.47	26.47	26.47	26.47	26.47	26.47 26.47 26.48	26.47
26.48 26.48 26.48	26.48 26.48 26.48	26.48 26.48 26.48	26.48 26.48 26.48	26.47 26.48 26.48 26.48 26.48	26.47 26.48 26.48 26.48	26.47 26.48 26.48 26.48	26.47 26.48 26.48 26.48	26.47 26.48 26.48 26.48	26.47 26.48 26.48 26.48	26.48 26.48 26.48	26.47 26.48 26.48 26.48 26.48
26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49	26.48 26.49	26.48 26.48 26.49	26.48 26.48 26.49
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26.49	26.49	26.49	26.49	26.49	26.49	26.49	26.49	26.49	26.49	26.49	26.49
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26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50
26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50	26.50
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March	26.92		26.92	26.92		26.92	26.92	26.92		26.92		26.92
March Marc	26.93 26.93											
20.54	26.93 26.93											
24.00	26.94		26.94	26.94		26.94	26.94	26.94		26.94		26.94
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24.00	26.94 26.94											
24.00	26.95 26.95	26.95 26.95	26.95 26.95	26.95 26.95	26.95 26.95	26.95 26.95	26.95	26.95 26.95	26.95 26.95	26.95	26.95 26.95	26.95 26.95
20.50	26.95 26.95	26.95 26.95	26.95 26.95	26.95 26.95	26.95	26.95 26.95	26.95 26.95	26.95	26.95 26.95	26.95 26.95	26.95 26.95	26.95 26.95
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25.50 25.5	26.96 26.96	26.96	26.96 26.96	26.96	26.96 26.96	26.96 26.96						
March Marc	26.96 26.97	26.96 26.97	26.97	26.97	26.96 26.97	26.96 26.97	26.96 26.97	26.96	26.96 26.97	26.96 26.97	26.96 26.97	26.96 26.97
2.69	26.97		26.97	26.97	26.97 26.97	26.97	26.97 26.97	26.97 26.97	26.97 26.97	26.97		26.97
March Marc	26.97 26.97 26.98	26.97 26.97 26.99	26.97 26.97 26.98	26.97 26.97 26.98	26.97 26.97 26.98	26.97 26.97 26.98						
20.00	26.98		26.98	26.98		26.98	26.98 26.98	26.98		26.98		26.98
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2700	26.99	26.99 26.99	26.99	26.99 26.99		26.99 26.99	26.99 26.99		26.99	26.99		26.99
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270 270	27.00 27.00											
2761	27.01		27.01	27.01		27.01	27.01			27.01		27.01
2760	27.01 27.01		27.01 27.01	27.01 27.01	27.01 27.01							
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179.0	27.03 27.03											
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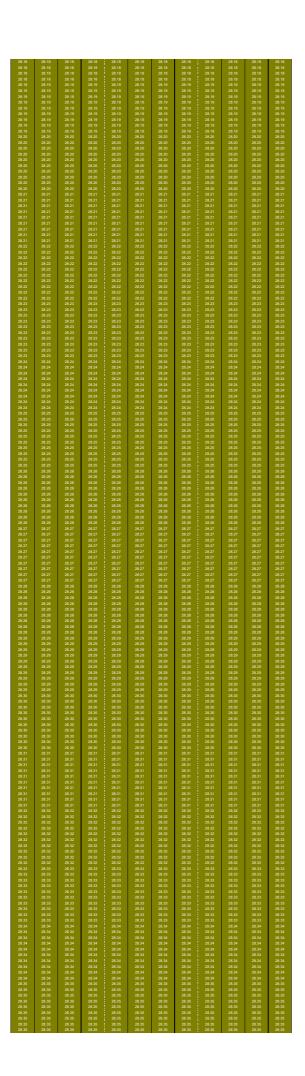
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27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.56 27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57
27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57	27.57 27.57 27.57
27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57	27.57 27.57
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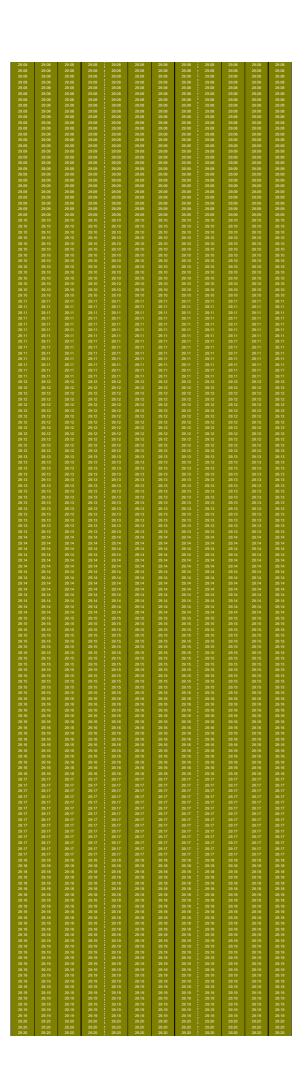
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28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72		28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72
28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72	28.72 28.72 28.72
28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72	28.72 28.72
28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73	28.72 28.72 28.73
28.73 28.73 28.73	28.73 28.73	28.73 28.73	28.73 28.73	28.73 28.73 28.73	28.73 28.73	28.73 28.73	28.73 28.73 28.73 28.73	28.73 28.73	28.73 28.73	28.73 28.73	28.73 28.73
28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73	28.73 28.73 28.73
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28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74	28.73 28.74 28.74
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2016		29.51 29.52	29.51 29.52	29.51						29.51 29.52	29.51 29.52	29.51 29.52
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29.67 29.67 29.68	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67	29.67 29.67
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29.72 29.72 29.72	29.72 29.72 29.72				29.72 29.72 29.72		29.72 29.72 29.72			29.72 29.72 29.72	29.72
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29.73 29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73	29.73 29.73 29.73
	29.73 29.74 29.74	29.73 29.74	29.73 29.74	29.73 29.74	29.73 29.74	29.73 29.74 29.74		29.73 29.74	29.73 29.74	29.73 29.74	29.73 29.74 29.74
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29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74	29.74 29.74 29.74 29.74	29.74 29.74 29.74
	29.74 29.74 29.74	29.74 29.74 29.74	29.74	29.74 29.74 29.74			29.74 29.74 29.74				29.74
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29.74 29.74	29.74 29.74	29.74 29.74	29.74 29.74	29.74 29.74 29.74 29.74	29.74 29.74	29.74 29.74	29.74 29.74 29.74	29.74 29.74	29.74 29.74	29.74 29.74	29.74 29.74
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29.74	29.74	29.74	29.74	29.74	29.74	29.74	29.74	29.74	29.74	29.74	29.74
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75 29.75 29.75	29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75	29.75 29.75 29.75
	29.75 29.75		29.75								29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75	29.75
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29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
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29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76	29.76
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Gains due to alte improvement

Note: Note, Cb, bases are calculated using two approaches: PCC default methodology and more site specific equations derived for this project. The PCC methodology is included because it is the established approach, although it contains not included. The west equation is that been throughly leaded approach gains (or permission and included in the reversal contains and included in the expectation is that been throughly leaded approach gains (or permission and included in the project.)

Selected Methodology = IPCC default

peatland =	

Reduction in GHG emissions due to improvement of site		Expecte	d result			Minimur	m result			Maximu	m result	
	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &	Degraded Bog	Felled Forestry	Borrow Pits	Foundations &
Improvement of	Degitated Dog	T chica T orestry	Dollow 1 its	Hardstanding	Degraded Dog	r chear orestry	DOTTOW 1 ILD	Hardstanding	Degraded Dog	renear oresay	201101111113	Hardstanding
Description of site Period of time when effectiveness of the improvement can be guaranteed (years)	2	2	2	40	2	2	2	40	2	2	2	40
Area to be improved (ha)	0	0	0	0	0	0	0	0	0	0	0	0
Average air temperature at site (°C)	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1	10.1
Depth of peat drained (m)	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34	0.34
Depth of peat above water table before improvement (m)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Depth of peat above water table after improvement (m)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2. Losses with improvement												
Flooded period (days year ⁻¹)	178	178	178	178	178	178	178	178	178	178	178	178
Time required for hydrology and habitat to return to its previous state on restoration	2	2	1	0	2	2	1	0	2	2	1	0
(years) Improved period (years)	0	0	1	40	0	0	1	40	0	0	- 1	40
Methane emissions from improved land			-	40				40	,	U		40
Site specific methane emission from improved soil on acid bogs (t CH _a -C ha ⁻¹ yr ⁻¹)	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499
Site specific methane emission from improved soil on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499
IPCC annual rate of methane emission on acid boos (t CHC ha ⁻¹ vr ⁻¹)	0.040	0.040	0.040	0.040	0.040	0.040	0.560	0.980	0.040	0.040	0.040	0.040
IPCC annual rate of methane emission on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219	0.219
Selected annual rate of methane emission (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
CH ₄ emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from improved land												
Site specific CO ₂ emission from improved soil on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56
Site specific CO ₂ emissions from improved soil on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73
IPCC annual rate of carbon dioxide emission on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
IPCC annual rate of carbon dioxide emission on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Selected annual rate of carbon dioxide emission (t CO ₂ ha ⁻¹ yr ⁻¹)	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
CO ₂ emissions from improved land (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
3. Losses without improvement												
Flooded period (days year ⁻¹)	0	0	0	0	0	0	0	0	0	0	0	0
Time required for hydrology and habitat to return to its previous state on restoration	2	2	1	0	2	2	1	0	2	2	1	0
(years) Improved period (years)	0	0	1	40	0	0	1	40	0	0	1	40
Methane emissions from unimproved land	U	U		40	U	U		40	U	U		40
Site specific methane emission from unimproved soil on acid bogs (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499	0.499
Site specific methane emission from unimproved soil on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.560	0.560	0.560	0.560	0.560	0.560	0.560	0.560	0.560	0.560	0.560	0.560
IPCC annual rate of methane emission on acid bogs (t CH _a -C ha ⁻¹ yr ⁻¹)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
IPCC annual rate of methane emission on fens (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.000	0.000		0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
			0.000									
Selected annual rate of methane emission (t CH ₄ -C ha ⁻¹ yr ⁻¹)	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
CH ₄ emissions from unimproved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Carbon dioxide emissions from unimproved land	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50	0.50
Site specific CO ₂ emission from unimproved soil on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56
Site specific CO ₂ emissions from unimproved soil on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73	5.73
IPCC annual rate of carbon dioxide emission on acid bogs (t CO ₂ ha ⁻¹ yr ⁻¹)	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
IPCC annual rate of carbon dioxide emission on fens (t CO ₂ ha ⁻¹ yr ⁻¹)	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
Selected annual rate of carbon dioxide emission (t CO ₂ ha ⁻¹ yr ⁻¹)	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20
CO ₂ emissions from unimproved land (t CO ₂)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
RESULTS												
4. Reduction in GHG emissions due to improvement of site												
Total GHG emissions from improved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Total GHG emissions from unimproved land (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Reduction in GHG emissions due to improvement (t CO ₂ equiv.)	0	0	0	0	0	0	0	0	0	0	0	0
Additional CO ₂ payback time of windfarm due to site improvement												
coal-fired electricity generation (months)	0	0	0	0	0	0	0	0	0	0	0	0
grid-mix of electricity generation (months)	0	0	0	. 0	0	U	0	. 0	0	U	0	0
fossil fuel - mix of electricity generation (months)	0	0	0	0	0	o	0			n	0	0

Click here to move to Payback Time Click here

Gains due to site improvement

Note: Note, Clb, bisses are calculated using two approaches: PCC default methodology and more site specific equations derived for this project. The PCC methodology is included because it is the established approach, although it contains no site detail. The reve equations have been thoroughly tested against experimental data (see Nayak et al., 2009. - Final report).

_	Note Methons ensistion from and Exp. Equation defined by regreation analysis against 57 measurements (Mysel, at 2009). The equation derived was $R_{\rm col} \approx 10000000 \times 10000000000000000000000000$	
	$R_{\rm cut} = 1.6771000) \times ((6700 \times expl-0.26 \times expl-0.0515 \times ((Wx100)-50)))) + ((72.54 \times T) - 800))$ where $R_{\rm cut}$ the manual rate OCQ, retination (CQC (fast) 4 yr ⁴). 4 average annual peak temperature (C) and (Wx100 4 yr ⁴) is the value table depth (m). The equation shows a significant correlation with measurements ($r^2 \cdot 0.51 \cdot 9 \cdot 7 \cdot 6.05$) and an automost provided ($r^2 \cdot 0.21 \cdot 9 \cdot 7 \cdot 6.05$) and an automost provided ($r^2 \cdot 0.21 \cdot 9 \cdot 7 \cdot 6.05$) and an automost provided ($r^2 \cdot 0.21 \cdot 9 \cdot 7 \cdot 6.05$).	
\	Note: Cathor disolde missions from fem. Equation derived by regression analysis against 44 missions from fem. Equation derived by regression analysis against 44 missions regression analysis against 44 missions fem. (2018) The equation derived by regression analysis against 45 missions fem. (2018) The equation of the against and of CQ, emissions (CQ, bit b)* p* 1. With the waiter face day of the equation of the against analysis of the equation of these against analysis against corrections with missions regressions (p* 1-14,2 p-3,001). With the waiter face day of the equation of the	

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Frequently Asked Questions

Click here to email question

GENERAL

Syin Yi Phoon (Senior Hydrologist, EnviroCentre Ltd)

I could see the benefit of protected feature on the all the sheets, but it this means we cannot even copy the equations for testing sensitivity of a parameter without changing the entire sheet. The

protection should be removed as it reduces the usefulness of the tool.

Response: Syin Yi Phoon (Senior Hydrologist, EnviroCentre Ltd)

We miss the carbon payback table that used to be at the bottom of every carbon gain/loss component. Our clients like to see how quickly they can payback C emitted due to individual Comment:

components. This is useful in planning and should be replaced.

Response: This feature has been replaced

CORE INPUT DATA

Cameron McIver (Cameron Ecology Ltd)

The note on "extra capacity required for backup (%)" suggests there is a choice of % capacity or % output - I'm not clear how you know which you have chosen. Question:

Response: The note is misleading. The number that should be entered is the percentage of the actual output of the windfarm (MWh yr -1) that is required for backup. Text has been added to the note to clarify

Stephen Lockett (AECOM)

Question:

Average extent of drainage around drainage features at site (m)

We have reviewed the guidance but are still unsure of what this variable means. We have used a standard input of 100m but the sheet appears to be extremely sensitive to this variable and we have limited confidence on the value chosen. The note in the cell refers to obtaining data on the ground water level but I am unsure how this relates to extent of drainage around drainage

features

Average extent of drainage around each drainage feature can be measured following the method by Stewart and Lance (1991). In order to determine the extent of drainage, the undrained water Response: table depth, and the 95% confidence interval of the measurements are needed.

Possible approach:

1. Install a series of dipwells or boreholes both upslope and downslope from the drainage feature.

2. In the first instance, assume that all dipwells are from undrained areas of the site. This incorrect assumption is used to initialise the iterative process that calculated the water table depth of the undrained soil.

3. For a particular sampling occasion, calculate the mean water table depth and 95% confidence interval from all the available data.

4. Assume all dipwells with water table depths deeper than the calculated mean water table depth plus the 95% confidence interval are within the area that is drained by a ditch and so exclude these from the calculation.

5. Calculate a new mean water table depth and 95% confidence interval using only data from undrained area.

6. Repeat the process until the calculation of the mean water table depth and 95% confidence interval has stabilised, and no further data points need to be excluded. This gives the water table depth of the undrained soil.

7. The distance from the drain to the first dipwell where the water table depth of the undrained soil occurred (to within the 95% confidence interval) can then be assumed to be the total extent of the drainage impact.

Question:

Our drainage strategy is to mimic the existing drainage patterns as closely as possible by intercepting surface run-off and discharging at regular intervals downstream of the tracks back onto

natural ground. As such, is there an argument this value could be effectively zero? Response:

No - removing water increases the drainage of the site, and this needs to be accounted for. However, if you are following existing drainage patters, it will be easier to determine the extent of drainage because the drains are already established.

For our example site there is a significant difference in pay back when using site specific and IPCC default values (ranging from 3 to 15 years). Would you be able to provide a brief description of Question:

what is being ignored when selecting IPCC default?

The IPCC default takes no account of the previous condition of the site. It provides the result for a typical acid bog or fen across Europe. Response: Therefore, if you are working with an unusually pristine peat or a badly drained peat, you would expect the result to be very different to the average.

Tanya Ogilvy (SEPA)

5c. Volume of peat drained Stephen Lockett (AECOM)

Question:

Our new drainage will be surface swales above the ground water table so should not have any effect on the ground water table.

If the surface swales will just convey storm water that would not otherwise have percolated into the soil, these swales will have no impact on the water table of the soil profile, but will only impact the water that would have runoff the surface, causing erosion. However, if the swales also reduce the amount of water entering the soil profile, then they could have an impact on the wetness of the soil. This should really be accounted for in the calculation. However, there is nothing to describe this in the carbon calculator, so you would be justified in neglecting this effect but need to indicate this in the note

Question:

5e. Emission rates from soils Stephen Lockett (AECOM)

We would expect the rate of emission in undrained soil to be worse than the rate in drained soil. This is only the case when the ground water level is very shallow. Does the output define 'drained soil' as soil which is being drained by our engineering activities and 'undrained soil' as excavated soil which was dry to start with?

Response:

I think the confusion comes about due to the definition of terms.

The "drained soil" refers to the soil after it has been drained for the windfarm development. The "undrained soil" refers to the soil before it was drained for the development. This doesn't refer to the status of the site before the development. Agreed, where a "drained site" refers to a site that has already been drained for a number of years, much of the labile carbon would already have been lost, and so losses due to the windfarm construction would be much less than the losses from an "undrained site" where the peat was still in pristine condition. Worksheet 5e calculates the rate of emissions of CO2 and CH4 for the soil

1. when drained (ie dry soil);

2. when undrained (ie wet soil)

In a drained (dry) soil, we expect high rates of CO2 emissions and low rates of CH4 emissions.

In an undrained (wet) soil, we expect high rates of CH4 emissions and low rates of CO2 emissions

These rates are then used in sheet 5d to calculate the net GHG emissions (in CO2 equivalents) attributable to the windfarm development. This is taken as the difference between the losses following drainage for the development and the losses that were occurring before the soil was drained for the development. Because the net emissions are usually higher in the drained (dry) soil than in the undrained (wet) soil, the net emissions due to draining the site usually come out as positive. If we were to compare a "drained site" and an "undrained site" in sheet 5d, the net CO2 emissions calculated for the drained site would be much less than for the undrained site because a smaller volume of soil is being further drained by the development

CHANGES IN VERSION 2.1.0			
Worksheet Core input data	Cells C31, E31, F31	<u>Change</u> Redundant input for soil pH removed	Thanks to Ffion Causer, Natural Power
Forestry input data	C31, E31, 1 31	Different areas of forestry included	N/A
Construction input data		Different areas of construction included	
Windfarm CO ₂ emission savings		Different areas of forestry included	
 CO2 loss due to turbine life Volume of peat removed 		Different areas of construction included Different areas of construction included	
7ii. Forestry CO2 loss - detail		Different areas of construction included	
7a. C sequest. in trees (3PG)		Different areas of forestry included	
7d. Wind speed ratios		Different areas of forestry included	
CHANGES IN VERSION 220			
<u>Worksheet</u>	<u>Cells</u>	Change	Thanks to
Construction input data	C28, C29	"Volume cement" changed to "Volume concrete"	Marianne Brownlee, Arcus Renewable Energy Consulting Ltd
Windfarm CO ₂ emission saving	F49	=IF(F19=1,365*24*F11*F10*G21/100,SUM(I49,L49,O49,R49,U49)) changed to =IF(D19=1,365*24*F11*F10*G21/100,SUM(I49,L49,O49,R49,U49))	Cameron McIver, Cameron Ecology Ltd
CHANGES BUILDED CONTO		-1 (025-2505 24 + 12 + 10 0223200)2011(143)243)(045)(143)(045)(1	
CHANGES IN VERSION 2.3.0	_		
Worksheet 5a. Volume of peat removed	Cells F23	Change =IF('Core input data'!C48=1,'Core input data'!C51,'Construction input data'!D17) changed to	Thanks to Stuart McGowan, Golder Associates
		=IF('Core input data'!C48=1,'Core input data'!C49,'Construction input data'!D17)	
5a. Volume of peat removed 5a. Volume of peat removed	G23,H23 F24	Similar to above =IF('Core input data'!C48=1,'Core input data'!C52,'Construction input data'!D18) changed to	
		=IF('Core input data'!C48=1,'Core input data'!C50,'Construction input data'!D18)	
5a. Volume of peat removed	G24,H24	Similar to above	
CHANGES IN VERSION 2.4.0	=		
Worksheet	Cells	Change	Thanks to
5c. Volume of peat drained	F ₃₃	=(\$C9+F31+\$C9)*(\$C9+F32+\$C9)-(F31*F32) changed to	Stuart McGowan, Golder Associates
5c. Volume of peat drained	G ₃₃ -T ₃₃	=IF(F23>0,(\$C9+F31+\$C9)*(\$C9+F32+\$C9)-(F31*F32),0) Similar to above	
		Similar to above	
CHANGES IN VERSION 2.5.0	_		
Worksheet	Cells	Change	Thanks to
7ii. Forestry CO2 loss - detail 7ii. Forestry CO2 loss - detail	F ₅₅ G ₅₅ -T ₅₅	=F50*F53/F54 changed to =IF(F50>0,F50*F53/F54,0) Similar to above	Jenny Sneddon, AMEC
7ii. Forestry CO2 loss - detail	F46	=IF(F35="Yes", F44*F45, o) changed to =IF(F35="Yes", IF(F39>o, F44*F45, o), o)	
7ii. Forestry CO2 loss - detail 7ii. Forestry CO2 loss - detail	G46-T46 F63	Similar to above =(F57*'Core input data'!\$E41)-F62 changed to =IF(F55>0,(F57*'Core input data'!\$C41)-F62,0)	
7ii. Forestry CO2 loss - detail 7ii. Forestry CO2 loss - detail	G63-T63 G38	Similar to above ='Forestry input data'!sF39 changed to ='Forestry input data'!sH39	
7ii. Forestry CO2 loss - detail	J38,M38,P38,S38	Similar to above	
7ii. Forestry CO2 loss - detail 7ii. Forestry CO2 loss - detail	H ₃ 8 K ₃ 8,N ₃ 8,Q ₃ 8,T ₃ 8	='Forestry input data'!\$H39 changed to ='Forestry input data'!\$F39 Similar to above	
ii. Forestry CO2 loss - detail	D66	=D17+D24+D32-D47-D63 changed to =D17+D24+D32-E47-E63	
7ii. Forestry CO2 loss - detail 7ii. Forestry CO2 loss - detail	G66, J66, M66, P66, S66 E66	Similar to above =E17+E24+E32-E47-E63 changed to =E17+E24+E32-D47-D63	
7ii. Forestry CO2 loss - detail	H66, K66, N66, Q66, T66	Similar to above	
5c. Volume of peat drained 5c. Volume of peat drained	C ₅₄ D ₅₄ , E ₅₄	='Core input data'!C68 changed to ='Core input data'!C70 Similar to above	SEPA
5c. Volume of peat drained	D48	='Core input data'!Cs65 changed to ='Core input data'!Es65	
5c. Volume of peat drained 5c. Volume of peat drained	E48	Similar to above =IF(G23>o,(\$C9+G31+\$C9)*(\$C9+G32+\$C9)-(G31*G32),o) changed to	
Sc. volume of peat drained	G ₃₃	=IF(G23>0,(\$d9+G31+\$d9)*(\$d9+G32+\$d9)-(G31*G32),0)	
5c. Volume of peat drained 5c. Volume of peat drained	J ₃₃ ,M ₃₃ ,P ₃₃ ,S ₃₃ H ₃₃	Similar to above =IF(H23>o,(\$C9+H31+\$C9)*(\$C9+H32+\$C9)-(H31*H32),o) changed to	
		=IF(H23>o,(\$e9+H31+\$e9)*(\$e9+H32+\$e9)-(H31*H32),0)	
5c. Volume of peat drained	J ₃₃ ,M ₃₃ ,P ₃₃ ,S ₃₃	Similar to above	
CHANGES IN VERSION 2.6.0	_		
	Cells	Change	Thanks to
Worksheet		=D\$31/D9 changed to =D\$31/E9 Similar to above	Sarah Lister, Natural Power
Payback Time and CO2 emissions	D ₃₃		Salar Elster, National Force
Payback Time and CO2 emissions Payback Time and CO2 emissions	D ₃₄ ,D ₃₅	=E\$31/E9 changed to =E\$31/D9	Sudi Este, National Office
Payback Time and CO2 emissions Payback Time and CO2 emissions Payback Time and CO2 emissions Payback Time and CO2 emissions	D ₃₄ ,D ₃₅ E ₃₃ E ₃₄ , E ₃₅	=Es31/E9 changed to =Es31/D9 Similar to above	Saut Ester, read at the
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Payback Time and CO2 emissions Payback Time and CO2 emissions 6. CO2 loss by DOC & POC loss 6. CO2 loss by DOC & POC loss 7. CO2 loss by DOC & POC loss 8. CO2 loss by DOC & POC loss 9. CO2 loss by DOC & POC loss 9. CO2 loss by DOC & POC loss 9. Loss by DOC & POC loss 9. Loss by DOC & POC loss 1. Windfarm CO2 emission saving 9. Emission rates from soils 9. Emission rates	D34, D35 E33 E34, E35 D31 E31 C31 D31, E31 C26 C32 Row 25 D48 E37 F37-U37 C34 D34, E34	=E531/E5 changed to =E531/D9 Similar to above =D319-D35 changed to =D319-E35 =E539-E35 changed to =D319-E35 Contents deleted Similar to above =(C9-C12+C32+C14+C15+(C10+C32+C18+C19+C20)(C21)/3-66 changed to =(C9-C12+C32+C14+C15+(C10+C32+C18+C19+C20)(C21)/3-66 changed to =(C9-C12+C32+C14+C15+(C10+C32+C18+C19+C20)(C21)/3-66 changed to =(C9-C12+C32+C14+C15)/3-66) (((C10+C32+C38+C39+C30)(C21)/3-(21)/6) Wording changed to dairly that the tool SHOULD be used with highly organic soils, but COULD also be used with sites undergoing drainage or deforestation Set to 2 g and fixed to comply with planning applications for Section 36 (planning period = 25 years) Average depth of peat at site not used - therefore removed Set to AVERAGE(C48,14,8,Ma,8,24,8,24,8) to ensure a value is provided 24*365*4D11 changed to 24*365*E11 Similar to above =C38/(C37*10000) changed to =MAX(C28/(C27*10000),C33) Similar to above Change =-12*C60/1-Windfarm CO2 emission saving*15D54 changed to =-12*C60/1-Windfarm CO2	Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power
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Payback Time and CO2 emissions So. CO2 loss by DOC & POC loss	D34,D35 E33 E34,E35 D31 E31 C31 D31,E11 C26 C12 Row 25 D48 E37 F37-U37 C34 D34,E34	=E331/E3 changed to =E331/D9 Similar to above D319-D32 changed to D319-E35 E319-E32 changed to D319-E35 E319-E32 changed to E319-D35 Contents deleted Similar to above (C9-C12+C13)*C14-C13)*661+((C10+C12)*C18+C13+C20)(C21)*(12)(6) Similar to above (C9-C12+C13)*C14-C13)*661+((C10+C12)*C18+C13+C20)(C21)*(12)(6) Similar to above Wording changed to clarify that the tool SHOULD be used with highly organic soils, but COULD also be used with sites undergoing drainage or deforestation Set to 25 and fixed to comply with planning applications for Section 36 (planning period = 25 years) Average depth of peat at site not used - therefore removed Set to AVERAGE(G4,8,14,8,M48,P48,S48) to ensure a value is provided 247-56*9101 changed to 24*36*5*E11 Similar to above	Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power
Payback Time and CO2 emissions So. CO2 loss by DOC & POC loss	D34,D35 E33 E34,E35 D31 E31 C31 D31,E31 C26 D26,E26 C12 Row 25 D48 E37 D34,E34	=E\$31/E\$ changed to =E\$31/D\$ Similar to above D319-D32 changed to D319-E35 E139-E32 changed to D319-E35 Contents deleted Similar to above #(C9+C12+C31+C13+C13+C13+C13+C13+C20)(C21)(3 66 changed to #(C9+C12+C31+C13+C13+C13+C13+C13+C13+C13+C20)(C21)(21)(3 66 changed to #(C9+C12+C31+C13+C13+C13+C13+C13+C13+C13+C13+C13	Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power
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Payback Time and CO2 emissions 5. CO2 loss by DOC & POC loss 5. CO2 loss 5. C	D34,D35 E33 E34,E35 D31 E31 C31 D31,E31 C26 D26,E26 C12 Row 25 D48 E37 C34 D34,E34	=Es3;Eg changed to =Es3;IDg Similar to above D3;9-D3; changed to =Es3;IDg Similar to above D3;9-D3; changed to =Es3;D3; Contents deleted Similar to above =(Cg-C12+C3;+C1;+C5;+C10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C1;+C5;+C3);66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+(IC10+C3)(C3);66 changed to =(Cg-C12+C3;+C3);66)+(IC10+C3)(C3);66 changed to =(Cg-C12+C3;+C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power
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Payback Time and CO2 emissions 5. CO2 loss by DOC & POC loss 5. CO2 loss 5. C	D34,D35 E33 E34,E35 D31 E31 C31 D31,E31 C26 D26,E26 C12 Row 25 D48 E37 C34 D34,E34	=Es3;Eg changed to =Es3;IDg Similar to above D3;9-D3; changed to =Es3;IDg Similar to above D3;9-D3; changed to =Es3;D3; Contents deleted Similar to above =(Cg-C12+C3;+C1;+C5;+C10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C1;+C5;+C3);66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+((IC10+C12+C18+C3;+C20)(C2;1)3;66 changed to =(Cg-C12+C3;+C14+C3;)3;66)+(IC10+C3)(C3);66 changed to =(Cg-C12+C3;+C3);66)+(IC10+C3)(C3);66 changed to =(Cg-C12+C3;+C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(C3)(Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power Rob McCall, Countryside Council for Wales
Payback Time and CO2 emissions 5. CO2 loss by DOC & POC loss 5. CO2 loss 5. CO2 loss by DOC & POC loss 5. CO2 loss by DOC & POC loss 5. CO2 loss 5. CO2 loss by DOC & POC loss 5. C	D34,D35 E33 E34,E35 D31 E31 C31 D31,E31 C26 D26,E26 C12 Row 25 D48 E37 C34 D34,E34	=Es31/Eg changed to =Es31/Dg Similar to above D319-D32 changed to =B31/D35 Similar to above D319-D32 changed to =B31-D35 Contents deleted Similar to above =(Cg-C12+C319-C14-C53)-E60+C12+C18+C39+C20)(C21)3/, 66 changed to =(Cg-C12+C319-C14-C53)-E60+C12+C18+C39+C20)(C21)3/, 66 changed to =(Cg-C12+C319-C14-C53)-E60+C12+C319-C30)(C21)3/, 66 changed to =(Cg-C12-C319-C14-C53)-E60+C12+C319-C30)(C31)3/, 66 changed to =(Cg-C12-C319-C14-C319)-E60+C12+C319-C30)(C31)3/, 66 changed to =(Cg-C12-C312-C14-C319)-E60+C319-E60+C319-C319-C319-C319-C319-C319-C319-C319-	Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power Rob McCall, Countryside Council for Wales
Ayaback Time and CO2 emissions Ayaback Time and CO2 emissions Payback Time and CO2 emissions So. CO2 loss Do2 POC LOSS DO3	D34, D35 E33 E34, E35 D31 E31 C31 D31, E31 C36 C32 C34	### ### ### ### ### ### ### ### ### ##	Ffion Causer, Natural Power SEPA Sarah Lister, Natural Power Ffion Causer, Natural Power Thanks to Sarah Lister, Natural Power Rob McCall, Countryside Council for Wales

/orksheet	Cells	Change	Comment	Thanks to
CO2 gain - site improvement	C13	='Core input data'!C80 changed to =IF('Core input data'!C81>'Core input data'!C82,'Core input data'!C80,o)		Ffion Causer, Natural Power
	G13, K13	Similar to above		
	D13	='Core input data'!C85 changed to =IF('Core input data'!C86>'Core input data'!C87,'Core input data'!C85,o)		
	H13,L13	Similar to above		
	E13	='Core input data'!C90 changed to =IF('Core input data'!C91>'Core input data'!C92,'Core input data'!C90,0)		
	l13, M13	Similar to above		
	F13	='5c. Volume of peat drained'!C34/10000 changed to =IF('Core input data'!C95>'Core input data'!C96,'5c. Volume of peat drained'!C34/10000,0)		
	J13, N13	Similar to above		

CHANGES IN VERSION 2.8.	0_			
Worksheet cc. Volume of peat drained	<u>Cells</u> Rows 67 - 76	<u>Change</u> Inserted rows to included additional excavated peat in volume of peat drained	Comment Include additional excavated peat	Thanks to Susana Sebastian, SEPA
	C67-C68; D67-D68; E67-E68	Title lines	in volume of peat drained	
	C69	='Core input data'!C74		
	D69,E69	Similar to above ='Core input data'!C75		
	C70 D70,E70	= Core input data: 1275 Similar to above		
	C71	=IF(C7o>o,C6g/C7o,o)		
	D71,E71	Similar to above		
	C72	=SQRT(C70/PI())		
	D72,E72	Similar to above		
	C73	=C72+C9 Similar to above		
	D73,E73 C74	=(PI()*C73*C73)-C70		
	D74,E74	Similar to above		
	C ₇₅	=C74*C71		
	D75,E75	Similar to above		
	C ₇₉	=C18+C34+C57+C64 changed to =C18+C34+C57+C64+C74		
	D79,E79 C8o	Similar to above		
	D80,E80	=C19+C35+C58+C65 changed to =C19+C35+C58+C65+C75 Similar to above		
rii. Forestry CO2 loss - detail	F62	=F60*F61 changed to =F60*F61*F55	Calculation of emissions	Susana Sebastian, SEPA
*		= ***	associated to the transport of	•
	CC - TC -	Clarificate above	wood to biomass plant should	
orestry input data	G62-T62 C23	Similar to above	account for number of trips to	
		Units changed from g CO2 km ⁻¹ to g CO2 km ⁻¹ t ⁻¹	plant Limit improvements following	Sucana Sahartian CEDA
Core input data B. CO2 gain - site improvement	Row 25 Row 15	Insert input for average depth of peat at site Insert average depth of peat at site	Limit improvements following restoration to the depth of the	Susana Sebastian, SEPA
s. coz gam site improvement	C15	='Core input data'!C25	peat	
	D15-N15 (excl. E15, l15 & M15)			
	E15	='Core input data'!C46		
	l15,M15	Similar to above		
	C16	Core input data!!C82 changed to =IF('Core input data'!C82 <c15,'core data'!c82,c15)<="" input="" td=""><td></td><td></td></c15,'core>		
	D16-N16	Similar to above		
	C17	='Core input data'!C83 changed to =IF('Core input data'!C83 <c15,'core data'!c83,c15)<="" input="" td=""><td></td><td></td></c15,'core>		
	,			
	D17-N17	Similar to above		
	C21	C12-C20 changed to =IF(C12-C20>0,C12-C20,0)		
	D21-N21	Similar to above		
Core input data 3. CO2 gain - site improvement	Rows 85, 91, 97 C12	Insert period of time when the improvement can be guaranteed to work (years) ='Core input data'!C12 changed to ='Core input data'!C85	Improvements in C sequestration should continue for as long as the	Rob McCall, NRW
s. CO2 gain - site improvement	D12-N12 (excl. E12, l12 & M12		improvement can be guaranteed.	
Payback Time and CO2 emissions	Row 37	Insert ratio of soil carbon loss to gain by restoration	Include calculation of ratio of soil	Rob McCall, NRW
	C ₃₇	=IF(C26<0,-(C17+C18)/C26,0)	losses to gains	
	D6 ₃₇ ,E ₃₇	Similar to above		
Payback Time and CO2 emissions	Row 38	Insert ratio of C emissions to power generation	Include calculation of C emissions	Susana Sebastian, SEPA
	C38	=((C20+C26)*1000000)/(C12*1000) Similar to above	to power generation	
. Loss of soil CO2	D637,E37 D11	=D8+D9 changed to =MIN(D8+D9,E8+E9)	Correct use of minimum and	Peter Batten
. 2033 0. 3011 CO2	E11	=E8+E9 changed to =MAX(D8+D9,E8+E9)	maximum wrt water table depth at	
e. Emission rates from soils	D31	='Core input data'!E24 changed to ='Core input data'!G24	very low depths	
	E31	='Core input data'!G24 changed to ='Core input data'!E24		
	D ₃₃	='Core input data'!E28 changed to ='Core input data'!G28		
COs sais sits is	E33	='Core input data'!G28 changed to ='Core input data'!E28	Connections of militarian and	to Conitis Hairardity of Abandan
. CO2 gain - site improvement	G17	=IF('Core input data'!E83 <g15, 'core="" changed="" data'!e83,g15)="" data'!g83,g15)<="" data'!g83<g15,="" input="" td="" to="IF('Core"><td>Correct use of minimum and maximum depth of water table</td><td>Jo Smith, University of Aberdeen</td></g15,>	Correct use of minimum and maximum depth of water table	Jo Smith, University of Aberdeen
	H17-J17	Similar to above	after restoration	
	K17	=IF('Core input data'!G83 <k15,'core changed="" data'!g83,k15)="" input="" input<="" td="" to="IF('Core"><td>arter restoration</td><td></td></k15,'core>	arter restoration	
		data'!E83 <k15,'core data'!e83,k15)<="" input="" td=""><td></td><td></td></k15,'core>		
	L17-N17	Similar to above		
. CO2 gain - site improvement	G12	='Core input data'!E85 changed to ='Core input data'!G85	Correct use of min/max period	Jo Smith, University of Aberdeen
	H12-J12	Similar to above	when restoration can be restored	
	K12 L12-N12	='Core input data'!G85 changed to ='Core input data'!E85 Similar to above		
3. CO2 gain - site improvement	C34	=IF('Core input data'!\$C\$112=2,'8. CO2 gain - site improvement'!C30,'8. CO2 gain - site	Correct selection of emission	Elizabeth Keen, Peter Brett Associates LLP
		improvement'!C32) changed to =IF('Core input data'!\$C\$112=2,IF('Core input	factor when soil type is fen	
	D N	data'!\$C\$23=1,C30,C31),IF('Core input data'!\$C\$23=1,C32,C33))		
	D34-N34	Similar to above		
	C ₅₃	=IF('Core input data'!\$C\$112=2,'8. CO2 gain - site improvement'!C49,'8. CO2 gain - site improvement'!C51) changed to =IF('Core input data'!\$C\$112=2,IF('Core input data')		
		improvement: C51/ cridinged to =ir(Core input data: \$C\$112=2,ir(Core input		
	D ₅₃ -N ₅₃	data'!\$C\$23=1,C49,C50),IF('Core input data'!\$C\$23=1,C51,C52)) Similar to above		

Vorksheet	Cells	<u>Change</u>	Comment	Thanks to
Core input data	B94	"Water table depth in borrow pit before restoration (m)" changed to "Depth of water table in borrow pit before restoration with respect to the restored surface (m)"	Confusing wording as water table depth may always be entered as	Clare Wharmby - Carbon Forecast
	B ₉₅	"Water table depth in borrow pit after restoration (m)" changed to "Depth of water table in borrow pit after restoration with respect to the restored surface (m)"	zero.	
. CO2 gain - site improvement	C47	=(23*16/12)*C\$13*C\$4,0*C4,6*(C\$19/36\$) changed to =(23*16/12)*C\$13*C\$4,0*C4,6*(C\$38/36\$)	Error in formula using the improved flooded period instead of the unimproved flooded period	Elizabeth Keen - Peter brett Associates
	D47-N47	Similar to above		
rc. Average stand data	Rows 13-29	Stand data extended from 17 year to 0 years	If forest stand is less than 17 years old, the calculations fail	Brenda Park - AMEC
	Rows 168-86	Similar to above	•	
ii. Forestry CO2 loss - detail	F ₃₁	=IF (F29>0,IF(F27="Deep Peat",(VLOOKUP(F29,'7c. Average stand data'!\$D\$87:\$G\$118,3)), (VLOOKUP(F29,'7c. Average stand data'!\$D\$90:\$G\$63,3))),o) changed to		
	G31-T31	=IF(F29>0,IF(F27="Deep Peat",(VLOOKUP(F29,'7c. Average stand data!!\$D\$68:\$G\$118,3)), Similar to above		
ii. Forestry CO2 loss - detail	G35	=IF(Forestry input data'!sFs33=1,"Yes", "No") changed to =IF(Forestry input data'!sDs33=1,"Yes", "No")	Use of felled wood as biofuel not correctly read in min and max calculations	Jo Smith - University of Aberdeen
	H35,J35,K35,M35,N35,P35,Q3 5,S35,T35	Similar to above		
ii. Forestry CO2 loss - detail	F16	='7a. C sequest. in trees (3PG)'!\$F\$24_changed to =IF(F12>0,'7a. C sequest. in trees (3PG)'!F\$24,0)	Avoid #NA	Claire Frost - AECOM
	G16-T16	Similar to above		
orestry input data	Note: Emissions from felling and timber removal.	"the emissions are 6657 g CO ₂ m ⁻³ " changed to "the emissions are 6675 g CO ₂ m ⁻³ "		Jonathon Davison - Mott MacDonald
orestry input data	Note: Emissions associated	"3933000 g CO ₂ km ⁻¹ (range 3850000 – 4015000 g CO ₂ km ⁻¹ - average = 39.33 g CO ₂ km ⁻¹ t ⁻¹)"		Jonathon Davison - Mott MacDonald
	with transportation	changed to "39.33 g CO ₂ km ⁻¹ t ⁻¹ (range 38.5 – 40.15 g CO ₂ km ⁻¹ t ⁻¹ - average = 39.33 g CO ₂ km ⁻¹	r	
		7"		
Payback Time and CO2 emissions	C ₃₇ D6 ₃₇ ,E ₃₇	=IF(C26<0,-(C17+C18)/C26,"No gains!") Similar to above	Ensure no restoration is highlighted as no gains rather than	Sarah Lister, Natural Power
ayback Time and CO2 emissions	C38	=((12/44)*(C20+C26)*1000000)/(C12*1000)	Express ratio as CO2 rather than C	Sarah Lister, Natural Power
	D637,E37	Similar to above	emissions to power generation	

CHANGES IN VERSION 2.10.0	<u>)</u>			
Worksheet 3. CO2 gain - site improvement	Cells K13	Change =IF('Core input data'IG82>'Core input data'IG83,'Core input data'IG81,0) changed to =IF('Core input data'IG82>'Core input data'IG81,0)	Comment Change to correct test for improvement in restored area.	Thanks to Sarah Lister, Natural Power
	L13-N13 G13	Similar to above =IF('Core input data'!E82>'Core input data'!E83,'Core input data'!E81,0) changed to =IF('Core input data'!E82>'Core input data'!E82>(Ore input data'!E83,0)		
ayback Time and CO2 emissions	H13-J13 B22	Similar to above **Ba. Gains due to improvement of degraded bogs" changed to "8a. Change in emissions due to improvement of degraded bogs"	due to restoration and	Sarah Lister, Natural Power
	B23 - B26 D38 C38, E38	Similar to above =((D20+D26)*1000000)/(D12*1000) changed to =(D32*1000)/(E12) Similar to above	improvement Error in min / max calculation	Peter Batten
Windfarm CO2 emission saving		="Forestry input data"!\$F28 changed to =G39	The power curve code for Min and	Carlos Ruiz, SEPA
. Willula III CO2 etilission saving	H ₃₉	= rorestry input data:sr28 changed to = 439 Similar to above	Max were not correctly retrieved, because the dropdowns located in the tab Forestry Input Data cells	Carlos Ruiz, SEPA
	H40	=OFFSET(\$D\$24,H39,2) changed to =OFFSET(\$D\$24,H39,2)	F28 and H28 do not have any value associated to them. Column in offset incorrectly	
	140-U40 H44	Similar to above =OFFSET(\$D\$24,H39,4) changed to =OFFSET(\$D\$24,H39,5)	specified Column in offset incorrectly	
	140-U40 G49	Similar to above =24*365*G11*G10*G48/100 changed to =IF(G10<=0,0,24*365*G11*G10*G48/100)	specified	
	H48-U49	Similar to above	Incorrect calculation of annual energy output when less than 5 areas of forestry included.	
CO2 loss due to turbine life	C19-T19	o.173 changed to 0.316	The emission rate of 173kg/m3 is	Carlos Ruiz, SEPA
			the rate for "mass foundations". However foundations for wind turbines are reinforced, so the rate is changed to that for Reinforced Foundations, and revised to the new emission rate, from the Table 7 in http://www.concretecentre.com/s ustainability/energy_efficiency/em bodied co_asox	
	C23	=IF('Core input data'!\$C\$20=1,\$C9+C20,\$C13+C20) changed to =IF('Core input data'!\$C\$20=1,\$C9,\$C13+C20)	Direct input of emissions includes cement already	
a. Volume of peat removed	D23-E23 F26	$\label{eq:similar to above} \begin{split} &= \text{Fa-$\alpha^{(F_{22}-F_{24})}(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24})(F_{22}-F_{24}$	Error in formula	Carlos Ruiz, SEPA
. Volume of peat drained	G26-T26 C34	Similar to above =C33*C23 changed to =F34+l34+L34+O34+R34		Carlos Ruiz, SEPA
	D ₃ 4-T ₃ 4	Similar to above		
	C ₅₅	='Core input data'!C7o changed to =C52*(C9+C9)		
	D ₅₅ -E ₅₅	Similar to above		
	C ₇₃ D ₇₃ -E ₇₃	=C72+C9 changed to =IF(C70>0,C72+C9,0) Similar to above		
I. CO2 loss from drained peat	C43	=(28*(C35+C36)*((C42*C34))/365 changed to =(28*(C35+C36)*(((C42*C34)/365)+(C29*(365-C34)/365))	Accounts for emissions during both flooded and unflooded times of the year in an undrained soil	Carlos Ruiz, SEPA
	D43,E43 C40	Similar to above $= (3*(c_3)*(-2)^6)*(c_3)*((-3)^8(-2,4))/365 \text{ changed to} \\ = (3*(-2,5)^6)*(-2)^3*(((-3)^8(-2,4))/365)*((-2,5)^6)(-2,5)^6)(-2,5)(-$		
	D40,E40 D50	Similar to above =D ₄₇ -D ₄₈ changed to *IF(D ₄₇ -D ₄₈ <e<sub>47-E₄8,D₄₇-D₄₈,E₄₇-E₄8)</e<sub>	Protection against unusual conditions that result in incorrect order for min and max calculations	Carlos Ruiz, SEPA
e. Emission rates from soils	E50 D31	Similar to above ="Core input data"!G24 changed to ="Core input data"!E24	Correction from previous min/max change	Carlos Ruiz, SEPA
ore input data	E31 C103 E103, G103, C107, E107, G107			Carlos Ruiz, SEPA
a. C sequest. in trees (3PG)	E24 F24, G24, E25-G25, E26-G26	=AVERAGE(F24,124,L24,O24,R24) changed to =AGGREGATE(1,6,F24,124,L24,O24,R24) Similar to above	Correction to avoid error when some areas of foresttry are not filled.	Carlos Ruiz, SEPA
	F ₂₅ G ₂₅ -T ₂₅	$= VLOOKUP(F15_5 C62:SAQ212_5 G, TRUE) \ changed \ to \ = VLOOKUP(F15_5 B62:SAQ212_10_7, TRUE) \\ Similar \ to \ above$	Correction to formula so that it looks in the age column	
	F ₂ 6	$= SUM(OFFSET(((INDIRECT(ADDRESS(MATCH(F19,$862:$8112,0)*61,9,4)))),0,1,F19,1)) \\ changed to = SUM(OFFSET((((INDIRECT(ADDRESS(MATCH(F18,$862:$8112,0)*61,9,4)))),0,1,F19,1)) \\ changed to = SUM(OFFSET((((INDIRECT(ADDRESS(MATCH(F18,$862:$8112,0)*61,9,4)))),0,1,F19,1)) \\ changed to = SUM(OFFSET((((INDIRECT(ADDRESS(MATCH(F18,$862:$8112,0)*61,9,4))),0,1,F19,1)) \\ changed to = SUM(OFFSET((((INDIRECT(ADDRESS(MATCH(F18,$862:$8112,0)*61,9,4))),0,1,F19,1) \\ changed to = SUM(OFFSET((((INDIRECT(ADDRESS(MATCH(INDIRECT($	Change to correct lookup of net primary production of replanted	
. Wind speed ratios	G26-T26	F19,1)) Similar to above	forestry Changes to calculate final height	Carlos Ruiz, SEPA
a. visitu apeeu Idilos	Insert row 9 C9 D9-Q9	Years after planting when felling occurs ='Forestry input data'ID41 Similar to above	of replanted forestry by accounting for years after felling	CONTROLL, JEI A
	Insert row 10 C10	#Forestry input data!!D42	when replanting occurs and age of seedlings as well as lifetime of	
	D10-Q10	Similar to above	windfarm - previously only	
	C21 D21-Q21	=VLOOKUP(C11-)z. Average stand data*sDs30:sHs63,2,TRUE) changed to =VLOOKUP(C11-C9+C10,7c. Average stand data*sDs30:sHs63,2,TRUE) Similar to above	accounted for lifetime of windfarm.	
	C22	=OFFSET(")c. Average stand data"sD ₃ 0,C8-")c. Average stand data"sD ₃ 0-C11,1,1) changed to =lf(C8+C11<=S0,OFFSET(")c. Average stand data"sD ₃ 0,C8-")c. Average stand	Change to allow for normal harvesting of forestry during the lifetime of the windfarm	
	D22-Q22 C52	data*IsO3+C1-150+C1-C-03,1,1) Similar to above =IF((0.75+0.03*(LN(C43/C44)))*C44*POWER(C18/C44,0.8)+C46 <c49,(0.75+0.03*(ln(c43 c44)))*c41*c44*(ln(c42="" c44)))*c44*power(c18="" c44))*c41*(ln(c42="" c44))*c41*c44*(ln(c42="" c44))*c<="" c44,0.8)+c46<c49,(0.75+0.03*(ln(c42="" c44,0.8)+c46<c49,(0.75+0.03*(ln(c43="" td=""><td>height of new internal boundary</td><td></td></c49,(0.75+0.03*(ln(c43>	height of new internal boundary	
	D52-Q52)))*C44*POWER(C18/C44,0.8)*C46,C49) Similar to above	roughness of group in gap instead of roughness of ground in forested area	
			Changes to correct the calculation	
	C ₅₄	$ \label{eq:constraints} \begin{split} & = F((0.75 \circ 0.03^\pm LN(C_44/C_4))^* C_45^* POWER(C_19/C_22,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49) + changed to \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_45^* POWER(C_19/C_45,0.8) + C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_47^* C_49,(0.75 \circ 0.03^\pm LN(C_44/C_45))^* \\ & = F((0.75 \circ 0.03^\pm LN(C_44/C_45))^* C_47^* $	of height of boundary layer in replanted area	
onstruction input data	C ₅₄ D ₅₄ -O ₅₄ C ₁₃	$C_4S^*POWER(C_3(C_4S_0.8)+C_4P,C_4g)\ changed to \\ = f(C_0.7S+0.02^kLN(C_44 C_4S))^kC_4S^*POWER(C_1g)(C_4S_0.8)+C_4P^*C_4g_3(0.7S+0.03^kLN(C_44 C_4S))^k\\ C_4S^*POWER(C_13g(C_4S_0.8)+C_4P,C_4S)\\ Similar to above \\ "Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat$	of height of boundary layer in replanted area Changes in wording to improve	Carlos Ruiz, SEPA
	D54-O54 C13 C20, C34, C41, C55, C62, C76, C83, C97, C104	$C_4S^*POWER(C_3)(C_4S_0.8)^*+C_47^*C_49)\cdot changed to \\ **IF((0.75^*0.03^\pm LN(C_44)(C_4S))^*+C_45^*POWER(C_1g)(C_4S_0.8)^*+C_47^*C_49,(0.75^*0.03^\pm LN(C_44)(C_4S))^*+C_45^*POWER(C_1g)(C_4S_0.8)^*+C_47^*C_49)$ Similar to above $"Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" Similar to above$	of height of boundary layer in replanted area Changes in wording to improve clarity of input data	
	D54-Q54 C3 C20, C34, C42, C55, C62, C76, G83, C97, C104	$C_4S^*POWER(C_3)(C_4S_0.8)^*C_4P,C_4g)\ changed to **IR(0,75_90.2)^*LN(C_4G_2)(0,75_90.03^*LN(C_4G_2))^*C_4S^*POWER(C_1g)(C_4S_0.8)^*C_4P,C_4g,(0,75_90.03^*LN(C_4G_2))^*C_4S^*POWER(C_1g)(C_4S_0.8)^*C_4P,C_4g)$ Similar to above "Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" Similar to above "Core input data" scale (a) Similar to above "Cor$	of height of boundary layer in replanted area Changes in wording to improve clarity of input data Correction of error	Carlos Ruiz, SEPA
onstruction input data Windfarm CO2 emission saving	D54-O54 C13 C20, C34, C41, C55, C62, C76, C83, C97, C104	$C_4S^*POWER(C_3)(C_4S_0.8)^*+C_47^*C_49)\cdot changed to \\ **IF((0.75^*0.03^\pm LN(C_44)(C_4S))^*+C_45^*POWER(C_1g)(C_4S_0.8)^*+C_47^*C_49,(0.75^*0.03^\pm LN(C_44)(C_4S))^*+C_45^*POWER(C_1g)(C_4S_0.8)^*+C_47^*C_49)$ Similar to above $"Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" Similar to above$	of height of boundary layer in replanted area Changes in wording to improve clarity of input data	
	D54-Q54 C13 C20, C34, C41, C55, C62, C76, C83, C97, C104 H17	C45*POWER(C45/C45,0.8)+C47,C49) changed to **IR(0.75+0.02*INCA4/C45)]**C47*C49,(0.75+0.03*LN(C44/C45))**C45*POWER(C19/C45,0.8)+C47,C49) Similar to above "Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" similar to above "Similar to above "Core input data"!SC\$41 changed to "Core input data"!SE\$41 **AVERAGE(G48,148,M48,P48,S48) changed to "AGGREGATE(1,6,G48,148,M48,P48,S48)	of height of boundary layer in replanted area Changes in wording to improve clarity of input data Correction of error Changes to average capacity factor only over forcestry areas that	Carlos Ruiz, SEPA
Windfarm CO2 emission saving	D54-O54 C13 C20, C34, C42, C55, C62, C76, C83, C97, C104 H17 D48 E48,F48	C45*POWER(C45(C45,0.8)+C47,C49) changed to #ER(O75:0.92*LN(C44)C45)** C45*POWER(C45)(C45,0.8)+C47,C49) Similar to above "Depth of hole dug when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" changed to "Average depth of peat removed when constructing foundations (m)" Similar to above "Core input data"!5C\$41 changed to "Core input data"!5E\$41 *AVERAGE(G48,J48,M48,P48,S48) changed to "AGGREGATE(1,6,G48,J48,M48,P48,S48) Similar to above "Core input data"!521*D12**Core input data"!51*L4**1. Windfarm CO2 emission saving"!D48/100 changed to "Core input data"!521*D12**Core input data"!51*L4**1. Windfarm CO2 emission saving"!D48/100 changed to "Core input data"!521*D12**Core input data"!51*L4**1. Windfarm CO2 emission	of height of boundary layer in replanted area Changes in wording to improve clarity of input data Correction of error Changes to average capacity factor only over forestry areas that have valid data Changed so that minimum and maximum emission factors are	Carlos Ruiz, SEPA Jo Smith, University of Aberdeen

	F69	Dropdown menu linked to cell D69		
	H69	Similar to above		
	F88	Dropdown menu linked to cell D88		
	H88	Similar to above		
	F107	Dropdown menu linked to cell D107		
	H107	Similar to above		
ii. Forestry CO2 loss - detail	F ₃₇	='7a. C sequest. in trees (3PG)'!\$F\$25 changed to ='7a. C sequest. in trees (3PG)'!F\$25	Change to correctly reference	Carlos Ruiz, SEPA
	G ₃₇ -T ₃₇	Similar to above	different forestry areas	
	F ₅₂	='7a. C sequest. in trees (3PG)'!\$F19 changed to ='7a. C sequest. in trees (3PG)'!F19		
	G52-T52	Similar to above		
	F53	='7a. C sequest. in trees (3PG)'!\$F26 changed to ='7a. C sequest. in trees (3PG)'!\$F26		
	G53-T53	Similar to above		
	138	='Forestry input data'!\$D39_changed to ='Forestry input data'!\$D58	Change to refer to different	
	J ₃ 8-T ₃ 8	Similar to above	forestry areas	
	D61	='Forestry input data'!\$D23/1000000 changed to ='Forestry input data'!\$F23/1000000	Change to reference the correct	
	G61,J61,M61,P61,S61	Similar to above	cell	
	E61	='Forestry input data'!\$D23/1000000 changed to ='Forestry input data'!\$H23/1000000		
	H61,K61,N61,Q61,T61	Similar to above		
	G63	=IF(G55>0,(G57*'Core input data'!\$C41)-G62,0) changed to =IF(G55>0,(G57*'Core input		
	203	data'!\$E41)-G62,0)		
	H83-T63	Similar to above		
ore input data	E23	Menu linked to cell C23	Change to allow only one soil type	Carlos Ruiz, SEPA
	G23	Similar to above		
. CO2 gain - site improvement	D62	=-12*D60/1. Windfarm CO2 emission saving!\$D53 changed to =-12*D60/1. Windfarm CO2	Change to allow use of different	Carlos Ruiz, SEPA
		emission saving'!sE53	counterfactual emission factors	
	E62-N62;D63-N63;D64-N64	Similar to above		

CHANGES IN VERSION 2.11.0

Martin bara	Cells	Character	C	Therefore
Worksheet	Cells	Change	Comment	Thanks to
5e. Emission rates from soils	D21	=IF('Core input data'!D23=1,D11,D16) changed to =IF('Core input data'!C23=1,D11,D16)		Peter Batten
	E21	=IF('Core input data'!E23=1,D11,D16) changed to =IF('Core input data'!C23=1,D11,D16)		
	Dan Eng Dan Eng	Cincilar to above		

CHANGES IN VERSION 2/2.0						
Worksheet Core input data	<u>Cells</u> C27,E27,G27	Change Cell validated to be betweeen 0.01 and 1000	Comment Avoids incorrect entry of zero for extent of drainage	Thanks to Carlos Ruiz, SEPA		
Payback and CO2 emissions	C ₃₇	=IF(C26>o,(C17+C18)/C26,"No gains!") changed to =IF(C26>o,(C17+C18)/C26,"No gains!")	Error introduced by change in sign of C26			
	D ₃₇	=IF(D26<0,-(D17+D18)/D26,"No gains!") changed to	Error introduced by change in sign of D26 plus correction in use of minimum and maximum values	Alexa Morrison, RSPB		
	E ₃₇	Similar to D ₃₇				
2. CO2 loss due to turbine life	C9,D9,E9	"Core input data"(C21*C22*Core input data"(C14*1. Windfarm CO2 emission saving"(D48/200 to "Core input data"(C22*C12*"Core input data"(C14	Corrected to remove dependence on capacity factor	Clare Wharmby		

CHANGES IN VERSION 213.0 CHANGES MADE BY SEPA - REPLICATED IN VERSION 2.14

CHANGES IN VERSION 214.0						
Worksheet 5a. Volume of peat removed	<u>Cells</u> F ₃₇ G ₃₇ ,H ₃₇ I ₃₇ J ₃₇ - T ₃₇	$\label{eq:change} \begin{split} &\frac{Change}{\text{will $($\xi_3$)=2,'$Core input data'!$C_54,'$Construction input data'!$D_13)$} \rightarrow \text{will $($\xi_3$)=2,'$Core input data'!$D_20)$} \\ &\text{Similar to above} \\ &\text{will $($\xi_3$)=2,0,'$Construction input data'!$D_34)$} \rightarrow \text{will $($\xi_3$)=3,0,'$Construction input data'!D_42} \\ &\text{Similar to above} \end{split}$	Comment Correction to use depth of hardstanding instead of depth of foundations	Thanks to Clare Wharmby - Carbon Forecast		